

LUNAR EXCURSION MODULE

## PRIMARY GUIDANCE, NAVIGATION, AND CONTROL SYSTEM MANUAL

**VOLUME** 1







### APOLLO

LUNAR EXCURSION MODULE

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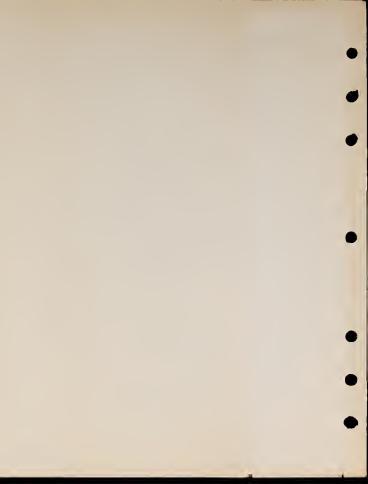
**VOLUME I OF II** 

PREPARED FOR

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MANNED SPACECRAFT CENTER

AC ELECTRONICS
DIVISION OF GENERAL MOTORS
MILWAUKEE, WISCONSIN 53201

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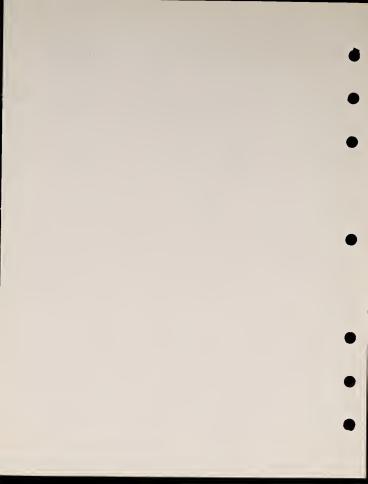
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4-34W Added A 4-86 Blank Original 4-34W Blank A 4-87. Original 4-34W Blank Original 4-34AB Blank A 4-89 Blank Original 4-34AB Blank A 4-90 Blank Original 4-34AC Bru 4-34AE Added A 4-90 Blank Original 4-34AC Bru 4-34AE Added A 4-91 L Original 4-34AC Bru 4-34AE Added A 4-92 Blank Original 4-34AC Bru 4-34AE Added A 4-93 Blank Original 4-34AC Bru 4-34AB Added A 4-93 Blank Original 4-34AC Bru 4-34AB Added A 4-95 Blank Original 4-34AC Bru 4-34AB Added A 4-96 Blank Original 4-34AO Bru 4-34AB Added A 4-96 Blank Original 4-34AU Bru 4-34AB Added A 4-97 Original 4-34AU Bru 4-38 Added A 4-98 Blank Original 4-34AV Added A 4-98 Blank Original 4-34AV Added A 4-99 Blank Original 4-35 Blank Original 4-36 Blank Original 4-37. T 4-101 Original 4-38 Bru 4-40 Original 4-42 Bru 4-42 A 4-103 Original 4-44A Bru 4-42 Added A 4-104 Blank Original 4-44A Bru 4-42 Added B 4-106 Blank Original 4-44A Bru 4-44C Added B 4-106 Blank Original 4-44A Bru 4-44C Added B 4-106 Blank Original 4-44A Bru 4-44C Added B 4-106 Blank Original 4-44B D W 4-110 Bru 4-112 U 4-45 Bru 4-47 W 4-111 Bru 4-112 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-120 Bru 4-121 U 4-48 Blank W 4-131 Bru 4-119 Original 4-48 Dru 4-48 Added W 4-131 Bru 4-119 Original 4-48 Dru 4-48 Dru 4-48 Dru 4-14 Dru 4-121 U 4-50 Bru 4-48 Dru 4-48 Dru 4-14 Dru 4-15 Dru 100 Bru	Page No.	Rev.	Page No.	Rev.
4-34Y thru 4-34AA Added A 4-88 Blank Original 4-34AC thru 4-34AE ddded A 4-90 Blank Original 4-34AC thru 4-34AE ddded A 4-90 Blank Original 4-34AC thru 4-34AI Added A 4-91	4-34W Added			
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#### LIST OF RELATED MANUALS

ND-1021038 ND-1021039 ND-1021040 ND-1021043 Packing, Shipping and Handling Manual Auxiliary Ground Support Equipment Manual Bench Maintenance Ground Support Equipment Manual Block II Primary Guidance, Navigation, and Control System Manual



Engineering change proposals (ECP's) which affect this manual and from which pertnent data has been incorporated are listed below. Unless otherwise specified, the ECP number listed is an AC Electronics ECP number.

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
172	GSE Statement of Work Change		_	Basic
179	GSE-PSA Filter Change			Basic
221	180 Degree Z IRIG Rotation			Basic
57	LEM Dimming Circuit			В
86	Additional GSE Items			В
204	Block II Temperature Control Change			В
306	IMU Harness Cable Clamp	102636	8102658	В
361	Exhibit D Statement of Work Change			В
388	Corrosion Protection	102645 102648 102650 102651 102652	8102670 8102674 8102676 8102677 8102678	В

# MANUAL

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
197R2	Vacuum Testing of AOT			c
248	Pulse Torque Power Supply Redesign	102640	8102663	С
340	Navigation Base Redesign			С
360	Addition of AOT Cam Lock			С
321	AOT Eyepiece Heater Addition			С
421	Eyepiece Redesign to Provide Long Eye Relief Capability			С
389	ECP of Record for Improved Protective Covers for Cables (PN 2014137-011 and PN 2014199-011)			Е
410	Relocation of AOT Focus Adjustment Cam Lock			E
422	CCRD Mounting Change			E
473	Pseudo Field Stop to Elimi- nate Light Scatter from the Radar Mount			Е
226	Aluminum to Magnesium Conversion of Computer Trays			F
254	Computer Multilayer Board Layout			F
257	Redesign of Rope and Erasable Memory Drivers			F
258	Redesign of Computer Power Supply Module			F

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
259	Redesign of Computer Erasable Memory			F
291	Redesign of DSKY Alarm Lights			F
324	Computer Sense Amplifier Change			F
351	Modify Computer Alarm Module			F
402	Computer Clear Driver Circuit Modification			F
403	Computer Strobe Adjustment			F
460	Addition of Jumper Wires in Tray A of Computer			F
176	Computer Module Vibration			Н
263	PSA Helicoil Change			II
296	Cementing Relay Assembly			11
301	Thermal Instrumentation			Н
316	PSA and PTA Header Change			Н
318	Corrosion Protection of Exposed Beryllium			Н
320	Edge Blackening of AOT Lense	s		Н
322	Computer Wiring Changes			Н
336	Change CDU Potting Material			Н

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
353	Change AOT Pressure Seal Material			Н
355	IRIG Change			Н
367	Addition of Light Diffusing Paint to DSKY			Н
368	Improved Computer Power Supply Module Relays			н
419	DSKY Indicator Drive Module Relay Replacement			Н
440	"Clear Rope" Driver Circuit Modification	0104101	8104209	Н
443	Replacement of Computer Screws			Н
447	Replacement of Plastic Pads under Computer Tray A and B Covers	0104101	8104209	Н
452	Computer Wiring Changes to Accommodate Auxiliary Memory Unit			Н
454	AOT Pinning			Н
461	Replacement of Diodes in Gimbal Servo Amplifier	0102666	8102696 8102707	Н
462	Addition of Ground Strap to LEM Nav Base	0102668	8102701	Н
470	Random Workmanship Vibration			Н

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
474	Computer Test Connector Jumpers	0104113	8104221	Н
476	Painting of DSKY Alarm Indicator Face			Н
478	Painting of Exposed Surfaces on Computer Mid-Tray Spacer			н
479	DSKY Teflon Coated Push- button Shaft			Н
485	Redesign Computer Power Supply			Н
486	Cut Pins on Computer Power Supply	0104104	8104212	Н
489	Replacement of Transformers in LEM ECDU	3		Н
493	DSKY Y-Line Feedback Base Resistor Change			Н
494	DSKY Wiring Improvement			н
499	Addition of ECDU Damper Plate		8102712 8102719	Н
500	Replacement of Capacitor in PIPA Preamplifier	0102681	8102717 8102715 8102716	н
501	Implementation of Flight Processing Spec ND-1002313		8102713	Н
515	Replacement of Resistors in ECDU CSA			Н

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
518	Standby Change on Computer			н
533	Addition of Uplink Wires in A Harness		8102726	Н
483	Correction of Sense Ampli- fier Breakdown			J
505	Implementation of Flight Processing Spec ND-1002341 and New Diode			J
511	Correction of Computer Nois SCAFAL Problem	e		J
148	CDU Transformer Change			K
173	Reticle Mount and Objective Lense Assembly			K
179	G and N Filter Change			K
191	CDU Electronics Module Change			К
217	Delete Signal Conditioner Power Supply Assembly			К
221	Z Axis Irig Rotation			К
307	Middle Axis Assembly Clamp Changes			К
308	Stable Member Heat Transfe Change	r		К
309	PIP Temperature Deviation Reduction and Temperature Alarm Test			К

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
310	IMU Cross Coupling change			к
359	Replacement of IMU Mounting Bolts	0102643	8102668	к
505	Implementation of Flight Processing Specification ND1002314 and New Diode			к
302	Manufacture of Block II and LEM Signal Conditioner Assemblies			L
538	Replacement of CCRD Reticle Brightness Potentiometer			L
558	Replacement of Mounting Hardware in LGC Installation Kit	0104120		L
358	Redesign of AGC Handling Fixture	0104096	8104172	M
506	Modification of AGC Handling Fixture (Block II)			M
509	AGC/GSE Compatibility	0104107	8104215	M
512	AOT High Density Filter Assembly			M
539	AOT Reticle Lamp Change		8106058	M
540	AOT Reticle Knob Change		8106058	M
542	AOT Eyeguard Plug		8106058	M
543	AOT Counter Moisture Proofing and Illumination		8106058	M

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
562	Replacement of LM-1 Harness Lacing Tape			М
585	PIP Preamplifier Capacitor Replacement		8102733 8102734	M
594	CCRD Aluminum Overlay		8102738 8102735 8102729	М
605	IMU Blanket Removal	0102687 0102688	8102733 8102734	M
603	Capacitor Replacement in CDU MSA and Quadrature Rejection Module		8102744 8102746	R
609	Elimination of CDU DAC Saturation during coarse align		8102744 8102746	R
577	Addition of Diode to LEM PSAAM's			s
582	LTA-8 Modifications			s
587	IRIG Gyro End Cap Replace- ment			S
596	LM-2 Modifications			S
618	LM-3 Modifications			s
622	Non-metallic materials Flammability Modification for PSA	0102690	8102754	S
624	Non-metallic materials Flammability Modification for SCA	0102691	8102749	S
626	Modification of LEM Harness Group for Flammability Protection	0102692	8102751	s

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
564	Implementation of Flat Pack Specifications ND 1002359A and ND 1002358B			U
631	Replace RTV-102 with RTV-109	0102679 0102689 0102690	8102752 8102755 8102754 8102766	U
653	Modification of IMU Wiring to Reduce IRIG Pre-Amp Oscillation		8102763	U
641	Non-metallic Materials Modification for DSKY	0104126	8104241	W
655	New LGC Mounting Bolts and Spacers			W
673	Redesign of DSKY Push- button Cap Housing Assembly Leaf Spring	0104126	8104241	W
678	IRIG End Cap Change	0102697	8102767 8102768	W
633	AOT Pressure Seal Protec- tion and Other Flammability Fixes	0106049 0106048	8106069 8106073	
604	Incorporation of E-memory Vibration Pads			Z
688	Modification of IMU to Reduce Sporadic Oscillation of IRIG Preamps		8102773 8102774	
657	Conical Sunshade and Radar Shield Assembly for AOT	0106050	8106076	AC
697 Rev. Z	AOT Harness Protective Shield	0106054	8106085	AC I-xxx

ECP No.	Functional Description	Retrofit Instruction Bulletin (RIB) No.	Kit No.	Incorporated In Manual Revision
719	Computer Alarm Module Modification, V-Fail Detection	0104132	8104248	AD
735	DSKY IL and EL Safety Glass Fix	0104135	8104251	AD
743	New Configuration of Installation Kit			AD
<b>7</b> 57	Design Changes to Correct LEM PSA Reverse Power Problem			AE
768	DSKY EL thermal/ Vacuum Screen modification	0104138	8103954	AG
739	Addition of 4 lights on DSKY indicator panel	0104136	8103952	AG
780	Taping of AOT cable			AG
781	ECDU mounting bolt change in length	0102703	8102789	AG
815	Replace AGC Connector Assembly with a restart monitor	0102705	8102793	АН
1017 & 1032	Replace blower motor in IMU to increase reliability	-	8102796	AJ
1030	Replace ECDU modules containing 1010274 transformers to increase reliability	-	-	AJ

#### WARNING AND CAUTION PAGE

The following warnings and cautions apply to the system for which this manual was written. These warnings and cautions must be observed to avoid personal injury and/or equipment damage.

CHEMICAL HAZARDS

# WARNING

Beryllium is a highly toxic metal. Procerses such as deburring, machining, or grinding of beryllium, if expressly authorized, as well as other procedures that produce airborne beryllium particles, should be performed with local exhaust ventilation which is connected with an acceptable exhaust-filtration system. The inhalation of airborne beryllium particles can cause serious respiratory disability. All injuries where the skin is damaged, including puncture wounds and skin rashes, should be reported immediately so that proper treatment measures can be taken. Air in these areas should be monitored to insure that the amount of airborne beryllium remains below the established threshold limit value.

CAUTION: Wear nylon gloves or finger cots while handling beryllium parts unless parts are to be immediately cleaned after bandling. Moisture and oils from the skin bave a highly corrosive effect on beryllium.

### WARNING

When using equipment containing mercury (i.e. battery power pack; auxiliary battery pack; differential voltmeter, Fluke 803B), avoid spilling mercury. Mercury is a toxic metal and may contaminate equipment, clothing, and body. After use of such equipment, visually inspect area and equipment to verify absence of mercury. If mercury contamination exists, see mercury use guide lines (page 1-xxxivB).

### WARNING

Do not leave mercury in open <u>containers</u>. Keep in tightly closed unbreakable container when not in use, since mercury vanor is toxic.

CAUTION: Avoid spilling mercury from open mercury pool. Liquid or vaporous mercury can cause severe corrosion and/or cracking of unprotected aluminum and other non-ferrous metals. If mercury contamination of equipment exists, report to AC Electronics site manager and site quality control representative.

# WARNING

Wear goggles, rubber gloves, and rubber aprons when working with acid solutions. Do not spatter solution. If acid contacts skin or eyes, immediately flush affected area with mild boric acid solution or water and report to nearest medical facility.

# WARNING

Do not spatter battery cell <u>electrolyte</u>. If electrolyte contacts skin or eyes, immediately wash affected area with mild boric acid solution or water and report to nearest medical facility.

CAUTION: Always add acid to water; do not pour water into acid. Equipment surface can be damaged from uncontrolled chemical reaction. However, distilled water, if required, may be slowly added to replenish the electrolyte of a battery.

CAUTION: Keep battery cells upright, unless otherwise noted, to prevent loss of electrolyte.

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CAUTION: Add only distilled water to nickel cadmium battery cells. Never add acid or use instruments that have been used to fill lead acid batteries. Acid will damage the plates of the nickel cadmium cells.

CAUTION: Prevent acid from contacting painted surfaces. Immediately wipe off any acid on a painted surface, since prolonged contact will cause damage.

#### ELECTRICAL HAZARDS

### WARNING

Use extreme care when reaching inside the <u>G and N coolant and power console</u>. Lethal voltages exist at power line filters and at the power and signal input panel.

# WARNING

Always use <u>moisture-proofing protection</u> (covers, rubber seals, gaskets, and sealing compound) for <u>PSA</u> connectors and <u>pins</u> not secured to mating connectors. Otherwise, <u>connectors</u> and <u>pins</u> corrosion may cause short circuits.

CAUTION: Maintain <u>IMU heater power</u> at all times, except during use of IMU shipping container, to prevent damage to IMU.

CAUTION: Handle G and N harnesses with care to avoid damage to connectors, conductor wires, and/or potting.

CAUTION: Turn off equipment when any power connections are being made to prevent pin damage due to arcing.

CAUTION: Exercise extreme care when removing and installing electrical connectors. Visually check all pins for straightness. Where applicable, use specialgages and reticles to check pin alignment during connector removal or installation. Install or remove connectors with jack screws by turning each screw one turn at a time to maintain parallelism between plug and connector during entire operation. Otherwise, bent pins can cause short circuits and additional equipment damage.

#### MECHANICAL HAZARDS

# WARNING

Do not extend any equipment <u>cabinet drawer slides</u> until drawers are to be installed. The extended slides can cause serious injury to personnel.

# WARNING

Do not extend more than one <u>cabinet drawer</u> at a time. Extension of more than one drawer at a time can cause console to topple, endangering personnel and equipment.

### OPTICAL HAZARDS

CAUTION: Always keep lens covers on optical equipment when it is not in use to protect optically ground and coated surfaces from damage.

#### MERCURY USE GUIDE LINES

- A. Mercury is volatile at room temperature, and mercury and mercury vapors are toxic. If mercury is accidentally spilled, avoid further contamination using the following methods:
  - (1) Ventilate area with fans or other suitable means during clean-up.
  - (2) Clean up major portion of spill.
- B. Avoid prolonged or repeated contact with skin.
- C. Wash hands thoroughly with soap and warm (<u>not</u> hot) water before eating or smoking.

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#### Chapter 1

#### SYSTEM TIE-IN

#### 1-1 SCOPE

This chapter presents the lunar excursion module (LEM) mission. The chapter also describes the functional interface between the primary guidance, navigation, and control system (PGNCS) and the other spacecraft systems.

#### 1-2 LEM MISSION

The purpose of the LEM mission is to transfer the LEM from a circular lunar orbit into a descent orbit, land two astronauts on the lunar surface, and return them to the orbiting command and service module (CSM). The LEM mission (figure 1-2), with respect to the PGNCS, is best described by dividing it into six phases: separation and transfer orbit insertion, descent coast, powered descent and landing, lunar stay, launch and powered ascent, and rendezvous and docking.

1-2.1 SEPARATION AND TRANSFER ORBIT INSERTION. Approximately one hour before the LEM enters the descent orbit, two astronauts leave the CSM and enter the LEM through the top docking hatch. The crew then checks out the various LEM systems, establishes a voice link, and, after initial PGNCS turnon, establishes a time reference for the LEM guidance computer (LGC), and coarse aligns the inertial measuring unit (IMU) using CSM data. One astronaut then manually commands reaction control system (RCS) jet firing to separate the LEM from the CSM. The IMU is fine aligned. Near the end of the second lunar orbit, the LEM descent engine is fired by the PGNCS and the LEM begins its descent. The timing and duration of LEM descent engine firing is critical, to insure the proper elliptical Hohmann transfer orbit.

1-2.2 DESCENT COAST. During the descent coast phase, the LEM is in free fall on an elliptical flight path. During free fall, the astronauts check out the landing radar (LR). At the perilune of the Hohmann transfer orbit, the LEM is at an altitude of approximately 50,000 feet and has a velocity vector essentially parallel to the lunar surface. During this phase, the PGNCS determines the flight parameters required for powered descent. The rendezvous radar (RR) tracks its transponder in the orbiting CSM and provides the LGC with updated information on the position of the CSM.

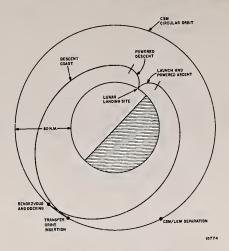


Figure 1-2. LEM Mission Phases

1-2.3 POWERED DESCENT AND LANDING. In preparation for powered descent, an IMU fine alignment is performed. At the perilune of the descent orbit, the PGNCS issues a descent engine start discrete. The descent engine firing slows the LEM which hegins the actual descent to the lunar surface. During descent, the PGNCS controls the engine trim and thrust level, controls the LEM attitude, and provides visual displays of the guidance system status. During the final approach and landing, the PGNCS holds the LEM at a constant attitude, allowing the astronaut to view the landing site. The astronaut can select a new landing site by inserting new landing site coordinates into the LGC. The LGC will automatically control the RCS and the descent engine to guide the LEM to the new landing site. Inertially derived flight parameters are updated in the LGC hy comparison with the altitude and velocity parameters determined from LR measurements.

1-2.4 LUNAR STAY. After LEM touchdown the astronauts check out all systems for damage and insure that the systems can perform the functions required for a successful ascent. All equipment not required for lunar stay is then turned off. The astronauts survey the surrounding lunar landscape, secure the hatches, and perform a final check on the portable life support system (PLSS). After the LEM is secured, one astronaut, wearing the PLSS, leaves the LEM to explore the lunar surface. The exploring astronaut inspects the LEM and sets up communication antennas. A television system sends pictures of the lunar scene to earth. The astronaut, always indirect voice contact with the LEM, explores the lunar surface, makes photographic records, and collects surface samples. After approximately three hours, the astronaut must return to replenish his PLSS. Additional surface explorations depend upon the planned stay time. Near the end of the lunar stay, the PGNCS is brought to an operate condition and the IMU is coarse and fine aligned. The IMU is fine aligned to a known reference coordinate system by making star sighting measurements with the alignment optical telescope (AOT). RR tracks its transponder in the orbiting CSM and sends data to the LGC which calculates applicable flight parameters in preparation for the launch and power ascent.

1-2.5 LAUNCH AND POWERED ASCENT. After the astronauts prepare the LEM, the PGNCS determines time of launch and ascent trajectory based on a fixed rendezvous aim point. Mechanical and electrical separation of the two LEM stages takes place and the LGC issues the ascent engine start discrete at a time calculated to effect a successful rendezvous.

During powered ascent, the LEM rises vertically and then is pitched to attain a Hohmann transfer orbit for the rendezvous. Because the ascent engine is a fixed-position, fixed-thrust engine, the LEM attitude during ascent is controlled by the LGC which issues commands to the RCS jets. The LGC determines necessary RCS commands by comparing calculated values with actual flight parameters obtained from the inertial subsystem (ISS), and determines required attitude changes to correct any differences. When the injection of the LEM into the proper elliptical orbit is accomplished, the LGC issues the ascent engine off discrete and the LEM enters the coasting portion of the ascent phase.

1-2.6 RENDEZVOUS AND DOCKING. LEM guidance during this phase is a combination of radar tracking data and inertial data. Shaft and trunnion data from the RR and velocity and attitude information from the IMU are used by the LGC to control the RCS to maintain attitude and to provide a display of position and velocity information. During rendezvous, the LEM is maintained at an orientation such that the CSM is visible through the vehicle windows.

Terminal rendezvous maneuvers begin when the LEM and CSM are approximately five nautical miles apart. The LGC computes the intercept time and with this data updates the thrust vector and velocity requirements. Three ascent engine burns during terminal rendezvous reduce the closing rate to near zero. The LGC utilizes the RCS

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MANUAL

to maintain vehicle attitude during these burns. The final step is docking, which is initiated when the vehicles are approximately 500 yards apart. The astronaut uses the translation controller and attitude controller in a computer-aided manual operation to guide the LEM to hard docking with the CSM. The two astronauts then leave the LEM and transfer to the CSM through the vehicle's upper tunnel to prepare for the return to earth. The LEM is jettisoned following crew transfer to the CSM.

#### 1-3 LEM STRUCTURE

The LEM (figure 1-3) has two stages mated to form one structure: the ascent stage and the descent stage. These stages and the umbilical interconnecting cables can be separated at launch from the lunar surface or because of mission abort during descent.

The approximate LEM external dimensions are shown in figure 1-4. At earth launch, the weight of the LEM is approximately 30,000 pounds.

1-3.1 ASCENT STAGE. The ascent stage, constructed mainly of aluminum alloy, consists of the crew compartment, a midsection, aft equipment bay, tankage sections, associated hatches, and windows.

From the crew compartment, the astronauts control all phases of the LEM mission. The crew also uses this compartment as their operations center during their lunar stay.

The displays and controls associated with the PGNCS are located at the front of the crew compartment. The IMU, a portion of its electronics, and the AOT are located in an enclosure above the crew compartment. The remaining PGNCS components are mounted on coldplates to the rear wall of the ascent stage midsection.

The midsection is cylindrical, smaller than the crew compartment, and directly behind it. The ascent engine and related components are in the midsection, the LEM's center of gravity. Also contained in the LEM's midsection are the ascent engine hatch, top hatch, environmental control system (ECS), and equipment that requires crew accessibility.

To transfer from the CSM to the LEM while in lunar orbit, the crew uses the upper docking tunnel at the top centerline of the ascent stage. The forward tunnel, at the lower front of the crew compartment, is used for entering and leaving the LEM while on the lunar surface.

The aft equipment bay, at the rear of the vehicle, is separated from the midsection by a pressure-tight bulkhead. This area houses the glycol loop for the ECS, inverters, batteries, and equipment for the electrical power system (EPS).

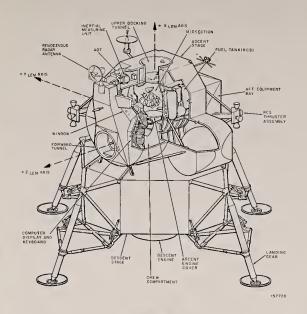


Figure 1-3. LEM

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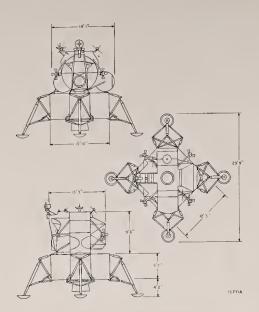


Figure 1-4. LEM External Dimensions

The propellant tankage sections are located on either side of the midsection outside the pressurized area. The tankage sections contain the ascent engine fuel and oxidizer tanks; RCS fuel, oxidizer, and helium tanks; and ECS water tanks. The ratio by weight of oxidizer to fuel is 1.6 to 1; therefore, to maintain the lateral center of gravity on the vehicle X axis, the ascent engine propellant tanks are offset to one side.

Two triangular windows in the front face of the crew compartment provide visibility. Each window has approximately 1.6 square feet of viewing area and are canted down and to the side to increase visibility. Each window consists of two panes.

1-3.2 DESCENT STAGE. The descent stage, constructed mainly of aluminum alloy, has equipment necessary to land on the lunar surface. It is also a platform for the launching of the ascent stage after completion of the lunar exploration. The descent engine is the center of the stage surrounded by its four main propellant tanks. In addition to the descent engine and its related components, the descent stage houses the descent control instrumentation; scientific equipment; EPS batteries; and tanks for water used by the ECS. Landing gear and the LR antenna are attached to the descent stage.

### 1-4 LEM SYSTEMS

Functionally, there are seven LEM systems. Four of these systems control the LEM flight. The PGNCS or the stabilization and control system (SCS) receives inputs from the crew and electrical inputs from the inertial sensors to generate commands that result in rotation and translation maneuvers. The RCS or propulsion system provides external forces and mechanical couples to maneuver the LEM under the control of the PGNCS, or the SCS. The crew obtains information from the LGC (part of the PGNCS), by communications (Manned Space Flight Network), or displays that indicate the necessity to initiate one or more of the basic LEM motions. The three remaining LEM systems are indirectly related to LEM control. They provide the power (EPS), environmental control (ECS), and the communications [communications instrumentation system (CIS)].

1-4.1 PRIMARY GUIDANCE, NAVIGATION, AND CONTROL SYSTEM. The PGNCS provides the measuring and data processing capabilities and control functions necessary to accomplish the LEM mission. The PGNCS utilizes inertial components for guidance, an optical device and radar for navigation, and a digital computer for data processing and issuance of flight control signals.

The inertial guidance portion of the PGNCS, the IMU, employs accelerometers mounted on a gyroscopically stabilized gimbal-mounted platform. The IMU senses acceleration and attitude changes instantaneously and provides signals to a digital computer, the LGC, for the generation of attitude control and thrust commands.

For navigation, the PGNCS utilizes the AOT to take star sightings and obtain measurements. These sightings are used by the LGC to establish proper alignment of the stable platform. The LGC contains a catalog of celestial bodies and is programmed to calculate alignment commands using the information obtained from the optical sightings. During descent, altitude and velocity information from the LR is used to update inertially derived data. During the coasting descent, lunar stay, and rendezvous phases of the mission, the RR tracks its transponder in the orbiting CSM to provide range, range rate, and antenna angle measurements to the LGC. In addition to functioning as a data processing unit, the LGC, through its flight programs, performs the function of a digital autopilot in controlling the LEM.

1-4.2 STABILIZATION AND CONTROL SYSTEM. The SCS consists of two major sections: the control electronics section (CGS) and the abort guidance section (AGS). The CES processes flight control signals during all mission phases. The AGS provides the CES automatic steering commands, derived from explicit guidance equations, in the event of mission abort due to a PGROS maifunction.

The CES consists of an attitude and translation control assembly (ATCA), a descent eleme control assembly (BCA), rate grow assembly (RGA), two translation controller assemblies (TCA), and two attitude controller assemblies (ACA). The CES processes and routes signals to fire any combination of the 16 thrusters in the RCS to control LEM attitude and translational control inputs originate from any of three sources: the PGNCS during normal automatic operation, the ACA and TCA during manual operations, or the AGS during an abort.

The CES converts the applicable input commands into pulsed or constant level signals and routes them to the RCS to fire the appropriate thrusters. Rate signals from the CES are displayed on the flight director attitude indicator (FDAI).

The CES also processes "ON-OFF" commands for the ascent and descent engines, and routes automatic and manual throttle commands to the descent engine. Trim control of the descent engine insures that the thrust vector operates through the vehicle center of gravity.

The AGS provides abort capability from any point in powered descent or powered acts and increases crew safety by acting as a backup system to the PGNCS. This backup guidance provides vehicle attitude, angular velocity, and translational acceleration indications. The AGS has three main assemblies: abort sensor assembly (ASA), abort electronics assembly, and data entry and display assembly.

The ASA utilizes a strap-down technique employing three single-degree-of-freedom integrating rate gyros and three accelerometers. It is mounted to the PGNCS navigation base on the same mounting pads as the AOT. The outputs of the abort sensor assembly to the abort electronics assembly, a 4,096 word capacity general purpose computer. Computations are performed using the inputs from the abort sensor assembly. When the AGS is in control of the LEM, the results are displayed and control signals are issued to the vehicle's reaction control and propulsion systems.

The abort sensor assembly measures the accelerometer triad rotation from, and sensors the acceleration into, a fixed reference frame. This reference frame is provided by an initial alignment of the AGS with the PGNCS. Initial alignment is required for attitude, velocity, time, and position. Velocity and position vectors are manually entered into the computer by a data entry device available to the astronaut.

Attitude alignment is accomplished by transferring PGNCS IMU gimbal angles to the computer. The abort electronics assembly receives this data from the coupling data unit (CDU) in the same manner and at the same time as the LGC (i.e. incremental angles accumulated from a zero reference after "CDU ZERO").

1-4.3 PROPULSION SYSTEM. The LEM utilizes separate, complete, and independent descent and ascent propulsion systems, which consist basically of a liquid propellant rocket engine and its propellant storage, pressurization, and feed components.

The descent propulsion system is in the LEM descent stage and utilizes a throttlecontrolled, gimbaled engine. The engine injects the LEM into the descent transfer orbit and is used during powered descent and landing to control the rate of descent. The descent engine, developing 10,500 pounds maximum thrust in a vacuum at full throttle and 1,050 pounds minimum thrust, can be gimbaled 6 degrees in any direction. The PGNCS issues the "ON-OFF" commands for the descent engine and also provides signals controlling thrust magnitude and gimbal trim position.

The propellant used in both propulsion systems is a 50-50 fuel mixture of hydrazine unsymmetrical dimethylhydrazine using nitrogen tetroxide as the oxidizer and helium as the tank pressurant.

The ascent propulsion system utilizes a fixed, constant-thrust engine installed along the centerline of the ascent stage midsection and includes the associated propellant feed tanks and pressurization components. The engine develops 3,500 pounds thrust in a vacuum, sufficient to launch the ascent stage from the lunar surface and place it in orbit. The PGNCS issues the "ON-OFF" commands for the ascent engine.

1-4.4 REACTION CONTROL SYSTEM. The RCS provides rocket thrust impulses that stabilize the LEM during descent and ascent and control the LEM attitude and translation about or along all axes. The RCS has 16 thrust chambers supplied by two separate and independent propellant feed and pressurization sections. The thrust chambers are mounted in clusters of four on outriggers equally spaced around the LEM ascent stage. In each cluster, two thrust chambers are mounted on a vertical axis, facing in opposite directions; the other two are spaced 90 degrees apart, parallel to the LEM's Y and Z axes. The RCS utilizes the same fuel as the ascent engine. In the event of RCS fuel depletion, the remaining ascent fuel can be used for the RCS. The RCS can be operated in any of three modes: manual, automatic, or semi-automatic. The PGNCS supplies "ON-OFF" signals through the SCS to the valves on the desired thrust chambers during the automatic or semi-automatic mode. The automatic mode is normally used to provide attitude control during all mission phases except when manual control is required. It is possible to select manual control in one or two axes and retain automatic control in the other axis during all mission phases. The semiautomatic mode combines automatic attitude hold control with manual control. The LEM attitude is changeable about each axis using the astronaut's attitude controller. This mode is used primarily to control the LEM during the rendezvous and docking phase of the mission. In the manual mode, all control commands originate from the attitude controller, including manual control of the thrust duration.

All automatic translational commands originate in the PGNCS and are routed to the RCS similar to the attitude control signals.

1-4.5 ELECTRICAL POWER SYSTEM. The EPS provides 28 vdc and 115 vac, 400 cps power to the PGNCS. This power originates from six batteries, four in the descent stage, and two in the ascent stage. The hatteries, the silver-zinc type, are rated at 80 watts per hour per pound of weight. The 115 vac, 400 cps power is obtained by routing the 28 vdc through an inverter.

1-4.6 ENVIRONMENTAL CONTROL SYSTEM. The ECS sustains life in space hy providing hreatable atmosphere, acceptable temperatures, food and water, and waste disposal. In addition, the ECS circulates an ethylene glycol-water coolant about the temperature sensitive electronic equipment in the PGNCS and other LEM systems to provide thermal stability. The IMU has coolant circulated through its case while the power and servo assembly (PSA), pulse torque assembly (PTA), signal conditioner, LGC and CDU are mounted on coldplates through which the coolant is circulated to provide temperature control.

1-4.7 COMMUNICATIONS AND INSTRUMENTATION SYSTEM. The CIS links the lunar astronauts, the orbiting CSM, and earth monitoring stations.

The communications portion contains two radio frequency (RF) sections, one operating in the VHF range and the other in the UHF range; a television section; and a signal processing section. In addition to two-way voice communication, the RF section receives and transmits tracking and range information, hiomedical information, and emergency code keying in the event of voice transmission failure. The television section is used by the extravehicular astronaut to televise the lunar surface within an eighty foot radius of the grounded LEM. In the signal processing section, critical signals of the PGNCS are conditioned and supplied to pulse code modulated (PCM) telemetry equipment for transmission to earth. Telemetry data can he stored when direct communication with the earth is not possible.

The instrumentation portion provides the astronauts and ground facilities with LEM performance data during the mission by sensing physical status data, monitoring the various systems, and performing inflight and lunar surface checkout. This system also contains the scientific instruments which are used by the astronauts during their lunar stay.

#### 1-5 PGNCS INTERFACE

PGNCS operation during the LEM mission requires the interface of the PGNCS with the other LEM systems, the displays and controls on the crew display and control panels, the RR, the LR, and the astronauts. The functional interface of the PGNCS is shown in figure 1-5.

1-10

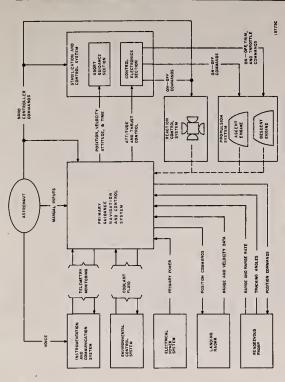


Figure 1-5. LEM PGNCS Functional Interface, Block Diagram

1-5.1 SYSTEMS. Four LEM systems (SCS, ECS, CIS, and EPS) have direct interface with the PGNCS and two systems (propulsion system and RCS) have indirect interface of the propulsion system and the RCS occurs through the SCS. These two systems may thus be controlled by the PGNCS or by the backup control provided by the AGS of the SCS. Descriptions and sources of the SCS interface signals are provided in table 1-1. Descriptions of the interfaces with the other systems are provided in paragraph 1-4.

1-5.2 DISPLAYS AND CONTROLS. Several displays and controls located on the crew control panels, LGC display and keyboard (DSKY) panel, and the SCS control panel interface with the PGNCS. Two sets of hand controllers are provided for manual control of the LEM and interface with the PGNCS, Descriptions of the displays and controls are in table 1-10.

1-5.3 LANDING RADAR. The landing radar (LR) provides data to the LGC from which LEM velocity (in antenna coordinates) and LEM altitude may be determined. The data is also available for visual display, independent of the PGNCS, except that the velocity is in spacecraft coordinates.

The landing radar which operates in the X-band, consists of an antenna assembly, a solid-state electronics assembly, and a control panel. Velocity data is acquired from a three beam continuous wave Doppler radar. Altitude data is provided by a one beam FM continuous wave radar altimeter. The antenna assembly accommodates the requirements of both the Doppler and the altimeter beams.

Landing radar and PGNCS interface include digital data transfer, scaling, velocity and range sensing, status, and antenna positioning. Descriptions and sources of the interface signals are in table 1-III.

1-5.4 RENDEZVOUS RADAR/TRANSPONDER. The rendezvous radar/transponder (RR/T) provides range, range rate, and angle data to the LGC to enable computation of a trajectory from the moon to a point in space where the final docking of the LEM to the CSM can begin. Outputs from the RR are also available for visual display.

When the LEM is on the lunar surface, the RR tracks the associated transponder in the CSM to furnish updated information to the LGC. During the LEM ascent coasting phases, the RR is used for monitoring or midcourse correction maneuvers. During automatic operation of the RR, the RR is controlled by inputs from the LGC. The astronauts can manually control! the RR with controls and indicators located on the radar panel of the commander's lower console.

The RR consists of an antenna assembly and an electronics assembly. The antenna assembly contains the microwave radiating and gimballing elements and internally mounted syros. resolvers, multiplier chains, modulators, and mixer preamplifiers.

The antenna is a four horn, amplitude comparison, monopulse type which uses a Cassegrainian configuration to minimize the total antenna depth. Components are distributed inside the antenna to achieve balance around each axis. Each axis (shaft and trumnion) is controlled by a brushless serve motor driven by pulse width modulated drive signals. The antenna transmits and receives circular polarized radiation to minimize signal variations resulting from attitude changes of the linearly polarized transponder antenna.

Four rate integrating gyros are used for line of sight (LOS) space stabilization and LOS angle rate measurement. Only two of the gyros are used at any one time; if either of the two gyros fail, a logic circuit transfers control to the other two gyros. A two speed resolver is mounted on each axis for antenna angle data required by the LGC and for display. The multiplier chain supplies X-band power for radiation and for local oscillator excitation. The modulator provides phase modulation of the X-band carrier.

The electronics assembly contains the antenna control amplifiers, range tracker, frequency tracker, frequency synthesizer, receiver, and signal data converter.

Shaft and trunnion positioning signals from the CDU are converted into dc error signals by the antenna control amplifiers. The dc error signals are used to torque the antenna gyros and produce gyro output error signals. The gyro error signals cause the antenna servo loop to drive the antenna to the commanded positions.

The range tracker operates with the transponder and uses a multitone ranging system. The RR transmission is phase modulated with sine wave, 200 cps, 6.4 kc, and 204.8 kc tones. By comparing the phase of the received 200 cps tone with the transmitted 200 cps tone, range measurements from 0 to 390 miles can be made. Similar phase comparisons made with the 6.4 and 204.8 kc tones provide successive refinements of ranging accuracy. The lower frequency tone is used for coarse range extraction; the higher frequency tones provide fine range data.

The frequency tracker nulls through the band of expected received Doppler frequencies and provides an output which represents range rate.

The frequency synthesizer generates all of the fixed frequencies required for coherent signal transmission and reception. A single 1.7 mc stable crystal oscillator and a system of multiplication, division, and mixing is used to produce the required frequencies.

The receiver is a highly stable, three channel, triple conversion superheterodyne. Two channels are provided for the shaft and trunnion signals and one channel is provided to amplify the sum or reference signal.

The signal data converter provides the interfaces between the RR and the LGC. The signal data converter contains a computer interface unit and an input-output amplifier. The computer interface unit processes the radar output signals into the format required by the LGC. The processed signals are then selected sequentially for transfer to the LGC by coded strobe signals provided by the LGC. Control and status discretes are routed to the LGC through the input-output amplifier. The input-output amplifier also routes control and status signals to and from the LEM controls and displays.

The transponder consists essentially of a triggered frequency-shifting transmitter. The purpose of the transponder is to extend the range of the low power radar by decreasing losses.

Table 1-I. SCS Interface Signals

Signal Name	Source	Description
Manual translation commands (±x, ±y, ±z)	scs	Signals from translation controller which fire RCS jets by LGC control.
Attitude control out of detent	scs	Signal from attitude controller indicating that it is not in neutral position.
Rate of descent (±)	SCS	Discretes commanding an increase or decrease in rate of descent.
Gimbal off (pitch, roll)	SCS	Signal to LGC indicating that descent engine pitch or roll gimbal is off null.
Trim commands (± pitch, ± roll)	LGC	Signals which control trim of descent engine.
Engine on-off	LGC	Signal to turn descent or ascent engine on or off.
Descent engine throttle command (decrease, increase)	LGC	Signal to increase or decrease thrust of descent engine.
RCS jets on-off	LGC	Signals (16) to turn RCS jets on or off.
Increments of IMU gimbal angles $(\pm \triangle \theta 1G, \pm \triangle \theta MG, \pm \triangle \theta GG)$	LGC	Supplies changes in 1MU gimbal angles to AGS.
CDU zero (initial clear)	LGC	Sets alignment logic of AGS to zero.
800 cps ±1%	PGNCS	Provides reference between PGNCS and SCS.

Table 1-II. Displays and Controls

Display or Control	Function		
GUID CONT switch	Selects either primary guidance (PGNS) or abort guidance (AGS). Normally in the PGNS position.		
MODE SEL selector	Three position switch used during landing phase to select one of three inputs to be displayed on AZ RT/ELEV RT-LAT VEL/FWD VEL indicator. Inputs are landing radar (LDG RADAR), PGNS and AGS.		
RNG/ALT MON switch	Controls display of RANGE/RANGE RATE-ALT/ ALT RATE indicator. Positions are RNG/RNG RT and ALT/ALT RT.		
RATE/ERR MONITOR switch (2)	Selects one of two inputs for AZ RT/ELEV RT-LAT VEL/FWD VEL indicator and attitude needles of FDAI.		
ATTITUDE MON switch (2)	Selects one of two inputs to FDAI total attitude dis- play and attitude error needles during landing.		
THR CONT switch	Selects either automatic (AUTO) or manual (MAN) control of descent engine throttle. Normally in AUTO position.		
MAN THROT switch	Activates either commander's (CDR) or system engineer's (SE) translation controller for manual throttling of descent engine.		
ABORT	Pushbutton to cause mission abort at any point be- tween LEM/CSM separation and touchdown on lunar surface with descent stage still attached.		
ABORT STAGE	Pushbutton to cause mission abort using ascent stage.		
AZ RT/ELEV RT- LAT VEL/FWD VEL meter (2)	Provides visual displays of vehicle forward and lateral velocity during landing.		

(Sheet 1 of 2)

Table 1-II. Displays and Controls

Display or Control	Function		
RANGE/RANGE RATE- ALT/ALT RATE meter	Provides visual displays of range, altitude, range rate, and altitude rate.		
FDAI meter (2)	Provides three visual displays, total attitude, atti- tude error, and attitude change rate. PGNCS or AGS provides inputs for total attitude and attitude error. Attitude rate signals are provided by SCS rate gyros.		
LGC and ISS warning indicators, PGNS caution indicator.	Controlled by instrumentation system which receives discretes from LGC when certain PGNCS troubles exist.		
MODE CONTROL selector	A three-position selector located on SCS control panel concerned with attitude control. Positions are OFF, ATT HOLD, and AUTO. In AUTO position, fully automatic attitude control is achieved through PGNCS or AGS control of RCS jets. ATT HOLD position allows crew to manually reposition LEM and have new position automatically maintained by LGC.		
IMU CAGE switch	Switch located on DSKY mounting panel to drive IMU gimbal angles to zero.		
Attitude controller (2)	Three-axis, pistol-grip, right-hand device for manual attitude control of LEM. Outputs from controller are processed by PGNCS or may be routed directly to RCS.		
Translation controller (2)	Three-axis, T-handle, left-hand device for manual translation control of LEM. Using switch located next to T-handle, controller can operate RCS jets or throttle the descent engine.		

(Sheet 2 of 2)

Table 1-III. Description of Landing Radar Interface Signals

Signal Name	Source	Description
Antenna positioning command	DSKY and LGC	Changes antenna position.
Antenna position #1 (descent)	LR	Indicates to LGC that antenna is in position #1.
Antenna position #2 (hover)	LR	Indicates to LGC that antenna is in position #2.
Velocity data good	LR	Indicates to LGC that LR velocity trackers bave locked on.
Range data good	LR	Indicates to LGC that LR range trackers have locked on.
Range low scale factor	LR	Indicates to LGC that a change in scale factor is necessary. Issued automatically at approximately 2,500 feet.
LR in "0" and LR in "1"	LR	Digital pulses sent to LGC which contain range and velocity data.
Readout command	LGC	Indicates that LGC is ready to receive LR data pulses.
Gate reset	LGC	3,200 cps continuous LGC output to reset LR transfer gates.
Range strobe	LGC	Timing pulses to enable LR transfer gates.
V <sub>xa</sub> , V <sub>ya</sub> , V <sub>za</sub> strobe pulses	LGC	Timing pulses to enable LR transfer gates.

Table I-IV. Description of Rendezvous Radar Interface Signals

Signal Name	Source	Description
Antenna shaft angle	RR	Sine and cosine of 1X and 16X shaft angle resolvers.
Antenna shaft command	CDU	Torquing signal from LGC via CDU which changes position of antenna shaft.
Antenna trunnion angle	RR	Sine and cosine of 1X and 16X trunnion angle resolvers.
Antenna trunnion command	CDU	Torquing signal from LGC via CDU which changes position of antenna trunnion.
RR data good	RR	Digital pulses to LGC to indicate that RR is locked on and data is good.
RR in "0" and RR in "1."	RR	Digital pulses to LGC which contain range and range rate data.
Range gate and range rate gate	LGC	Timing pulses to enable RR trans- fer gates.
Radar gate reset	LGC	Reset pulses for gates.
Counter readout command	LGC	Fifteen pulses from LGC which read out contents of RR output shift register.
Power on and in auto LGC mode	RR	Pulses to indicate RR is on and in auto mode.
RR auto track enable	LGC	Allows RR to lock on return signal.
RR range low scale	RR	Scaling of data has changed to low scaling.



### Chapter 2

## SYSTEM AND SUBSYSTEM FUNCTIONAL ANALYSIS

#### 2-1 SCOPE

This chapter provides functional descriptions of the PGNCS and its subsystems. This chapter describes how the PGNCS subsystems perform the PGNCS operations.

# 2-2 PRIMARY GUIDANCE, NAVIGATION, AND CONTROL SYSTEM.

The PGNCS is functionally divided into three major subsystems: inertial, optical, and computer. The PGNCS performs three basic functions: inertial guidance, navigation, and autopilot stabilization and control. Within these functions the subsystems, or combination of subsystems, with assistance from the astronaut, perform the following operations:

- (1) Establish an inertial reference which is used for measurements and computations.
- (2) Aligns the inertial reference by optical measurements and, through interface, aligns the inertial reference with the CSM PGNCS.
  - (3) Calculates the position and velocity of the LEM by inertial navigation.
- (4) Accomplishes a LEM and CSM rendezvous by radar tracking, optical navigation, and inertial guidance.
- (5) Generate attitude control and thrust commands to maintain the LEM on a satisfactory trajectory.
  - (6) Control throttling of descent engine during lunar landing.
  - (7) Display pertinent data related to guidance status.
  - (8) Controls ascent engine hurn time to obtain proper velocity for rendezvous orbit.

To perform its inertial guidance functions, the PGNCS employs an IMU containing accelerometers mounted on a gyro stabilized, gimbal-mounted platform (stable member). The IMU, three channels of the CDU, the pulse torque assembly (PTA), and the PSA form the ISS of the PGNCS.

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To perform its navigational functions, the PGNCS employs the AOT, the LR, and the RR. The AOT provides a means of manually taking direct visual sightings and precision angular measurements of preselected celestial targets. During the powered descent and landing phases, the PGNCS receives altitude and velocity data from the LR, which is used to update or check inertially derived data. During the coasting descent, lunar stay, and rendezvous phases, the RR tracks its transponder in the orbiting CSM to provide range, range rate, and antenna angle measurements to the LGC.

The LGC is a digital computer which serves as both the control element and the primary data processing element of the PGNCS. The LGC and the display and keyboard (DSKY) form the computer subsystem of the PGNCS.

Figure 2-1 illustrates the signal flow and interface between the PGNCS subsystems and navigational aids.

2-3 LEM AND PGNCS AXES

Several sets of axes are associated with the LEM and PGNCS. Figure 2-2 illustrates these various orthogonal sets which are defined in the following paragraphs. Positive rotation about each axis is as defined by the right hand rule.

2-3.1 LEM SPACECRAFT AXES. The LEM spacecraft axes provide a reference for all other sets of axes and define the point about which attitude maneuvers are performed. The LEM spacecraft axes, designated X<sub>LEM</sub>, Y<sub>LEM</sub>, Z<sub>LEM</sub>, are referred to as the yaw, pitch, and roll axes respectively. The X<sub>LEM</sub> axis points through the upper docking hatch and the Z<sub>LEM</sub> axis points through the forward hatch. The Y<sub>LEM</sub> axis perpendicular to the X<sub>LEM</sub> and the Z<sub>LEM</sub> axes and can be considered to be pointing out of the astronaut's right shoulder as hefaces toward the forward portion of the LEM.

2-3.2 NAVIGATION BASE AXES. The navigation hase provides a precise alignment of the IMU to the AOT and the ASA and a means of attaching all three units to the spaceraft. The navigation hase is mounted to the LEM structure so that a coordinate reference system is formed by its mounting points. The YNB axis is defined by the centers of the two upper mounting points and is parallel to the YLEM axis. The XNB axis is defined by a line through the center of the lower mounting point, perpendicular to the YNB axis and parallel to the XLEM axis. The ZNB axis is mutually perpendicular to the XNB and YNB axes and is parallel to the ZLEM axis.

2-3.3 INERTIAL AXES. The inertial axes provide references for measuring changes in velocity and attitude. At zero gimbal angles, the inertial axes are parallel to the navigation base axes.

2-3.3.1 Gimbal Axes. The gimbal axes (outer, middle, and inner) are the axes of the movable gimbals. The axes are defined by the intergimbal assemblies which provide each gimbal with rotational freedom. The attitude of the spacecraft with respect to the stable member is measured by the gimbal resolvers located in the intergimbal assemblies.

2-3.3.2 Stable Member Axes. The stable member axes (XSM, YSM, ZSM) provide a reference for aligning the inertial components and for defining the angular orientation of the inertial axes during flight.

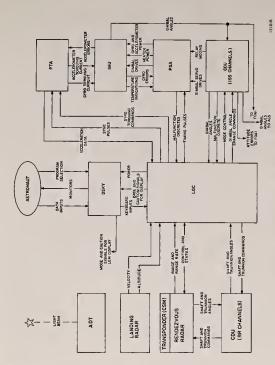


Figure 2-1. PGNCS Internal Interface, Block Diagram

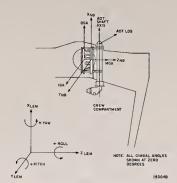


Figure 2-2, LEM and PGNCS Axes

2-3.3.3 <u>Accelerometer Axes.</u> The accelerometer axes  $(X_a, Y_a, Z_a)$  are the positive input axes of the accelerometers and are parallel to the stable member axes. Velocity changes are measured along the accelerometer input axes. This velocity data is used to determine spacecraft position and velocity.

2-3.3.4 Gyro Axes. The gyro axes  $(X_p, Y_g, Z_g)$  are the positive input axes of the stabilization gyros and are parallel to the stable member axes. If the attitude of the stable member is changed with respect to inertial space, the gyro senses the change about its input axis and provides an error signal to a servo loop which realigns the stable member to its original orientation.

## 2-4 INERTIAL SUBSYSTEM

The ISS performs three major functions. It measures changes in LEM attitude, assists in generating steering commands, and measures spacecraft velocity due to thrust. To accomplish these functions, the IMU provides an inertial reference consisting of a stable member with a three degree of freedom gimbal system and stabilized by

three rate integrating gyros. Each time the inertial subsystem is energized, the stable member must be aligned with respect to a predetermined reference. During flight and prior to launch from the lunar surface, this alignment is accomplished by sighting the optical instrument on celestial objects.

Once the ISS is energized and aligned, any rotational motion of the LEM will be about the stable member, which remains fixed in space. Resolvers mounted on the gimbal axes act as angular sensing devices and measure the attitude of the LEM with respect to the stable member. These angular measurements are displayed by the FDAI and angular changes are sent to the LGC via the CDU.

The desired LEM attitude is calculated in the LGC and compared with the actual gimbal angles. Any difference between the actual and calculated angles results in the generation of attitude error signals by the ISSchannels of the CDU which are sent to the FDAI for display.

Vehicle acceleration is sensed by three pendulous accelerometers mounted on the stable member with their input axes orthogonal. The signals from the accelerometers are supplied to the LGC which calculates the total vehicle velocity.

The modes of operation of the inertial subsystem can be initiated automatically by the LGC or by the astronaut selecting computer programs through the DSKY. The status or mode of operation is displayed on the DSKY.

For purposes of explanation and description, the ISS is divided into functional blocks as shown in figure 2-3 and described in the following paragraphs.

2-4.1 STABILIZATION LOOP. The three stabilization loops (figure 2-4) maintain the stable member in a specific spatial orientation so that three mutually perpendicular 16 pulsed integrating pendulum (16 PIP) accelerometers can measure the proper components of LEM acceleration with respect to the coordinate system established by the stable member orientation. An input to the stabilization loops is created by any change in LEM attitude with respect to the spatial orientation of the stable member, Because of gimbal friction and unbalances, motion of the LEM structure relative to the stable member will produce a torque on the stable member whill tend to change its orientation. This change is sensed by the stabilization gyros. When the gyros sense an input, they issue error signals which are amplified, resolved, if necessary, into appropriate components, and applied to the gimbal torque motors. The gimbal torque motors then drive the gimbals until the stable member regains its original spatial orientation.

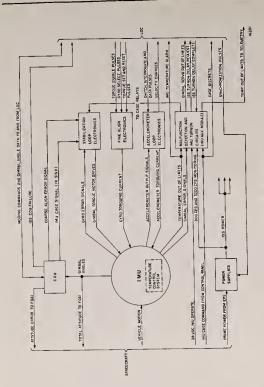


Figure 2-3, ISS, Block Diagram

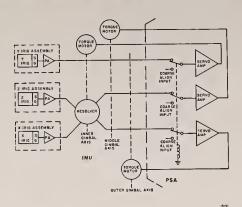


Figure 2-4. Stabilization Loop, Block Diagram

The stabilization toop consists of three pre-aligned Apollo II inertial reference integrating gyro (Apollo II IRIG) assemblies, a gyro error resolver, three gimbal servo amplifiers, three gimbal torque motors, three gimbals, and circuitry associated with these components. The inner gimbal is the stable member upon which the three stabilization gyros are mounted. The gyros are mounted with their input axes oriented in an orthogonal configuration. Movement of any gimbal tends to result in a movement of the stable member and rotation about the input axes of one or more of the stabilization gyros.

The stabilization loop contains three parallel channels. Each channel starts with a motor drives the glimbal resulting in a movement of the stable member and a movement of the stable member and a movement of the stable member and a movement of the stable member shade a movement of the IMU support glimbal attempts to displace the stable member from its erected position, one or more of the stablization gyros senses the movement and issues error signals. The phase and magnitude of the 3,200 cps gyro error signal represents the direction and amount of rotation experienced by the gyro about its input axis. The error signal is fed from the gyro signal

generator ducosyn to the associated IRIG preamplifier, which is a part of the prealigned Apollo II IRIG assembly, Amplification of the error signal is required to achieve a high signal-to-noise ratio through the gimbal slip rings.

The amplified gyroerror signals also represent motion of the stable member about its axis since the stable member axes (XSM, YSM, ZSM) and the gyro axes (Xg, Yg, Zg) are parallel to one another. \* If the middle and outer gimbal axes remain parallel with the stable member axes, then movement of the outer gimbal (a yaw movement of the LEM) is sensed by only the X gyro and movement of the middle gimbal (roll movement of the LEM) is sensed by only the Z gyro. Movement of the stable member about the inner gimbal axis (YSM), however, changes the relationship of the X and Z gyro input axes to the outer and middle gimbal axes. As a result, a movement of the middle or the outer gimbal is sensed by both X and Z gyros. The input required by the gimbal servo amplifiers to drive the gimbals and move the stable member back to its original position must be composed of components of both the X and Z gyros. The required gimbal error signals are developed by the gyro error resolver. The gyro error signals, E(Xg) and E(Zg), are applied to the stator windings of the gyro error resolver. The rotor windings are connected to the inputs of the outer and middle gimbal servo amplifiers. Movement of the stable member about the inner gimbal axis (pitch movement of the LEM) changes the position of the resolver rotor relative to the resolver stator. This change corresponds electromagnetically to the change in the relationship of the stable member axes to the outer and middle gimbal axes. The outputs taken from the rotor are the required middle and outer gimbal error signals (Emg and Eog). Since the inner gimbal torque motor axis and the Y axis of the stable member are the same axis, the Y gyro error signal, E(Yg), is equal to the inner gimbal error signal, (Eig), and is fed directly to the inner gimbal servo amplifier.

The three identical gimbal servo amplifier modules are located in the PSA and contain a phase sensitive demodulator, a filter, and a de operational power amplifier. The phase sensitive demodulator converts either the 3, 200 cps gimbal error or 800 cps coarse align error, zero or pl phase, signals into a representative positive or negative de signal. The de signal is filtered and applied to a de operational amplifier with current feedback. The compensation network in the feedback circuit of the amplifier controls the response characteristics of the entire stabilization loop. The output of the de amplifier has an operating range between +28 vdc and -28 vdc and drives the respective gimbal torque motor directly in either angular direction.

The gain required for each stabilization loop differs. This difference compensates for the differences in gimbal inertia. The proper gain is selected by the connections to the gimbal servo amplifier module. A single torque motor is mounted on each gimbal at the positive end of the gimbal axis. The torque motors drive the gimbals to complete the stabilization loop.

<sup>\*</sup> The Z gyro has its positive input axis aligned to the -Z<sub>SM</sub> axis but this is compensated for by reversing the polarity of the 3, 200 ops excitation to the primary winding of the Z gyro signal generator ducosyn which causes the Z gyro error signal to be representative of the direction and amount of motion about the Z<sub>SM</sub> axis.

The orientation of the stable member can be changed in either the coarse align, fine align, or IMU cage modes. Signals to reposition the gimbals are injected into the gimbal servo amplifiers from the CDU during the coarse align and IMU cage modes and into the stabilization gyros from the fine align electronics during the fine align mode. During the IMU cage mode and the coarse align mode, the reference signal for the demodulator in the gimbal servo amplifier is externally switched from 3, 200 cps to 800 cps.

2-4.2 FINE ALIGN ELECTRONICS. The fine align electronics (figure 2-5) provides torquing current to the stabilization gyros to change the orientation of the IMU gimbals during the fine align mode. The operation of the fine align electronics is controlled by the LGC.

The components of the fine align electronics are common to the three stabilization gross one at a time on a time shared basis. The fine align electronics consists of a gyro calibration module, a binary current switch module, and a dc differential amplifier and precision voltage reference module, all located in the PTA.

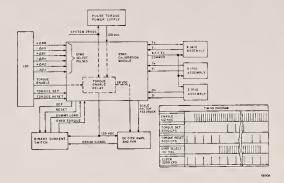


Figure 2-5. Fine Align Electronics - Computer Inputs

The fine align electronics is enabled and controlled by LCC inputs to the gyro calibration module. The LCC inputs consist of torque enable pulses, gyro select pulses, a torque set command, and a torque reset command. The fine align electronics is enabled by the torque enable pulses. The torque enable pulses are a train of pulses three microseconds in width and occurring at 102.4 kpps. The torque enable pulses are applied through a relay driver to energize the torque enable relay in the calibration module. When the torque enable relay is energized, system 28 vod is applied to the precision voltage reference (PVR) and regulated 120vde from the pulse torque power supply is applied to the dc differential amplifier and the binary current switch. The torque enable pulse train is received 20 milliseconds prior to any gyro set command.

The gyro to be torqued and the direction it is to be torqued is selected by the LGC by sending gyro select pulses to one of the six 'A6por - A6 injunts. (See figure 2-6.) The gyro select pulse consists of a train of pulses three microseconds in width and occurring at 102.4 kpps. The pulse train activates a transistor switch network which controls current through the T+ or T- coils of the torque generator ducosyn in the gyro selected. The gyro select pulse train is received 312.5 microseconds (one LGC clock time at 3,200 pps) prior to any torque set command.

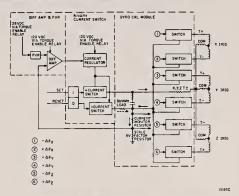


Figure 2-6. Fine Align Electronics - Gyro Selection

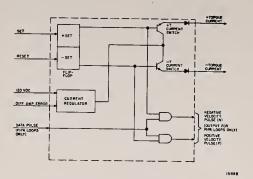
The torque set and reset commands are 3,200 pps pulse trains containing pulses that are three microseconds in width. A 3,200 pps pulse train will be present on the torque set line when any gyro is to be torqued. A 3,200 pps pulse train is present on the torque reset line at all other times. This ensures that the binary current switch is in the reset condition prior to receipt of a torque enable command from the LGC. When the gyro has been torqued the proper amount, a torque reset command is issued which causes the torque current to be cut off. The gyro select pulse train will be removed 312.5 microseconds after the torque reset command has been issued. The torque set and torque reset pulses are fed through a 1:2 step-up transformer in the calibration module to the set and reset inputs of the binary current switch.

The torque current from the binary current switch is applied through a tuned reststive-capacitive compensation network in the calibration module to make the torque generator ducosynwindings appear as a pure resistive load to the binary current switch. The torque current to the gyros is via the Tz(common) line. Current will flow only through the selected torque generator coils, the current monitor resistor, and the scale factor resistor. The voltage drop developed across the scale factor resistor is used as a feedback to the differential amplifier to regulate the torquing current. The voltage drop across the current monitor resistor is applied to PTA test points for external monitoring of gyro torque current.

When no gyro is being torqued, the binary current switch provides current flow through a dummy load resistor and through the current monitor and scale factor resistors. In this manner, the binary current switch maintains a continuous flow of torque current. The dummy load resistor simulates the impedance of the torque generator coil and a compensation network.

The torque set and torque reset pulses trigger a flip-flop (bi-stable multivibrator) in the binary current switch (figure 2-7), if the flip-flop is in the \*set condition, the \*set condition will remain until a reset command resets the flip-flop. The outputs of the flip-flop control two transistor switches. If the flip-flop is in the \*set condition, the \*set output is present at the base of the \*torque current switch, causing the switch to turn on. The \*torque current switch closes the path from the 120 volt supply through the current regulator to the proper T+ or T- winding of the selected gyro via the calibration module. If the flip-flop is in the \*set condition, the \*torque current switch will turn on and close the current path through the dummy load resistor.

The binary current switch used in the fine align electronics is identical to the one used in the accelerometer loops. The portion of the binary current switch used only for the accelerometer loop is disabled in the fine align electronics application. In the accelerometer Ioop application, current to the accelerometer T+ torque generator coil is provided by the +torque current switch and current to the T+ torque generator coil is provided by the -torque current switch. Therefore, the +torque and -torque designations of the switches have significance. In the fine align electronics application the switch designations have no significance since current to both the T+ and T- coils of the gyro torque generators is provided by the +torque current switch while the -torque current switch provides only the dummy load current.



Flgure 2-7. Binary Current Switch

The dc differential amplifier and PVR module (figure 2-8) maintains the current through the windings of the torque generator ducosyn at 84 milliamperes. The PVR is supplied with regulated 28 vdc and, through the use of zener diode circuits, developes an accurate 6 vdc for use as a reference voltage. The scale factor resistor in the calibration module also has 6 volts developed across it when 84 milliamperes of current flows through it. A comparison is made by the dc differential amplifier of the PVR 6 volts and the scale factor resistor 6 volts. Any deviation from the nominal 84 milliamperes of torquing current will increase or decrease the voltage developed across the scale factor resistor and cause an output error signal from the dc differential amplifier. This error signal controls the current regulator in the binary current switch. The current regulator, which is in series with the torque generator coils of the selected gyro and the 120 vdc source, will maintain the torquing current at 84 milliamperes.

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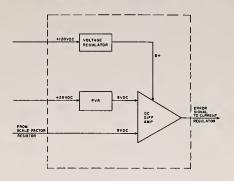


Figure 2-8. DC Differential Amplifier and Precision Voltage Reference

The current flow through the windings of the torque generator ducosyn causes the gyro float to rotate about the gyro's output axis.  $A+\Delta\theta$  gyro select command from the LGC will allow torque current to flow through a T- torque generator coil which results in a positive rotation of the gyro float about the output axis.  $A-\Delta\theta$  gyro select command produces a negative float rotation. Float rotation results in an error output from the signal generator ducosyn. The error signal is applied to the stabilization loop to reposition the gimbals and the stable member. The change in gimbal angles is transmitted by the CDU read counters to the LGC

<sup>\*</sup> The positive input axis of the Z gyro is aligned to the  $^{-2}$ SM axis but this is compensated for by reversing the T+ and T- connections to the Z gyro torque generator ducosyn. A  $^{+}$ A $^{-2}$ Z gyro-select command from LGC will cause a negative float rotation but since the polarity of the Z gyro signal generator is also reversed the gyro error signal will appear to represent a positive float rotation. The stabilization loops will then drive the gimbals in the desired direction.

2-4.3 ACCELEROMETER LOOP. The three accelerometer loops measure the acceleration of the stable member along three mutually perpendicular axes and integrate this data to determine velocity. The velocity is used by the LGC to determine the LEM velocity vector, Figure 2-9 is a functional diagram of an accelerometer loop.

The three accelerometer loops contain three prealigned 16 PIP assemblies, three PIP preamplifiers, three ac differential amplifier and interrogator modules, three binary current switches, three calibration modules, three differential amplifier and precision voltage reference modules, a pulse torque isolation transformer, and associated electronics.

The three mutually perpendicular PIP's are acceleration sensitive devices. When fixed in its associated accelerometer loop, the PIP becomes an integrating accelerometer. The PIP is basically a pendulum-type device consisting of a cylinder with a penduluous mass unbalance (penduluous float) pivoted with respect to a case. The axis of the pivots defines the PIP output axis. A signal generator is located at the positive end of the output axis to provide electrical output signals indicative of the rotational position of the float. A torque generator located at the other end of the float acts as a transducer to convert electrical signals into mechanical torque about the float shaft. The accelerometer loop using a PIP is mechanized to operate in a binary (two state) mode.

In the binary mode, the PIP pendulum is continually kept in an oscillatory motion. Thus the two states: positive rotation or negative rotation. The rotation is accomplished by continuously routing torquing current through the torque generator plus or minus windings.

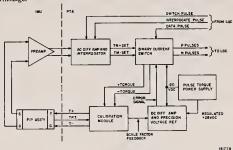


Figure 2-9. Accelerometer Loop

The torque generator has two windings, one to produce torque (rotation) in a positive direction, the other to produce torque (rotation) in a negative direction. Only one winding will have current in it at anyone time. The torque winding selection is accomplished by the setting of a flip-flop in the bluary current switch (figure 2-7). When the loop is first energized, the interrogator sets the flip-flop to route the torquing current to one of the windings, which will rotate the float to null. As the float passes through null, the phase of the output signal of the signal generator changes, which causes the interrogator to issue pulses to reset the flip-flop in the binary current switch and thus route torquing current to the other torque winding. The float is then torqued in the opposite direction until the signal generator output again changes phase as the float passes through null which reinstates the cycle.

The output of the signal generator, after being amplified by the PIP preamplifier is interrogated 3200 times a second by the interrogate pulse. The binary current switch flip-flop can be reset only when the interrogate pulse is present and the signal generator output is of the proper phase.

The PIP pendulum motion is an oscillatory motion about its null point and can be measured in cycles per second. As is characteristic of every electro-mechanical loop, there exists some natural resonant frequency. The natural frequency is dependent upon float damping, signal and torque generator sensitivities, and other loop characteristics. In the case of the accelerometer loop this natural frequency is approximately 500 cps, and the pendulum oscillates at a frequency close to that. At a torque winding selection rate of 3200 pulses per second, the value of this frequency can be any value equal to  $3200 \pm x$  where x is any even number.

Using the above ratio, it is possible for the pendulum to have a maximum frequency of 1600 cps (x equals 2). A frequency of 1600 cps means that for every torque selection pulse, the torque current would be routed to the opposite torque generator winding. Solving the equation  $f=3200 \div x$ , the frequency closest to 500 is 533-1/3. In this case; the value of x is six. Thus one complete pendulum cycle will occur during six torque selection pulses. Dividing the time for the six pulses into positive and negative rotations, it is seen that the PIP functions in a 3-3 mode (positive rotation for three torque selection pulses, negative rotation for the selection pulses, negative rotation for three torque selection pulses, negative rotation for three torque selection pulses

The physical configuration of the PIP is such that the float, when moding in its 3-3 state and sensing no acceleration, rotates an equal angular distance on both sides of an electrical and mechanical null.

The 2 voltrms, 3200 cps, one phase signal generator excitation voltage is synchronized with the LGC clock. The signal generator has a center tapped secondary winding which provides a double ended output, one side having a zero phase reference with respect to the 3,200 cps excitation and the other side a pi phase reference. The center tap is connected to ground. The output signal is representative of the magnitude and direction of the rotation of the pendulous float about the output axis. The error signal is then routed to the preamplifier mounted on the stable member. The phase of the output signal from the preamplifiers at stable member. The phase of the output signal from the preamplifier are applied as separate imputs to the ac differential amplifier and further amplified. The two signals are then sent to the interrogator.

The ac differential amplifier and the interrogator are packaged in the same module which is located in the pulse torque assembly (PTA) (figure 2-10). The interrogator analyzes the ac differential amplifier outputs to determine the direction of the 16 PIP float movement and generates appropriate torquing commands. The two amplified signals from the ac differential amplifier go to two summing networks and threshold amplifiers (represented in figure 2-10 by AND gates). Interrogate pulses (IP) are continuously being received by the interrogator from the LGC. An interrogate pulse is a two microsecond pulse occurring at 3,200 pps and timed to occur 135 degrees after the positive going zero crossing of the reference excitation. (See figure 2-11.) With this phasing, the interrogate pulse occurs at the 90 degree peaks of the phase shifted zero or pi phase input signals from the PIP preamplifiers. The interrogate pulse occurs at a positive 90 degree peak of the zero phase signal if the float angle is positive and at a positive 90 degree peak of the pi phase signal if the float angle is negative. The zero and pi phase signals and the interrogate pulses are ANDed by the summing network and threshold amplifier. The gated outputs of the threshold amplifier are applied to a flip-flop as set or reset pulses. If the flip-flop is in the +set condition, a succession of set pulses will maintain the +set condition. The +set condition will remain until the float angle passes through null. At this time, a reset pulse is produced to cause the flip-flop to go to the -set condition.

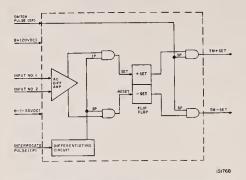


Figure 2-10. AC Differential Amplifier and Interrogator Module

The outputs of the flip-flop are applied to two AND gates which are also driven by switch pulses received from the LGC. The switch pulses are a train of clock driven 3,200 pps pulses three microseconds in width, timed to occur three microseconds after the leading edge of the interrogate pulse. The flip-flop enables only one output gate at any switch pulse time. The outputs of the AND gates are called the TM + set pulse and the TM - set pulse.

The binary current switch (figure 2-7) utilizes the TM+set and TM-set outputs of the interrogator to generate 16 PIP torquing current. The TM+set and the TM-set pulses (urnish the input to a flip-flop. If the flip-flop is in the +set condition will persist until the float angle passes through null. The phase change will cause the flip-flop of the ac differential amplifier and interrogator module to reset to the -set condition. At this time a TM-set pulse is developed and causes the binary current switch flip-flop to go to the -set condition. The outputs of the flip-flop control two transistor current switches. If the flip-flop is in the +set condition, the +set output will be at the base of the +torque current switch and will turn it on. The +torque current switch closes the path from the current regulated 120 vdc supply through the PIPA calibration module to the 16 PIP T torque generator coils. If the flip-flop is in the -set condition, the -torque current switch will be turned on, closing the path through the T- torque generator coils.

An acceleration along the PIP input axis causes the pendulous mass to produce a torque which tends to rotate the float about the output axis. The torque produced by the acceleration is proportional to the magnitude of the acceleration. The acceleration produced torque aids and opposes the torque generator forces causing changes in the time required for the float to be torqued back through mill. A change in velocity  $(\Delta V)$  is the product of acceleration and incremental time  $(\Delta t)$ , the torque is actually proportional to an incremental change in velocity  $(\Delta V)$ .

$$T_{ACCEL} = K_1 a \Delta t = K_1 \Delta V$$

The float is already in motion due to loop torquing, therefore additional torque is required to overcome the acceleration torque and to keep the pendulum in its oscillatory motion. The additional torque is obtained by supplying torquing current for additional time through one of the torque windings. The current at any one time is a constant, therefore the current must be present for a longer period of time. Thus to determine the amount of acceleration sensed by the PIP, it is necessary only to measure the length of time torquing current is applied to each torque winding.

$$ACCEL_{IND} = K_2 \Sigma \left[ (T+) - (T-) \right] \Delta t$$

MANUAL

From the above identities, it is seen that torquing time ( $\Delta t$ ) is proportional to the change in velocity ( $\Delta V$ ).

$$\begin{split} \kappa_1 \, \Delta v &= \, \kappa_2 \, \, \Sigma \, \left[ (\mathrm{T+}) \, - \, (\mathrm{T-}) \right] \, \, \Delta t \\ \\ \Delta v &= \frac{\kappa_2}{\kappa_1} \, \, \Sigma \, \left[ (\mathrm{T+}) \, - \, (\mathrm{T-}) \right] \, \, \Delta t \end{split}$$

The time (  $\Delta t),$  representative of the  $\Delta V,$  is sent to the LGC in the form of P and N pulses (figure 2-9).

In addition to selecting the proper torque generator winding, the outputs of the binary current switch flip-fine also go to two AND gates where they are ANDed with the 3,200 cps data pulses from the LGC. The data pulse is three microseconds in width and is timed to occur two microseconds after the leading edge of the switch pulse. (See figure 2-11.) The data pulse are both 3,200 cps, therefore the LGC receives either a P pulse or an N pulse once every 1 ÷ 3200 second. When the PIP is sensing no acceleration, the pendulum is oscillating at a frequency of \$33-1/3 cps; and the LGC is receiving three P pulses and three N pulses once every y cycle or once every 1 + 533-1/3 seconds. The LGC contains a forward-backward counter which receives the velocity pulses and detects any actual gain in velocity.

The counter counts forward on the three P pulses and then backward on the three N pulses. The counter continues this operation and generates no  $\Delta V$  pulses. With an acceleration input to the PIP, however, the loop no longer operates at the 3-9 ratio and the counter exceeds its capacity and reads out the plus or minus  $\Delta V$  pulses which are then stored and used by the LGC. The additional pulses above the 3-9 ratio are representative of the additional torque supplied by the torque generator to compensate for the acceleration felt by the LEM. Each pulse indicates a known value of  $\Delta V$  due to the loop scale factor.

The PIPA calibration module (figure 2-12) compensates for the inductive load of the 16 PIP torque generator ducosyns and regulates the balance of the plus and minus torques. The calibration module consists of two load compensation networks for the torque generator coils to make them appear as a pure resistive load to the binary current switch. A variable balance potentiometer regulates the amount of torque developed by the torque generator coils. Adjustment of this potentiometer precisely regulates and balances the amount of torque developed by the T-a and T- torque generator coils. This balancing insures that for a given torquing current an equal amount of torque will be developed in either direction.

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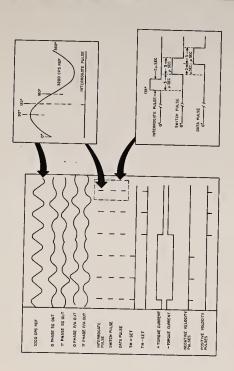


Figure 2-11. Accelerometer Timing

2-19

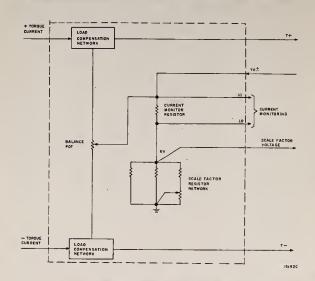


Figure 2-12. PIPA Calibration Module

The calibration module also includes a current monitor resistor and an adjustable scale factor resistor network in series with the torque generator colls. A nominal six volts is developed across the scale factor resistor network due to the torquing current and is applied as an input to the dc differential amplifier and precision voltage reference module. The voltage drop across the current monitor resistor is used for external monitoring purposes.

The dc differential amplifier and PVR are identical to the ones used in the fine align electronics. (See figure 2-8.) The dc differential amplifier and PVR module maintain the current through the ducosyn torque generator coils at a set value which produces the proper scale factor (approximately 43 milliamperes). The PVR is supplied with regulated 28 wdc and, through the use of precision circuits, develops a stable 6 volts (nominal) for use as a reference voltage. The scale factor resistor in the calibration module also develops 6 volts when the set value of current flows through it. A comparison is made by the dc differential amplifier of the PVR 6 volts and the scale factor 6 volts. Any deviation of the torquing current from the set value increases or decreases the scale factor resistor voltage and results in an output error signal from the do differential amplifier. This error signal controls the current regulator in the binary current switch. The current regulator, which is in series with the 120 vdc source and the ducosyn torque generator coils, maintains the torque current at the set value.

2-4.4 IMU TEMPERATURE CONTROL SYSTEM. The 1MU temperature control system (figures 2-13 and 2-13A) maintains the temperature of the stabilization gyros and accelerometers within the required temperature limits during both standby and operating modes of the IMU. The system supplies and removes heat to maintain the IMU heat balance. Heat is removed by convection, conduction, and radiation. The natural convection used during IMU standby mode changes to blower controlled, forced convection during IMU operating modes. The IMU internal pressure is maintained between 3.5 and 15 psia to enable the required forced convection. To add in removing heat, a water-glycol solution at approximately 45 degrees Fahrenheit from the spacecraft coolant system passes through the coolant passages in the IMU case.

2-4.4.1 Temperature Control Circuit. The temperature control circuit maintains the gyro and accelerometer temperature. The temperature control circuit consists of a temperature control thermostat and heater assembly, a temperature control module, three IRIG end mount heaters, three IRIG tapered mount heaters, two stable member heaters, and three accelerometer heaters. The thermostat and heater assembly is located on the stable member and contains a mercury-thallium thermostat, a bias heater, and an anticipatory heater. Except for the bias heater, all heaters (a total of 12) are connected in parallel and are energized by 28 vdc through an switching action of transistor Q2, which completes the dc return path. The thermostat acts as a control sensing element and senses the temperature of the stable member.

MANUAL

When the thermostat temperature fails below 130 (±0.2) degrees Fahrenheit, the more transistor Q2 conducts, our conducts and drives transistor Q2 to conduct on. When transistor Q2 conducts, our conduct on. When transistor Q2 conducts, our conduct on. The cause of the large mass of the stable member, its temperature will increase at a relatively slow rate as compared to the gyros, which have a heater in each end mount. The anticipatory heater improves the response of the thermostat to insure that the magnitude of the temperature oycling of the gyros and the accelerometers is as small as possible. When the thermostat temperature rises above 130 (±0.22) degrees Fahrenheit, the thermostat closes and the base of transistor Q1 is shorted to ground, cutting off transistors Q1 and Q2 and deenergizing the heaters. The temperature control circuit will maintain the average of the gyro temperatures at 135 degrees Fahrenheit and the average of the accelerometer temperature difference between the gyros and the accelerometers is adjusted by properly proportioning the amount of power in each heater.

During IMU operation, power is applied to the fixed accelerometer beaters to compensate for the additional heat supplied to the gross by the gyro wheel motor heat dissipation. Power is also applied to a bias heater on the control thermostat. The bias heater supplies a fixed amount of heat to the control thermostat to maintain the proper absolute temperature level of the gyros and accelerometers. The amount of bias heat is controlled by the selection of resistor R5. The power for the fixed accelerometer heaters and the thermostat bias heater are the -90 degree and -180 degree outputs, respectively, from the 28 vac power supplies which are also used for gyro wheel power.

The 28 vdc heater power is applied to the heaters through the contacts of a safety thermostat which will provide protection against an extreme overheat condition in case a malfunction occurs in the temperature control circuit. The safety thermostat contacts open at 139.5 (±3.0) degrees Fahrenheit and close at 137 (±3) degrees Fahrenheit.

2-4.4.2 Blower Control Circuit for PGNCS 601 and 602. The blowers maintain IMU heat balance by removing heat. The blowers operate continuously during IMU operate modes. The blower control circuit shown on figure 2-13 is inoperative because the contacts of blower control relay K1 are bypassed.

The blowers are supplied from the -90 and -180 degree outputs of the 28 volt, 800 cps, power supplies which also provide gyro wheel motor power. Fused phase shift networks are associated with each blower so that excitation and control current can be supplied from the same source.

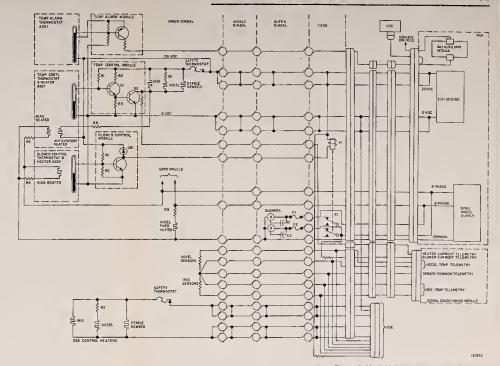
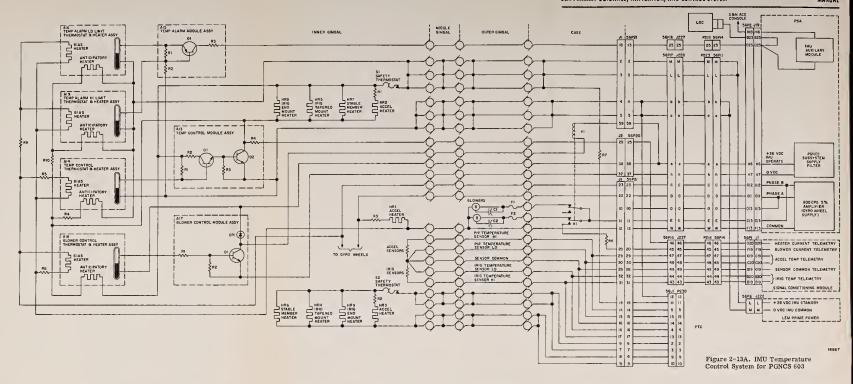


Figure 2-13, IMU Temperature Control System PGNCS 601 and 602







2-4.4.2A Blower Control Circuit for PGNCS 603. The blower control circuit (figure 2-13A) maintains IMU heat balance by removing heat. The blower control circuit consists of a blower control thermostat and heater assembly, a blower control module assembly, two axial blowers, and a relay. The contacts of the thermostat contained in the blower control thermostat and heater assembly close at 139 (±0.2) degrees Fahrenheit and remain closed at higher temperatures. Resistor R6 is provided to limit the current through the bias heater in the blower control thermostat and heater assembly. The amount of heat supplied by the bias heater is a constant. If the duty eycle of the temperature control circuit exceeds 50 percent, enough additional heat will be provided by the anticipatory heater to increase the temperature of the blower control thermostat and heater assembly to 139 degrees Fahrenheit. When the thermostat contacts close, transistor Q1 conducts and relay K1 is energized to remove the power from the blowers. The normal duty cycle of the temperature control circuit, with the IMU in a 75 degree Fahrenheit ambient temperature, is approximately 15 to 20 percent. Under this condition the blowers will operate continuously. Only a very low ambient temperature will cause a blower off condition.

Power to the blowers is supplied from the -90 degree output of the 28 volt, 800 cps, 5 percent power supply which also provides gyro wheel motor power. Fused phase shift networks are associated with each blower so that excitation and control current can be supplied from the same source.

2-4.4.3 Temperature Alarm Circuit for PGRCS 601 and 602. The temperature alarm circuit (figure 2-13) monitors the temperature control system. The temperature alarm circuit consists of a temperature alarm thermostal and a temperature control module. If a high or low temperature is sensed by the temperature alarm thermostal located on the stable member, a discrete is sent to the LGC and the IMU auxiliary module. When the temperature is within the normal range of 126.3 to 134.3 degrees Fahrenheit, 28 vod is applied through the thermostat to the emitter of transistor Q1 causing the transistor to conduct. Transistor Q1 conducts through a grounding system in the LGC.

When the temperature falls below 126.3 degrees Fahrenheit, 28 vdc will be removed from transistor Q1, causing it to stop conducting and thus signaling the LGC of an alarm condition. When the temperature rises above 134.3 degrees Fahrenheit, 28 vdc will be applied directly to the base of the transistor as well as to the emitter. With 28 volts applied to both emitter and base, the base-emitter junction is no longer forward biased and the transistor stops conducting which signals the LGC of an alarm condition. There is no differentiation between a high or low temperature alarm. When the LGC senses a temperature alarm, it causes the IMU TEMP lamp and the PGNCS lamp to light. When the IMU auxiliary module receives a temperature alarm, it sends the information to telemetry.



2-4.4.3A Temperature Alarm Circuit for PCNCS 503. The temperature alarm circuit which monitors the temperature control system, consists of a temperature alarm high limit thermostat and heater assembly, a temperature alarm module assembly, and a temperature alarm module assembly. If a high or low temperature is sensed by the thermostats located on the stable member a discrete is sent to the LGC and to the IMU auxiliary module. When the temperature is within the normal range, the low limit thermostat contacts are closed and the high limit thermostat contacts are grounding system in the LGC.

At temperatures below 128.0 (e0.2) degrees Fahrenheit both the low limit thermostat contacts and the high limit thermostat contacts are open. At temperatures above 134.0 (e0.2) degrees Fahrenheit both the low limit thermostat contacts and the high limit thermostat contacts are closed. In either case, transistor Q1 is not able to conduct. Non-conduction of transistor Q1 signals the LGC of an alarm condition. There is no differentiation between a high or low temperature alarm. When the LGC senses a temperature alarm. it causes the TEMP and PGNCS lamps to light. When the IMU auxiliary module receives a temperature alarm, it sends the information to telemetry.

2-4.4.4 External Temperature Control. External temperature control of the IMU is provided by GSE control heater circuits in the IMU which are controlled externally to the airborne equipment by the portable temperature controller (PTC) or the temperature monitor control panel of the optics-inertial analyzer (OlA). The GSE control heater circuitry consists of a safety thermostat, six gyro heaters, two stable member heaters, three accelerometer heaters, temperature indicating sensors, and an IMU standby power sensor which disables the GSE when airborne power is on. The temperature indicating sensors act as the control sensing element of the external control and indicating circuitry. The heaters are connected in parallel. The six gyro temperature indicating sensors (two in each gyro) are connected in series to sense the average temperature of the gyros. The three accelerometer temperature indicating sensors (one in each accelerometer) are connected in series to sense the average temperature of the accelerometers. All of the GSE control heater circuitry is electrically independent of the airborne temperature control system and will not be used at the same time that the IMU temperature is being controlled by the airborne temperature control system. The GSE control heater circuitry cannot be used as a backup temperature control system during flight.

2-4.5 ISS MODES OF OPERATION. The ISS has four major modes of operation: IMU turn on, CDU zero, coarse align, and inertial reference. Submodes which will also be discussed are fine align, IMU cage, attitude error indication and display inertial data. An additional mode is the master reset condition which is available during laboratory testing only. All ISS moding is initiated and controlled by computer discretes to the CDU. (See figure 2-14.) To select an ISS mode of operation, the LGC can send a single discrete, a combination of discretes, or no discretes. The display inertial data function utilizes the RR channels of the CDU. therefore, a description of the discretes to the RR channels of the CDU will also be presented.

MANUAL

2-4,5.1 <u>CDU Discretes.</u> All LGC discretes issued to the CDU to initiate and control the various ISS modes or functions are 0, 0 (42) vdc, LGC ground, applied through a 2,000 ohm source impedance to the CDU mode module.

2-4,5,1,1 ISS CDU Zero. The ISS CDU zero discrete zeros or clears all three ISS CDU read counters simultaneously. It also inhibits the transmission of incrementing pulses to the read counters for the period of time the discrete is present. The CDU discrete will be present (minimum duration is approximately 400 milliseconds) for as long as the read counters are to be held at zero. The IMU is not disturbed by the CDU zero discrete.

2-4,5,1,2 ISS Enable Error Counter. The ISS enable error counter discrete enables all three ISS error counters stmultaneously which allows them to accept incrementing pulses from the LGC. The error counters are normally cleared and inhibited. The ISS enable error counter discrete is used in conjunction with the coarse align enable discrete during the coarse align mode. The ISS enable error counter discrete is used alone when display of attitude error signals on the FDAI is required only.

2-4.5.1.3 Coarse Align Enable. The coarse align enable discrete enables a relay driver which energizes the coarse align and demodulator reference relays located in the PSA. This connects the coarse align error signal to the gimbal servo amplifiers and changes the reference voltage for the demodulator in the gimbal servo amplifiers from 3, 200 cps to 800 cps. The discrete also enables the digital feetback pulses from the read counter to the error counter. The presence of the coarse align enable discrete and the absence of the enable error counter discrete also inhibits the incrementing pulses to the read counter.

2-4.5.1.4 D/A Enable. The D/A enable discrete enables both RR CDU error counters simultaneously. The error counters are normally cleared and inhibited. The LGC normally provides positioning signals to the RR through the RR channels of the CDU. The D/A enable discrete, however, is also used in conjunction with the display inertial data discrete to allow the LGC to feed inertially derived velocity data through the RR channels of the CDU to meter displays.

2-4.5.1.5 Display Inertial Data. The display inertial data discrete energizes relays which switch the dc output from the digital to analog (D/A) converter in the RR channels of the CDU to the LEM velocity meters.

2-4.5.1.6 RR CDU Zero. The RR CDU zero discrete clears both RR read counters simultaneously and inhibits the transmission of incrementing pulses to the read counters. This discrete is not used for any ISS flight modes or functions but can be used for CDU test functions.

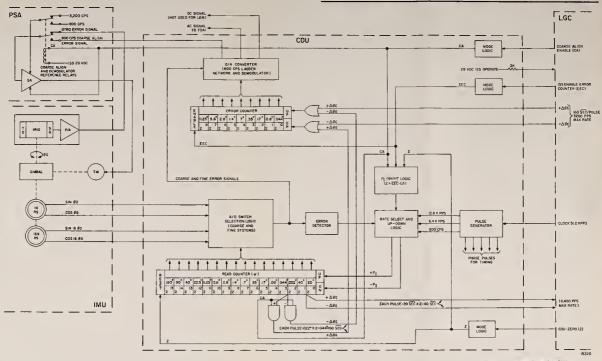


Figure 2-14, ISS-CDU Moding



2-4.5.2 IMU Turn On Mode. The purpose of the lMU turn on mode is to drive the gimbals to their zero position and hold them there. (See figure 2-15.) The lMU turn on mode is initiated upon closure of the ISS OPERATE circuit breaker and allows for a 90 second gyro run up period. The ISS OPERATE circuit breaker routes 28 vdc lMU operate power through the deenergized contacts of the ISS turn on control relay, located in the IMU auxiliary assembly module, to the cage relays. The 28 vdc IMU operate power is also routed through the same deenergized contacts to the LGC as a continuous turn on delay request discrete. The cage relays energize and, in turn, cause the coarse align relays to be energized. The cage relays route the IX gimbal resolver sine winding outputs through the contacts of the coarse align relays to the respective gimbal servo amplifiers. The gimbal servo amplifiers drive the gimbals until the resolver signals are nulled. The operation of the caging loops is discussed further in the IMU cage mode description.

Upon receipt of the ISS turn on delay request discrete, the LGC sends the ISS CDU zero discrete and the coarse align enable discrete to the CDU for a minimum period of 90 seconds. The CDU zero discrete clears the read counters and inhibits the incrementing pulses to the read counters. The coarse align enable discrete provides a redundant means of energizing the coarse align relays.

A second set of deenergized contacts on the ISS turn on control relay routes a ground to the time delay circuit of the pulse torque power supply which thinbits the operation of the power supply and thus prevents accelerometer pulse torquing during the 90 second turn on period. This allows time for the accelerometer floats to become centered and the gyro wheels to run up prior to torquing.

After the 90 second delay has been completed, the LGC sends the ISS turn on delay complete discrete acts through a relay driver to energize and latch in the ISS turn on control relay. Benergizing the ISS turn on control relay deenergizes the cage relay, removes the ISS turn on delay request discrete, and removes the inhibit from the pulse torque power supply. The computer program can then place the ISS in the inertial reference mode by removing both the CDU zero and the coarse align enable discretes, or it can initiate the coarse align mode by removing only the CDU zero discrete and sending the ISS enable error counter discrete. The IMU turn on circuit will be reset whenever 28 vdc IMU operate power is turned off.

2-4.5.3 IMU Cage Mode. The IMU cage mode is an emergency backup mode which allows the astronaut to recover a tumbling IMU by setting the gimbals to zero. (See figure 2-15.) During this mode, the IX gimbal resolver sine winding outputs are fed through the CDU to the gimbal servo amplifiers to drive the gimbals until the resolver signals are nulled.

The IMU cage mode is initiated when the astronaut presses the IMU CAGE switch. The switch is held until the gimbals settle at the zero position (five seconds maximum). The gimbal position may be observed on the FDAI. The IMU CAGE switch routes a world discrete signal to the LGC and to the cage relays located in the PSA. (See figure 2-15.) The cage discrete energizes the cage relays, which in turn, cause the coarse align relays, the demodulator reference relay, and a relay in the gimbal servo amplifiers to energize. The relay in the gimbal servo amplifiers to energize. The relay in the gimbal servo amplifiers so the servous constraints of the servous capacitance into the RC compensation networks to tune them for 800 cps operation. The demodulator reference relay changes the gimbal servo amplifier demodulator reference signal from 3,200 cps to 800 cps. The cage relays switch the 1X gimbal resolver sine winding outputs through the energized contacts of the coarse align relays into the corresponding gimbal servo amplifier inputs. The gimbal servo amplifiers drive the gimbal surful the resolver signals are nulled.

Upon receipt of the IMU cage discrete, the LGC will discontinue sending the error counter enable discrete, the coarse align enable, the display inertial data discrete, and the incrementing pulses to the CDU. The LGC will also discontinue sending torquing commands, if any are in process, to the fine align electronics.

After the IMU CAGE switch is released, the LGC will allow the read counters to settle and will then place the PGNCS in an attitude control mode. During the time the IMU cage discrete is present and while the read counters are settling, the NO ATT lamp on the DSKY is lighted.

The cage mode will also be entered automatically if the IMU is turned on when the LGC is off or in standby mode. During the normal turn on sequence, the closure of the ISS OPERATE circuit breaker will route 28 vdc through the deenergized contacts of the ISS turn on control relay to the cage relays. The cage relays energize and cage the gimbals. After the 90 second turn on time delay has been completed, the LGC will send the ISS turn on delay complete discrete which will energize the ISS turn on control relay which, in turn, deenergizes the cage relays. If, however, the LGC is off or in standby when the IMU is turned on, the ISS turn on control relay will remain deenergized and the ISS will remain in the IMU cage mode.

If the IMU cage mode is entered as a result of an IMU turn on with the LGC off or in standby, the ISS can be placed in the inertial reference mode by allowing 90 seconds for gyro runup then pressing the IMU CAGE switch. The IMU CAGE switch will energize and latch in the ISS turn on control relay which removes the 28 vdc which had been energizing the cage relays. With the ISS turn on control relay altached, the cage relays will deenergize and remain deenergized when the IMU CAGE switch is released. Deenergizing the cage relays causes the coarse align relays to be deenergized which connects the gyro error signals to the respective gimbal servo amplifiers. The stabilization loops will maintain the stable member inertially referenced to the orientation established by the caging loops.

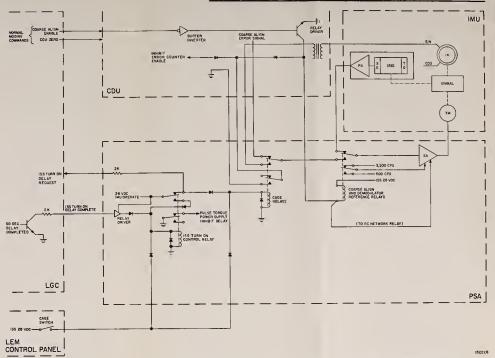


Figure 2-15. IMU Cage Mode



2-4.5.4 <u>ISS\_CDU\_Zero.</u> The purpose of the ISS\_CDU\_zero mode is to clear and inhibit the three ISS\_CDU\_read counters. (See figure 2-14.) The mode is initiated by the LGC sending the ISS\_CDU\_zero\_discrete. The presence of the discrete is maintained for as long as the read counters are to be held at zero.

2-4.5.5 Coarse Align Mode. The purpose of the coarse align mode is to change the orientation of the ginhals by LGC command. The change in gimbal orientation is accomplished by feeding the CDU error counter computer pulses equal to the required change in gimbal angles. The mode is initiated when the LGC sends the coarse align discrete and, after a short delay, the ISS error counter enable discrete to the three ISS channels of the CDU. The LGC, knowing the actual gimbal angle registered in the read counter, calculates the desired anount of change in gimbal angle registered to reposition the gimbal to the desired angle and converts this change into a number of  $^{\circ}\Delta\theta_{\rm G}$  pulses to be sent to the error counter. The  $^{\circ}\Delta\theta_{\rm G}$  pulses are sent to the error counter at a rate of 3.200 pps in bursts. Each  $\Delta\theta_{\rm G}$  pulses are sent to the error counter at a rate of 3.200 pps in bursts. Each  $\Delta\theta_{\rm G}$  pulses is equal to a change in gimbal angle of approximately 158 arc seconds. The error counter, having been enabled, accepts the pulses and counts up or down, as necessary, until all the pulses have been registered.

The digital information in the error counter is converted into an 800 cps, amplitude modulated, analog error signal by the ladder decoder in the D/A converter module. The ladder decoder signal is summed with a feedback signal and applied through a mixing amplifier located in the D/A converter module to the gimbal servo amplifiers to drive the gimbals to the desired angles. The function of the feedback signal and the mixing amplifier will be discussed later. The output of the mixing amplifier, referred to as the coarse align error signal, is applied to the gimbal servo amplifiers through the contacts of the coarse align relays located in the PSA, The coarse align relays, which are energized by the coarse align enable discrete acting through a relay driver, switch the input of gimbal servo amplifiers from the gyro preamplifiers to the coarse align error signal output of the ISS D/A converters. The demodulator reference relay is also energized by the coarse align enable discrete and switches the reference frequency of the demodulator in the gimbal servo amplifiers from 3,200 cps to 800 cps. The coarse align enable discrete also energizes a relay in the gimbal servo amplifiers which switches in additional capacitance into the amplifier's compensation networks to tune them for 800 cps operation,

As the gimbals are driven, pulses, representing the change in actual gimbal angle, are generated by the read counter and applied to the error counter. These pulses are also equal to approximately 15% are seconds and act to decrease the  $\Delta\theta_{\rm s}$  pulses registered in the error counter. The error counter output to the ladder decoder, therefore, represents the difference between the desired amount of change in gimbal angle and the amount of change actually accomplished. When the error counter reaches a null and the gimbals stop moving, the actual gimbal angle has changed by an amount equal to the total value of the  $\Delta\theta_{\rm c}$  pulses sent by the LGC to the error counter. The LGC checks the content of the read counters 2.1 seconds after sending the last  $\Delta\theta_{\rm c}$  pulse to the error counters. If the gimbal angles are not within two degrees of the desired angles, the LGC issues an alarm.

MANUAL

The rate at which the gimbals are driven is limited to prevent damage to the gyros and to assure that the read countercantrack the gimbal angle accurately. The rate of gimbal movement is limited by feeding backthe CDU fine error signal [sin 16 (θ-ψ)] to the input of the mixing amplifier located in the D/A converter module. The CDU fine error signal is out of phase with the output of the ladder decoder and has an amplitude proportional to the difference between the actual gimbal angle (0) and the angle in the read counter (4). The fine error signal is applied through a voltage limiting circuit to the summing junction of the mixing amplifier where it is summed with the 800 cps ladder decoder output signal. The D/A converter ladder decoder output is applied to the mixing amplifier through a scaling amplifier and a voltage limiting diode network. The scaling amplifier controls the signal gain to produce a scale factor of 0.3 volt rms per degree. The output of the mixing amplifier will be at a null when the D/A converter ladder decoder output, after limiting, is equal to the fine error feedback signal. The fine error signal will be a constant value only when the gimbal and the CDU are going at the same rate and with the gimbal angle leading the CDU angle. Since the CDU is limited to counting at one of two speeds, the gimbals will be limited to a rate equal to one of these two speeds. During the coarse align mode, the CDU is limited to a high counting speed of 6.4 kpps and a low counting speed of 800 cps. At all other times, the high counting speed is 12.8 kpps.

If the gimbals are moving ata faster rate than the rate at which the CDU is counting, the fine error signal will increase, causing a retarding torque to be developed by the gimbal servo amplifier. If the gimbals are moving at a rate slower than the rate at which the CDU is counting, the fine error signal will decrease, causing the gimbal servo amplifier to apply an accelerating torque to the gimbals. By adjusting the gain of the fine error signal into the mixing amplifier, the gimbal drive rate is limited to either 35.5 degrees per second (6.4 kpps CDU counting rate) or 4.5 degrees per second (800 cns CDU counting rate).

2-4.5.6 Inertial Reference Mode. The inertial reference mode provides a coordinate reference system on which attitude and velocity measurements and calculations may be based. During the inertial reference mode, the stable member is held fixed with respect to an inertial reference by the stabilization loops. The ISS CDU read counters provide the LGC with changes in gimbal angles with respect to the stable member. The ISS is in the inertial reference mode during any operating period in which there is an absence of moding commands. During the inertial reference mode, the fine align electronics is inhibited and the ISS CDU error counters are cleared and inhibited.

2-4.5.7 Fine Align Mode. The purpose of the fine align mode is to reposition the stable member to a fine alignment by torquing the gyros. The fine align mode is actually a gyro torquing function accomplished during the inertial reference mode. The torquing current to the gyros is provided by the fine align electronics located in the PTA. The fine align electronics is enabled and controlled by LGC pulses sent directly to the fine align electronics. The LGC does not send command discretes to the ISS CDU's during this mode. The ISS is in the inertial reference mode prior to the enabling of the fine align electronics and returns to that mode when the fine align electronics is disabled.

The fine align electronics torques the gyros on a time shared basis. The LGC sends four types of pulse trains to the fine align electronics. The first pulse train sent is the torque enable command which enables the fine align electronics. The second pulse train is a gyro select command which selects a particular gyro and the direction it is to be torqued by means of a switching network which closes the current path through the proper torque ducosyn coil. The third and fourth types of pulse trains are the torque set and torque reset commands which control a binary current switch to start and stop the current flow through the selected torque ducosyn coil. The amount of current flow through the torque ducosyn coils is precisely controlled at a fixed value. The amount of gyro torquing to be accomplished is determined by the amount of time torque current is applied; that is, the time duration between the receipt of the torque set and the torque reset commands. This time duration is calculated by the LGC. The torque ducosyn displaces the gyro float, causing the ducosyn signal generator to apply an error signal to the stabilization loop. The stabilization loops drive the gimbals to reposition the stable member. Upon completion of the torquing, the stable member remains fixed in its inertial reference and in fine align mode until the torque enable command is removed, after which the ISS remains in inertial reference mode until further change is commanded.

During the fine align mode, the ISS CDU error counters remain cleared and inhibited. The CDU read concinue to repeat the gimbal angles and send angular data  $\pm (\Delta\theta_c)$  to the LGC.

2-4.5.8 Attutide Error Indication. The attitude error indication mode supplies attitude error signals to the FDAI. The attitude error indication mode is initiated when the LGC sends the ISS error counter enable discrete to the CDU. The LGC will calculate the difference between the actual gimbal angles and the correct angles and convert this into the number of  $4 \, \Delta \theta_c$  pulsess to be sent to the error counter. The error counter, having been enabled, accepts the pulses and counts up or down until it has registered all the pulses.

The digital information in the error counter is converted into an 800 cps, amplitude modulated, analog error signal by the ladder decoder in the D/A converter. This as signal is applied through a scaling amplifier to the FDAI. As the actual gimbal angles change, the LGC sends additional  $\pm \Delta \theta_{\rm C}$  pulses to count the error counter upor down, thereby changing the signal to the FDAI.

2-4.5.9 <u>Display Inertial Data</u>. The display inertial data mode permits the LGC to provide inertially derived forward and lateral velocity signals through the digital to analog section of the RR channels of the CDU to the LEM velocity display meters. The display inertial data mode is used during the last phases of the LEM powered descent.

The display inertial data mode is requested by the astronaut closing a switch on the min control panel. (See figure 2-16.) The mode is initiated by the LGC sending the display inertial data discrete to the RR channels of the CDU. The display inertial data discrete acts through a relay driver to energize relays which connect the D/A converter do error signal outputs to the LEM velocity display meters. After a brief delay to allow for relay pull in time, the LGC sends the D/A enable discrete followed by incrementing pulses to the error counters. The LGC sends  $\pm \Delta \Phi_c$  pulses representing LEM forward velocity (motion along the  $Z_{\rm LEM}$  axis) to one error counter and  $\pm \Delta \Phi_c$  pulses representing LEM lateral velocity (motion along the vehicle  $Y_{\rm LEM}$ ) to the other error counter. The read counters will not send incrementing pulses to the error counters; therefore, the only information registered in the error counters will be the  $\pm \Delta \Phi_c$  pulses.

The digital information registered in the error counter is converted into an 800 cps, amplitude modulated, analog signal by the ladder decoder in the D/A converter. This signal is converted into a dc analog signal by a phase sensitive demodulator circuit also located in the D/A converter. The dc analog signal is applied through the energized relay contacts to the LEM velocity display meters. As the velocity changes, as calculated by the LGC, representative  $\pm\Delta\theta c$  pulses will continue to be sent to the error counter, causing it to count up or down and thereby changing the D/A converter dc signal to the display meters.

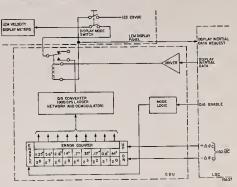


Figure 2-16. Display Inertial Data Mode

2-4.5.10 Master Reset Condition (Test Area Only). The purpose of the master reset condition is to establish preselected standard operating modes in both the airborne equipment and the GSE. The master reset condition is operable in the ISS test configuration only. The master reset condition is initiated when the MASTER RESET pushbutton on the test control panel of the OIA is pressed.

The effects of establishing a master reset condition are dependent upon the particular ISS level of test, power mode status, et cetera, at the time the MASTER RESET pushbutton is pressed, With the ISS STANDBY pushbutton selected, but prior to pressing the ISS OPERATE pushbutton, the MASTER RESET pushbutton will cause the simultaneous closure of the IMU stabilization loops. During the Irst 90 seconds after pressing the ISS OPERATE pushbutton, the MASTER RESET pushbutton is disabled. Ninety seconds after pressing the ISS OPERATE pushbutton the MASTER RESET pushbutton is enabled and, if selected, simultaneously performs the following operations: causes the coarse align mode to be commanded, places the gimbals under gimbal positioner control, and removes all IMU caging signals. The master reset condition also discontinues all RR mode commands and commands the RR channels of the CDU to repeat the RR angles.

## 2-4.6 ISS POWER SUPPLIES.

The ISS power supplies convert the +28 vdc prime LEM power into the various dc and ac voltages required by the ISS. The power supplies are the pulse torque power supply; the -28 vdc power supply; the 800 cps, I percent power supply; the 800 cps. 5 percent, 2 phase, power supply; and the 3,200 cps power supply. The pulse torque power supply is in the PTA and the remaining power supplies are in the PSA.

The +28 vdc prime power is supplied by the LEM electrical power system through the ISS OPERATE circuit breaker. All ac power supplies are synchronized to the LGC clock by means of computer pulses. The dc supplies, using multivibrators as ac sources for transformation, are also synchronized to the LGC. Synchronization is accomplished by a multivibrator which will free run at a lower frequency without the computer pulses, assuring operation of the ISS power supplies in the event of an LGC failure.

2-4.6.1 Pulse Torque Power Supply. The pulse torque power supply (figure 2-17) provides 120 vdc to the three binary current switches and three dc differential amplifiers in the accelerometer loops and the binary current switch and dc differential amplifier in the stabilization loop fine align electronics. The pulse torque power supply also provides three individual 28 vdc outputs to the accelerometer loop PVR's, 20 vdc to the three accelerometer loop ac differential amplifier and interrogator modules and the associated binary current switches, and -20 vdc to the ac differential amplifier and interrogator module in the accelerometer loops.

The -20 vdc output is derived from the -28 vdc power supply by using a zener diode as a voltage divider and regulator. The output is regulated at -20( $\pm0.8$ ) vdc.

The 20 vdc output is derived from 28 vdc prime power by the use of a three transistor series regulator which maintains the output voltage at 20 ( $\pm 0.55$ ) vdc.

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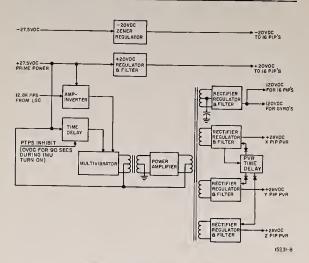


Figure 2-17. Pulse Torque Power Supply

The 120 vdc and 28 vdc PVR outputs are derived from a multivibrator, a power amplifier, and a rectifier and filter. A 12.8 kpps synchronizing pulse is received from the LGC through a buffer transformer in the pulse torque insolation transformer assembly and is applied to an amplifier-inverter. The output of the amplifier-inverter is applied to a multivibrator-chopper causing it to be synchronized at 6,400 cps. A transistorized time delay circuit is incorporated into the emitter circuits of the multi-vibrator to provide a turn on time delay of approximately 350 milliseconds. During the 90 second IMU turn on mode, 0 vdc is applied through the turn on circuits of the IMU auxiliary assembly module to the time delay circuit which inhibits the 120 vdc and

28 vdc PVR supplies. The multivibrator-chopper output is applied to the primary of a transformer which has 28 vdc prime power applied to its center tap. The secondary of the transformer, which is also center tapped, is coupled to a two stage push-pull power amplifier which operates from 28 vdc prime power. The output of the power amplifier consists of a transformer with four secondary windings; one with center tap return for the 120 vdc power supply, and one each for the X, Y, and Z accelerometer loop 28 vdc PVR supplies. The 120 vdc power supply consists of a full wave rectifier whose output is filtered, regulated, and again filtered. The 28 vdc power supplies are identical and consist of a full wave bridge rectifier whose output is filtered, regulated, and again filtered. The PVR time delay circuit inhibits the operation of the regulator in each 28 vdc PVR circuit to provide a six to eight second time delay in the 28 vdc PVR outputs.

2-4.6.2 -28 VDC Power Supply. The -28 vdc power supply provides input power to the three gimbal servo amplifiers in the stabilization loops and to the pulse torque power supply to generate -20 vdc for use in the accelerometer loops. The -28 vdc power supply consists of a pulse amplifier-inverter, a multivibrator-chopper, a power amplifier, and a rectifier and filter. (See figure 2-18.) The 25.6 kpps synchronization pulse input is amplified and inverted for use in synchronizing the multivibrator-chopper at 12.8 kcps. The multivibrator-chopper output is applied to the primary of a transformer which has 28 vdc prime power applied to its center tap. The secondary of the transformer, which is also center tapped, is coupled to a push-pull power amplifier. The output of the amplifier is transformer coupled to a full wave rectifier and filter whose positive side is referenced to ground to provide a -27.0 (±1.0) vdc output.

2-4.6.3 800 CPS Power Supply. The 800 cps power supply (figure 2-19) consists of four modules: an automatic amplitude control, filter, and multivibrator; a 1 percent amplifier: and two 5 percent amplifier control, filter, and multivibrator; a 1 percent amplifier excitation, gimbal servo amplifier demodulator reference, and FDAI and control electronics section (CES) reference. The two 5 percent amplifiers provide gyro wheel excitation, IMU blower excitation, and accelerometer fixed heater power. The 1 percent amplifiers also provides the input to one of the 5 percent amplifier is applied to the second 5 percent amplifier whose output is phase shifted -90 degrees. The output of this 5 percent amplifier is applied to the second 5 percent amplifier whose output is also phase shifted -90 degrees, or -180 degrees from the output of the 1 percent amplifier. The outputs of the 1 percent amplifier and the 5 percent amplifiers are applied to their respective loads through the IMU load compensation network which provides a power factor correction.

Zero and pi phase, 800 cps pulse trains from the LGC synchronize the multivibrator at 800 cps. In the absence of the synchronizing pulses, the multivibrator will free run between 720 and 790 cps. The output of the multivibrator controls the operation of the chopper and filter circuit. The filtered chopper output is applied to the 1 percent amplifier. The output of the 1 percent amplifier. The output of the 1 percent amplifier in addition to its direct uses, is a feedback signal to the automatic amplitude control circuit. The positive peaks of this feedback signal are detected and added to a dereference signal. The sum is filtered and provides a de bias to the multivibrator driven chopper. The bias controls the amplitude of the chopped signal.

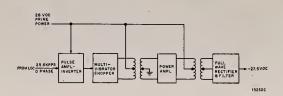


Figure 2-18. -28 VDC Power Supply

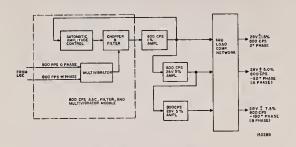


Figure 2-19. 800 CPS Power Supply

The 1 percent amplifier is push-pull in operation with transformer coupled input and output and with overall voltage feedback for gain and distortion control.

The two 5 percent amplifiers are identical in operation. The amplifiers are push-pull and have transformer coupled inputs and outputs. The Input transformer primary center tap is connected to the input signal low. The input signal high is applied directly to one side of the primary winding and is also applied through a phase shift network to the other, or out of phase, side of the primary. A feedback signal from the secondary of the output transformer is also applied to the out of phase side of the input transformer primary where it is mixed with the phase shifted portion of the input signal. This mixing results in a -90 degree phase shift in the secondary of the input transformer. The output of the first 5 percent amplifier is used as an input to the second 5 percent amplifier to provide an additional -90 degree phase shift.

2-4.6.4 3,200 CPS Power Supply. The 3,200 cps power supply provides excitation voltage for the signal generator and the magnetic suspension portions of the IRIG and PIP ducosyns. The 3,200 cps output is also used as a reference for the demodulator in the gimbal servo amplifiers.

The excitation voltage to the signal generators requires hoth voltage stability and phase stability. To accomplish this stability, the excitation voltage power transmission to the stable member is through a step down transformer on the stable member which reduces the slip ring current and, therefore, voltage drop effects due to slip ring, cable, and connector resistance. In addition, each wire connecting the output of the transformer to the input terminals of each PIP1s out to exactly the same length. The voltage level at the primary of the transformer is fed hack to the power supply and is compared to a voltage reference.

The 3,200 cps power supply (figure 2-20) consists of an amplitude control module and a 1 percent power amplifier. The amplitude control module contains an automatic amplitude control circuit, a multivihrator, a chopper, and a filter.

The 3, 200 pps pulse trains of zero degree phase and 180 degree phase synchronize a multivibrator. The output of the multivibrator controls the operation of the chopper circuit. The output of the chopper is applied to the 1 percent power amplifier. The 28 volt rms output of the amplifier is transmitted through the slip rings to the transformer on the stable member where the voltage is stepped down to 2 volts for the accelerometer ducosyns and 4 volts for the gyro ducosyns. A sample of the 28 volt level at the primary of the transformer is fed hack through the slip rings to the input of the automatic amplitude control circuit. The positive peaks of the feedback signal are detected and added to a dc reference signal. The sum is filtered and provides a dc hias to the chopper circuit. The dc hias controls the amplitude of the chopper output to the filter.

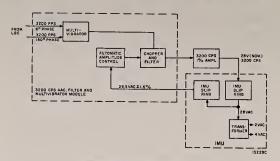


Figure 2-20. 3,200 CPS Power Supply

## 2-5 ALIGNMENT OPTICAL TELESCOPE

The AOT provides a means of manually taking direct visual sightings and precision angular measurements of preselected celestial targets. These measurements are manually transferred by the astronaut to the LGC through the DSKY, The LGC uses this angular information along with pre-stored data to compute the LEM position and velocity and to accomplish a fine alignment of the IMU stable member.

In the lunar pre-launch phase, the AOT is used to obtain the necessary information for an accurate LEM launch trajectory to intercept the CSM.

During lunar orbital flight, the measurements obtained with the AOT are used by the LGC to define the vehicle's position, and to correct vehicle velocity for the desired lunar orbital or landing trajectory.

2-5.1 LUNAR PRE-LAUNCH MODE. The primary function of the AOT is to facilitate an accurate determination of the vehicle's position and to fine align the IMU stable member, in an inertial coordinate reference system, prior to launch from the lunar surface. The AOT is first positioned (manually) to one of three viewing detents to make the preselected target visible within the 60 degree field of view. The AOT is then manually adjusted to obtain angular measurements, referenced to the nav base,

of the target's position in shaft and trunnion. The angular measurements are read out by the astronaut from a mechanical counter on the AOT and manually entered into the LGC through the DSKY. After angular measurements are made on two separate targets and data fed into the LGC, the LGC updates the computation of the LEM position. Using the star framework as a reference, the LGC then aligns the IMU stable member.

2-5.2 LUNAR ORBITAL FLIGHT MODE. In lunar orbital flight, the AOT is manually set to the center forward viewing detent. The LEM attitude is then changed by the astronaut until the target image is within the AOT field of view and the vehicle limit eycle causes the image to appear to oscillate across the reticle X and Y crosshairs. As the target image crosses the X or Y crosshair, the astronaut markes time of each crossing by manually keying the LGC through the MARK X or MARK Y pushbutton on the computer control and reticle dimmer assembly (CCRD). This procedure is then repeated using another target star. The LGC utilizes the crossing time inputs and the LEM attitude angles to compute the LEM velocity and improve the accuracy of the estimate of the LEM position. The LGC then fine aligns the IMU and fires the necessary RCS jets to increase or decrease velocity for the projected lunar orbital and landing trajectory.

## 2-6 COMPUTER SUBSYSTEM

The computer subsystem (CSS) is the control and processing center of the PGNCS. It consists of the LGC and a DSKY. The CSS processes data and issues discrete outputs and control pulses to the PGNCS and other LEM systems. The LGC is a parallel digital control computer with many features of a general purpose computer. As a control computer, the LGC aligns the IMU, positions the RR antenna and issues control commands to other LEM systems. As a general purpose computer, the LGC solves the guidance and navigation equations required for the LEM mission. In addition, the LGC monitors the operation of the LEM, including the CSS.

The main functions of the LGC (see figure 2-21) are implemented through the execution of the programs stored in memory, Programs are written in a machine language called basic instructions. A basic instruction contains an operation (order) code and a relevant address. The order code defines the data flow within the LGC, and the relevant address selects the data that is to be used for computations. The order code of each instruction is entered into the sequence generator, which controls data flow and produces a different sequence of control pulses for each instruction. Each instruction is followed by another instruction. In order to specify the sequence in which consecutive instructions are to be executed, the instructions are normally stored in successive memory locations. By adding the quantity one to the address of an instruction being executed, the address of the instruction to be executed next is derived. Execution of an instruction is complete when the order code of the next instruction is transferred to the sequence generator and the relevant address is in the central processor.



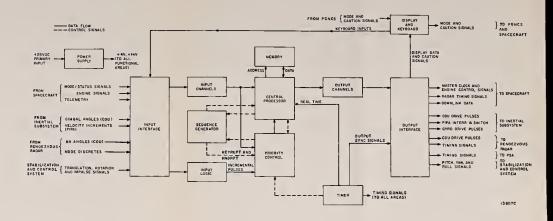


Figure 2-21. Computer Subsystem. Block Diagram



The central processor consists of several flip-flop registers. It performs arithmetic operations and data manipulations on information accepted from memory, the input channels, and priority control. Arithmetic operations are performed using the ONE's complement number system. Values of 14 bits, excluding sign, (up to 28 bits during double precision operations) are processed with an additional bit produced for overflow or underflow. All operations within the central processor are performed under control of pulses generated by the sequence generator (indicated by dashed lines in figure 2-21). In addition, all words read out of memory are checked for correct parity, and a parity bit is generated within the central processor for all words written into memory. The LGC uses odd parity, that is, all words stored in memory contain an odd number of ONE's including the parity bit. The central processor also supplies data and control signals through the output channels and provides interface for the various spacecraft subsystems.

The LGC has ten program interrupt conditions. These ten interrupts are T6 RUPT, T5 RUPT, T3 RUPT, T4 RUPT, KYRPT 1, KYRPT 2 (or MKRPT), UPRUPT, DLKRPT, RADRPT, and HNDRPT. The T6 RUPT through T4 RUPT conditions are internal interrupts initiated by the LGC. The KYRPT 1 condition is initiated when a DSKY pushbutton is depressed. A MARK signal (discrete bit), indicating a signiting, initiates KYRPT 2. This interrupt shares the same priority as the KYRPT 2 interrupt associated with the navigation DSKY in the CSM application of the computer. UPRUPT indicates the completion of an uplink word. RADRPT is generated when a complete radar word is received. HNDRPT is initiated as soon as the hand controller is moved out of detent by the astronaut.

Before a priority program can be executed, the current program must be interrupted; however, certain information about the current program must be preserved. This information includes the program counter contents and any intermediate results contained in the central processor. The priority control produces an interrupt request signal, which is sent to the sequence generator. This signal, acting as an order code, causes the execution of an instruction that transfers the current contents of the program counter and any intermediate results to memory. In addition, the control pulses transfer the priority program address in priority control to the central processor, and then to

memory through the write lines. As a result, the first basic instruction word of the priority program is entered into the central processor from memory, and execution of the priority program is begun. The last instruction of each priority program restores the LGC to normal operation, provided no other interrupt request is present, by transferring the previous program counter and intermediate results from their storage locations in memory back to the central processor.

Certain data pertaining to the flight of the LEM is used to solve the guidance and navigation problems required for the LEM mission. This data, which includes real time, acceleration, and IMU gimbal angles, is stored in memory locations called counters. The counters are updated as soon as new data becomes available. An incrementing process which changes the contents of the counters is implemented by

priority control between the execution of basic instructions. Data inputs to priority control are called incremental pulses. Each incremental pulse produces a counter address and a priority request. The priority request signal is sent to the sequence generator, where it functions as an order code. The control pulses produced by the sequence generator transfer the counter address to memory through the write lines of the central processor. In addition, the control pulses enter into the central processor the contents of the addressed counter to be incremented.

Real time plays a major role in solving guidance and navigation problems. Real time is maintained within the LGC in the main time counter of memory. The main time counter provides a 745.65 hour (approximately 31 days) clock. Incremental pulses are produced in the timer and sent to priority control for incrementing the main time counter. The LEM mission requires that the LGC clock be synchronized with the KSC clock. The LGC time is transmitted once every second by downlink operation for comparison with the KSC clock.

Incremental transmissions occur in the form of pulse bursts from the output channels to the CDU, the gyro fine align electronics, the RCS of the spacecraft, the optical tracker and the radar. The number of pulses and the time at which they occur are controlled by the LGC program. Discrete outputs also originate in the output channels under program control. These outputs are sent to the DSKY and various other subsystems. Continuous pulse trains originate in the timing output logic for synchronization of other systems.

The uplink word from the LEM telemetry system (unmanned flights) is supplied as an incremental pulse input to priority control. As this word is received, priority control procudes the address of the uplink counter in memory and requests the sequence generator to execute the instructions which perform the serial-to-parallel conversion of the input word. When the serial-to-parallel conversion is completed, the parallel word is transferred to a storage location in memory by the uplink priority program. The uplink program also retains the parallel word for subsequent downlink transmission. Another program converts the parallel word to a coded display format and transfers the display information to the DSKY.

The downlink operation of the LGC is asynchronous with respect to the LEM telemetry systems. The telemetry system supplies all the timing signals necessary for the downlink operation. These signals include start, end, and bit sync pulses.

Through the DSKY, the astronaut can load information into the LGC, retrieve and display information contained in the LGC, and initiate any program stored in memory. A keycode is assigned to each keyboard pushbutton. When a keyboard pushbutton on the DSKY is depressed, the keycode is produced and sent to an input channel. A signal is also sent to priority control, where it produces both the address of a priority program stored in memory and a priority request signal, which is sent to the sequence generator. This operation results in an order code and initiates an instruction for interrupting the program in progress and executing the KEYRUPT priority program stored in memory.

A function of this program is to transfer the keycode, temporarily stored in an input channel, to the central processor, where it is decoded and processed. A number of keycodes are required to specify an address, or a data word. The program initiated by a keycode also converts the information from the DSKY keyboard to a coded display format. The coded display format is transferred by another program to an output channel and sent to the display portion of the DSKY. The display notifies the astronaut that the keycode was received, decoded, and processed properly by the LGC.

2-6.1 PROGRAMS. An LGC program performs such functions as solving guidance and navigation problems, testing the operation of the PGNCS, and monitoring the operation of the LEM. Such a program consists of a group of program sections that are classified according to the functions they perform. These functions are defined as mission functions, auxiliary functions, and utility functions. (See figure 2-22.)

2-6.1.1 <u>Mission Functions</u>, Mission functions are performed by program sections that implement operations concerned with the major objectives of the LEM mission. These operations include erecting the IMU stable member and coarse aligning it to a desired heading prior to separating the LEM from the CSM and fine aligning it after separation. In addition, the mission functions include computation of spaceraff position and velocity during coasting periods of the flight by solution of second-order differential equations which describe the motions of a body subject to the forces of gravity.

2-6, 1.2 <u>Auxiliary Functions</u>. Auxiliary functions are executed at the occurrence of certain events, requests, or commands. These functions are performed by program sections that provide a link between the LGC and other elements of the PGNCS. This link enables the LGC to process signals from various devices and to send commands for control and display purposes. In addition, the auxiliary functions implement many and varied operations within the LGC in support of the LEM mission functions.



Figure 2-22. Program Organization

MANUAL

2-6.1.3 Utility Functions. Utility functions are performed by program sections that coordinate and synchronize LGC activities to guarantee orderly and timely execution of required operations. These functions control the operation of the LEM mission functions and schedule LGC operations on either a priority or a real-time basis. The utility functions also translate interpretite language to basic machine language which allows complex mathematical operations such as matrix multiplication, vector addition, and ot product computations to be performed within the framework of compact routines. In addition, the utility functions save the contents of registers A and Q during an interrupt condition and enable data retrieval and control transfer between isolated banks in the fixed-switchable portion of fixed memory.

2-6.2 MACHINE INSTRUCTIONS. The LGC has three classes of machine instructions: regular, involuntary, and peripheral (table 2-1). Regular instructions are programmed and are executed in whatever sequence they have been stored in memory. Involuntary instructions (with one exception) are not programmable and have priority over regular instructions. One involuntary instruction may be programmed to test computer operations. No regular instruction can be executed when the LGC forces the execution of an involuntary instruction. The peripheral instructions are used when the LGC is connected to the peripheral equipment. During the execution of any peripheral instruction, the LGC is in the monitor stop mode and cannot perform any program operation.

2-6.2.1 Regular Instructions. Four types of instructions comprise the regular instruction class. They are the basic, channel, extracode, and special instructions. Basic instructions are used most frequently. The instruction words stored in memory are called basic instruction words. They contain an order code field and an address field. Special instructions have predefined addresses and order codes; basic instructions have only predefined order codes. The special instructions are used to control certain operations in the LGC. For example, one special instruction is used to switch the LGC to the extend mode of operation. This mode extends the length of the order code field and converts basic instruction words to channel or extracode instruction words. Channel instructions can only be used withingut-output channel addresses. Extra code instructions perform the more complex and less frequently used arithmetic operations.

Regular instructions can also be functionally subdivided into the following:

- (1) Sequence changing.
- (2) Fetching and storing.
- (3) Modifying.
- (4) Arithmetic and logic.
- (5) Input-output.
- (6) Editing.

Table 2-1. Instruction Classes

Class	Туре	Control
Regular	Basic Extracode Channel Special	Program
Involuntary	Interrupt Counter	Priority
Peripheral	Keyboard Tape	Operator

The sequence changing instructions after the sequence in which the instructions stored in memory are executed. One group, called transfer control instructions, changes the program path as defined by the programmer. The other group, called decision midding instructions, branches to alternate program paths in response to predefined conditions.

The fetching and storing instructions move data, without alteration, from one location to another. One group, called copy instructions, provides a non-destructive transfer of data from memory to the central processor. Another group, called exchange instructions, transposes data between memory and the central processor. One instruction provides a nondestructive transfer of data from the central processor to memory.

The modifying instructions alter the next instruction to be executed by changing the contents of the order code field, address field, or both.

The arithmetic and logic instructions perform numerical computations. One group, called the basic arithmetic instructions, performs addition, subtraction, multiplication, and division in the ONE's complement number system. Another group, called the add and store instructions, performs single or double precision addition and transfers the resultant from the central processor to memory. The incrementing instructions increment a signed quantity, increment its absolute value, or diminish its absolute value by one. One instruction performs subtraction in the TWO's complement number system for angular data and one instruction performs the Boolean AND operation.

The input-output or channel instructions link the interface circuits to the central processor. One group, called read instructions, transfers the total or partial contents of any channel (register) location to the central processor either directly or accompanied by the Boolean AND, OR, or EXCLUSIVE OR operation. Another group of instructions transfers all new or partially new information to any channel location in the same manner.

The editing or special instructions are address-dependent and control the operation of the program. One special instruction, as mentioned previously, controls the extend mode of operation. Other instructions prevent a program from being interrupted or shift and cycle data to the left or right.

2-6, 2, 2 Involuntary Instructions. Involuntary instructions contain two types of instructions: interrupt and counter. The interrupt instructions use the basic instruction word format just as the regular instructions do; however, the interrupt instructions are not entirely programmable. The contents of the order code field and the address field are supplied by computer logic rather than the program. The counter instructions have no instruction word format. Signals which function as a decoded order code specify the counter instruction to be executed and the computer logic supplies the address. The address for these instructions is limited to one of 29 counter locations in memory.

There are two interrupt instructions. One instruction initializes the LGC when power is first applied and when certain program traps occur. The other interrupt instruction is executed at regular intervals to indicate time, receipt of new telemetry or keyboard data, or transmission of data by the LGC. This interrupt instruction may be programmed to test the computer.

There are several counter instructions. Two instructions will either increment or decrement by one the content of the counter location using the ONE's complement number system. Two other instructions perform the same function using the TWO's complement number system. Certain counter instructions control output rate signals and convert serial telemetry data to parallel computer data.

2-6.2.3 Peripheral Instructions. There are two types of peripheral instructions. One type deals with memory locations and the other type deals with channel locations. The peripheral instructions are not used when the LGC is in the LEM. They are used when the computer is connected to peripheral equipment during subsystem and preinstallation system testing. The peripheral instructions are not programmable and are executed when all computer program operations have been forcibly stopped. These instructions are used to read and load any memory or channel location and to start the computer program at any specified address. The peripheral instructions and counter instructions are processed identically.

2-6.3 TIMER. The timer generates the timing signals required for operation of the LGC and is the primary source of timing signals for all LEM systems.

The timer is divided into the areas indicated in figure 2-23. The master clock frequency is generated by an oscillator and is applied to the clock divider logic. The divider logic divides the master clock input into gating and timing pulses at the basic clock rate of the computer. Several outputs are available from the scaler, which further divides the divider logic output into output pulses and signals which are used for gating, for generating rate signal outputs, and for accumulating time. Outputs from the divider logic also drive the time pulse generator which produces a recurring set of time pulses. This set of time pulses defines a specific interval (memory cycle time) in which access to memory and word flow take place within the computer.

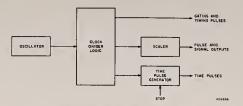


Figure 2-23. Timer, Block Diagram

The start-stop logic senses the status of the power supplies and specific alarm conditions in the computer and generates a stop signal which is applied to the time pulse generator to inhibit word flow. Simultaneous with the generation of the stop signal, a fresh start signal is generated which is applied to all functional areas in the computer. The start-stop logic and subsequent word flow in the computer can also be controlled by inputs from the Computer Test Set (CTS) during pre-installation systems and subsystem tests.

2-6.4 SEQUENCE GENERATOR. The sequence generator executes the instructions stored in memory. The sequence generator processes instruction codes and produces control pulses which regulate the data flow of the computer. The control pulses are responsible for performing the operations assigned to each instruction in conjunction with the various registers in the central processor and the data stored in memory.

The sequence generator (figure 2-24) consists of the order code processor, command generator, and control pulse generator. The sequence generator receives order code signals from the central processor and priority control. These signals are coded by the order code processor and supplied to the command generator. The special purpose control pulses are used for gating the order code signals into the sequence generator at the end of each instruction.

The command generator receives instruction signals from priority control and peripheral equipment and receives coded signals from the order code processor. The command generator decodes the input signals and produces instruction commands which are supplied to the control pulse generator.

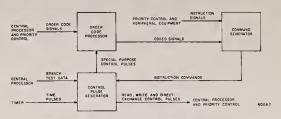


Figure 2-24. Sequence Generator, Block Diagram

The control pulse generator receives twelve time pulses from the timer. These pulses occur in cycles and are used for producing control pulses in conjunction with the instruction commands. There are five types of control pulses: read, write, test, direct exchange, and special purpose. Information in the central processor is transferred from one register to another by the read, write, and direct exchange control pulses. The special purpose control pulses regulate the operation of the order code processor. The test control pulses are used within the control pulse generator. The branch test data from the central processor changes the control pulse sequence of various instructions.

2-6.5 CENTRAL PROCESSOR. The central processor, figure 2-25, consists of the flip-flop registers, the write, clear, and read control logic, write amplifiers, memory buffer register, memory address register, and decoder and the parity logic. All data and ar irrefite manipulations within the LGC take place in the central processor.

Primarily, the central processor performs operations indicated by the basic instructions of the program stored in memory. Communication within the central processor is accomplished through the write amplifiers. Data flows from memory to the flip-flop registers or vice-versa, between individual flip-flop registers, or into the central processor from external sources. In all instances, data is placed on the write lines and routed to a specific register or to another functional area under control of the write, clear, and read logic. This logic section accepts control pulses from the sequence generator and generates signals to read the content of a register onto the write lines and to write this content into another register of the central processor or to another functional area of the LGC. The particular memory location is specified by the content of the memory address register. The address is fed from the write lines into this register, the output of which is decoded by the address decoder logic. Data is subsequently transferred from memory to the memory buffer register. The decoded address outputs are also used as gating functions within the LGC.

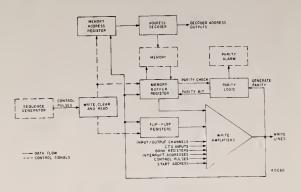


Figure 2-25. Central Processor, Block Diagram

The memory buffer register buffers all information readout or written into memory. During readout, parity is checked by the parity logic and an alarm is generated in case of incorrect parity. During write-in, the parity logic generates a parity bit for information being written into memory. The filp-flop registers perform the data manipulations and arithmetic operations. Each register is 16 bits or one computer word in length. Data flows into and out of each register as dictated by control pulses associated with each register. The control pulses are generated by the write, clear, and read control logic.

External inputs through the write amplifiers include the content of both the erasable and fixed memory bank registers, all interrupt addresses from priority control, control pulses which are associated with specific arithmetic operations, and the start address for an initial start condition. Information from the input and output channels is placed on the write lines and routed to specific destinations either within or external to the central processor. The CTS inputs allow a word to be placed on the write lines during system and subsystem tests.

2-6.6 PRIORITY CONTROL. Priority control is related to the sequence generator in that it controls all involuntary or priority instructions. The priority control processes input-output information and issues order code and instruction signals to the sequence generator and issues twelve-bit addresses to the central processor.

The priority control (figure 2-26) consists of the start, interrupt, and counter instruction control circuits. The start instruction control initializes the computer if the program works itself into a trap, if a transient power failure occurs, or if the interrupt instruction control is not functioning properly. The computer is initialized with the start order code signal, which not only forces the sequence generator to execute the start instruction, but also resets many other computer circuits. When the start order code signal is being issued, the T12 stop signal is sent to the timer. This signal stops the time pulse generator until all essential circuits have been reset and the start instruction has been forced by the sequence generator. The computer may also be initialized manually when connected to the peripheral equipment and placed into the monitor stop mode. In this mode, the time pulse generator is held at the T12 position until the monitor stop signal is released.

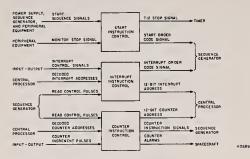


Figure 2-26, Priority Control, Block Diagram

The interrupt instruction control can force the execution of the interrupt instruction by sending the interrupt roder code signal to the sequence generator and the twelve bit address to the central processor. There are ten addresses, each of which accounts for a particular function that is regulated by the interrupt instruction control. The interrupt instruction control links the keyboard, telemetry, and time counters to program operations. The interrupt addresses are transferred to the central processor by read control pulses from the sequence generator. The source of the keyboard, telemetry, and time counter inputs is the input-output circuits. The interrupt instruction control has a built-in priority chain which allows sequential control of the ten interrupt addresses. The decoded interrupt addresses from the central processor are used to control the priority operation.

The counter instruction control is similar to the interrupt instruction control in that it links input-output functions to the program. It also supplies twelve-bit addresses to the central processor and instruction signals to the sequence generator. The instruction signals cause a delay (not an interruption) in the program by forcing the sequence generator to execute a counter instruction. The addresses are transferred to the central processor by read control pulses. The counter instruction control also has a built-in priority of the 29 addresses it can supply to the central processor. This priority is also controlled by decoded counter address signals from the central processor. The counter instruction control contains an alarm detector which produces an alarm if an incremental pulse is not processed properly.

2-6.7 INPUT-OUTPUT. The input-output section accepts all inputs to, and routes to other systems all outputs from, the computer. The input-output section (figure 2-27) includes the interface circuits, input and output channels, input logic, output timing logic, and the downlink circuits.

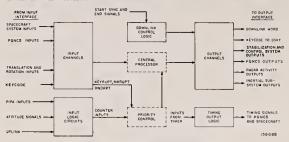


Figure 2-27. Input-Output. Block Diagram

Most of the input and output channels are flip-flop registers similar to the flip-flop registers of the central processor. Certain discrete inputs are applied to individual gating circuits which are part of the input channel structure. Typical inputs to the channels include keycodes from the DSKY and signals from the PGNCS proper and other LEM systems. Input data is applied directly to the input channels; there is no write process as in the central processor. However, the data is read out to the central processor under program control. The input logic circuits accept inputs which cause interrupt sequences within the computer. These incremental inputs (acceleration data from the PIPA's, et cetera) are applied to the priority control circuits and subsequently to associated counters in erasable memory.

Outputs from the computer are placed in the output channels and are routed to specific systems through the output interface circuits. The operation is identical to that in the central processor. Data is written into an output channel from the write lines and read-out to the interface circuits under program control. Typically, these outputs include outputs to the stabilization and control system, the DSKY, the PGNCS, et cetera. The downlink word is also loaded into an output channel and routed to the LEM spacecraft telemetry system by the downlink circuits.

The output timing logic gates synchronization pulses (fixed outputs) to the PGNCS and the LEM spacecraft. These are continuous outputs since the logic is specifically powered during normal operation of the computer and during standby.

2-6.8 MEMORY. Memory (figure 2-28) consists of an erasable memory with a storage capacity of 2048 words and a fixed core rope memory with a storage capacity of 36, 864 words. Erasable memory is a random-access, destructive-readout storage device. Data stored in erasable memory can be altered or updated. Fixed memory is a nondestructive storage device. Data stored in fixed memory is unalterable since the data is wired in and readout is nondestructive.

Both memories contain magnetic-core storage elements. In erasable memory, the storage elements form a core array; in fixed memory, the storage elements form three core ropes. Erasable memory has a density of one word per 16 cores: fixed memory has a density of eight words per core. Each word is located by an address.

In fixed memory, addresses are assigned to instruction words to specify the sequence in which they are to be executed; blocks of addresses are reserved for data, such as constants and tables. Information is placed into fixed memory permanently by weaving patterns through the magnetic cores. The information is written into assigned locations in erasable memory with the CTS, the DSKY, uplink, or program operation.

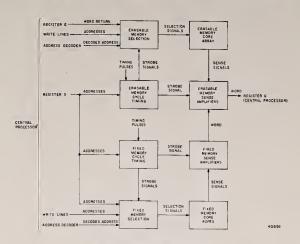


Figure 2-28. Memory, Block Diagram

Both memories use a common address register (register S) and an address decoder in the central processor. When resister S contains an address pertaining to erasable memory, the erasable memory cycle timing is energized. Timing pulses sent to the erasable memory expletiming then produce strobe signals for the read, write, and sense functions. The erasable memory selection logic receives an address and a decoded address from the central processor and produces selection signals which permits data to be written into orread out of a selected storage location. When a word is readout of a storage location in erasable memory, the location is cleared. A word is written into erasable memory through the memory buffer register (g) eighter G) in the central processor by a write strobe operation. A word read from a storage location is applied to the sense amplifiers. The sense amplifiers are strobed and the information is entered into register G of the central processor. Register G receives information from both memories.

The address in register S energizes the fixed memory cycle timing when a location in fixed memory is addressed. The timing pulses sent to the fixed memory cycle timing produce the strobe signals for the read and sense functions. The selection logic receives an address from the write lines, a decoded address and addresses from register S, and produces selection signals for the core rope. The content of a storage location in fixed memory is strobed from the fixed memory sense amplifiers to the erasable memory sense amplifiers and then entered into register G of the central processor.

2-6.9 POWER SUPPLIES. The two power supplies (figure 2-29) furnish operating voltages to the LGC and the DSKY. Primary power of 28 vde from the spacecraft is applied to both power supplies. Regulator circuits maintain a constant output of 44 volts and 44 volts switched from one supply, and +14 volts and +14 volts switched from the other. The regulator circuits are driven by a sync signal input from the timer, each power supply having a different sync frequency. During system and subsystem tests, inputs from the CTS can be used to simulate power supply failures.

The standby mode of operation is initiated by pressing the standby (STBY) pushbutton on the DSKY. During standby, the LGC is put into a RESTART condition and the switch-able +4 and +14 voltages are switched off, thus putting the LGC into a low power mode where only the timer and a few auxiliary signals are operative.

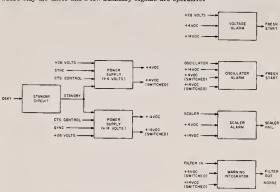


Figure 2-29. Power Supplies, Block Diagram

The voltage alarm circuits monitor the +28, +14, and +4 volt outputs and produce an LGC restart signal (Fresh Start) should any of the voltages deviate from nominal by more than a predetermined amount. The oscillator alarm produces an LGC restart signal (Fresh Start) if the oscillator fails or if the LGC is in the standby mode. The scaler alarm circuit monitors the scaler output of the timer and generates a fail signal if the scaler output fails. The warning integrator monitors certain operations and generates an LGC warning signal (Filter Out) if these operations are frequently repeated or prolonged.

 $2\text{-}6.10\,$  DISPLAY AND KEYBOARD. The DSKY is located below the center panels of the cockpit display and control panels.

The DSKY (figure 2-30) consists of a keyboard; a relay matrix with associated decoding circuits, displays, mode and caution circuits; and a power supply. The keyboard, which contains several numerical, sign, and other control keys, allows the astronaut to communicate with the LGC. The inputs from the keyboard are entered into an input channel and processed by the LGC.

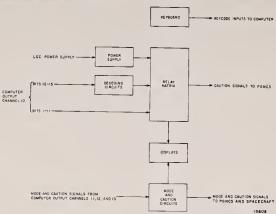


Figure 2-30. Display and Keyboard (DSKY), Block Diagram

MANUAL

The inputs entered from the keyboard, as well as other information, appear on the displays after processing hyprogram. The display of information is accomplished through the relay matrix. A unique code for the characters to be displayed is formed by fifteen bits from output channel 10 in the LGC. Bits 12 through 15 are decoded by the decoding circuits, and, along with hits 1 through 11, energize specific relays in the matrix which causes the appropriate characters to illuminate. The information displayed is the result of a keycode punched in by the astronaut, or is computer-controlled information. The display characters are formed by electroluminescent segments which are energized by a voltage from the power supply routed through relay contacts. Specific inputs from the PGNCS are also applied, through the LGC to certain relays in the matrix through output channel 10 of the LGC. The resulting relay-controlled outputs are caution signals to the PGNCS.

The mode and caution circuits accept direct input signals from channels 11, 12, and 13, without being decoded. The resulting outputs can give an indication to the astronaut on the DSKY and route the output signal to the PGNCS and spacecraft.

#### Chapter 3

#### PHYSICAL DESCRIPTION

#### 3-1 SCOPE

This chapter describes the physical characteristics of the components which components the LEM PGNCS. The locations of the PGNCS components within the LEM are illustrated in figure 3-1.

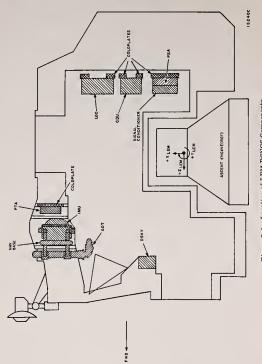


Figure 3-1. Location of LEM PGNCS Components

#### Chapter 3

#### PHYSICAL DESCRIPTION

#### 3-1 SCOPE

This chapter describes the physical characteristics of the components which comprise the LEM PGNCS. The PGNCS components and their locations within the LEM are listed in table 3-1 and illustrated in figure 3-1. The locations of PGNCS component modules are also illustrated and the module functions described.

#### 3-2 PGNCS INTERCONNECT HARNESS GROUP (LEM)

The PGNCS interconnect harness group (composed of interconnect harnesses A and B) interconnects the components of the PGNCS and provides the electrical interface between the PGNCS and other LEM systems. The IMU and PTA are interconnected by harness B. Harness A interconnects the PSA, CDU, LGC, and signal conditioner. The two harnesses are connected to each other by vehicle cables. Table 3-II lists the harness connectors and the components or cable to which they are mated.

Table 3-I. LEM PGNCS Components

Component	Part Number	Location
AOT	6011000	Mounted on nav base on forward struc- ture of LEM with shaft protruding through top of LEM.
CCRD	6014512	Mounted on bracket on side of AOT eyepiece assembly on PGNCS systems below P/N 6015000-061.
		Mounted on spacecraft AOT guard as- sembly on PGNCS systems P/N 6015000-061 and obove.
CDU	2007222 2010744	Mounted on coldplate on center section of after crew compartment wall.

(Sheet 1 of 3)

Table 3-I. LEM PGNCS Components

Component	Part Number	Location
PGNCS interconnect harness group (LEM)	6014515	
Interconnect harness A	6014506	Attached to rear wall of after crew compartment.
Interconnect harness B	6014507	Located in IMU compartment.
IMU and PTA	6010747 6007001	
IMU	2018601 2018699	Bolted to after end of nav base.
PTA	6007000 6010656	Mounted on coldplate on LEM structure immediately aft of IMU/nav base complex.
LEM guidance computer group	6003001	
DSKY	2003985	Mounted on front wall of crew com- partment below LEM display and control panel.
LGC	2003100	Mounted on coldplate on upper section of after crew compartment wall above CDU.
LGC	2003200	Mounted on coldplate on upper section of after crew compartment wall above CDU.
DSKY	2003950	Mounted on front wall of crew com- partment below LEM display and control panel.

(Sheet 2 of 3)



### 3-1A LEM COMPATIBILITY

Compatibility tables 3-1 through 3-IN list the LEM PGNCS components, part numbers, and dash numbers. These tables identify Apollo airborne component configurations and their compatibility to PGNCS applications, and trace Apollo airborne component configuration changes by ECP. The data is organized to assist field site personnel in determining equipment compatibility and to aid in making valid replacement decisions. Table 3-A1 lists the compatibility tables in alphabetical order according to component or assembly. An ECP matrix has also been provided in the table. The matrix is useful for determining which components or assemblies are affected by an ECP.

Table 3-A1. Compatibility and ECP Matrix

																							FCF	Nemi	her								,,,,,																																				
Component of Assembly	Table	1/2	1/2		//	//	//	1	1/	1	//	//	7/	//	//		Z/s	//	//	1/	//	//	1/	//	//	1/	1/2	//	14	//	1/4	//	//	//	1/	1/	//	//	//	//	//	//	//	//	//	//	//	1/1	//		1/	11	//	//	//	//	//	1/	14	1/	1/	//	13/5	1/	1	1:/	1	73	7
AOT	3-1	×	П	П	×	T	П	Ī	П	П	П	×	П	П	Ť	Т	×,	×	T	П	П	1	1	П	Ť	П	1	×	[=	П	П	7	T	×	П	П	П	ŤΙ		Í	П	1		ſΤ	١,	(1)	1	П	1		1	M	П	.		Π,		ĺ	1		П		П	Ĺ	T	1	7	Ť	
ccho	3-1A	П	П					Τ		П	П	T	П		T		П	П			П			П			П		x	П	П	П				П	П	П	T		П	П		×	П	П	П	П	П	П	× x	П	П	x	T		П	T	П	T	П	T	П	T				Т	
CDV	2-70	×	Ш	x.	Ш	1	П		Н	П	П	×	П	$\prod$	I				Τ	×	П	П	Ι	П	×	П		Ι		П						П	П		×		$\prod$	П	×			П			x x				×			x	П	Τ	П		П	T	П			П		Г	×
MU and PTA	3+80		П	П	×	x		4		П	П	x		x x	x	××	П					×		$\prod$	×														T	x						П				x x	к		×	×		×		×	П	x	×	Т	П		П	П		х	Г
Interconnect harness group	3-10	Ц	Ш	Ш	Ш		П	Ш		Ц	Ш		Ш				Ш			Ш	Ш			Ш	X	Ш				Ш	Ш					Ш	Ш	Ш	1		Ш			x		П	×	x	×		x	П	П	x	x						П	T							
LGC group LGC	3+1E	Ц	×	Ш	Ш		x	×	x	×	Ш	x	П				Ш		x x	Ш	×			Ш	x	X 3			,	×	×	x		×	x	x	¥			ŀ	( x )		x			Ш			x		9	×				x			Ш			×			Ш		ı,	x	
DSKY	3-1F		×	П	Ц	1	Ш			Ш	x						Ш	Ш		Ш	Ш			×			Ш	×		Ш			L	×	×	Ш	×	x	x	×	×										1						×		П	×	П	Ţ	×	×	×	4			Γ
LGC group tratallation kit	3-10	Ш	Ш	Ц			Ц			Ш							П		1					Ш					Ш	Ш	Ш			ш		Ш	Ш	Ш			Ш				П	Ш		x							T			×	П					x			П	T	
LOC test modules jumper modules	3-101	Ш	Ш	Ш	Ш		Ш	Ш		Ш	Ш								1					Ш		Ш	Ш		Ш		Ш	Ш				Ш	Ш		L		Ш			Ш	Ш	П												I	Ш			-							
rope modules	3-0	Ц	Ш	П			Ш			П	Ш		Ш	Ш			П													Ш						Ш			Ι		Ш				П					Ш									Ш										
Nev base	2+80		Ш	Ш			Ш			П			П	П			П		1	,	Ш		x							П			×			П					Ш														Ш	П		I	П		Ц								
PSA	3+1L	Ш	×	Ш		×					x	x	П	П	Ι	×	П							П	×			1	Ш	Ш			×		Ш	Ш	Ш	Ш			П	Ш				Ш			×		×	Ш		x X		x			Ц		Ц		Ц		x			L	
Signal conditioner assembly (SCA)	3-1N		П	IJ						П			×	П	Γ		Π									П																						ŀ	х		×			×	ĸ										Ц.		Ш		
Signal conditioner assembly installation kit	3+IN			П		T				П				$\prod$			П									П				П											П				H																				Ш				

The symbol () in the compatibility tables depicts an "OR" gate. Follow one path or the other (not both) for entry or exit from gate.

Table 3-1. AOT Compatibility (Sheet 1 of 2)

Act and and act of	040	DASH N	DASH NUMBERS FOR PN6015000	FOR PN6	015000						CVCTEN	Section of the sectio							
NUMBER	ας	109	021	031	041	003	909	109/120	809	160	019	1	1219	131	141	151	19	12	
6011000	000	×	T -		A	NO													K
	012	H	×	Ţ	A	NO													1
	031	၁	۲	ပ	L	ON													•
	032	၁	Т	ပ	×	ON	1				1								•
	041	D	T	O	<b>A</b>	ON	1	T		1					T				•
	042	ပ	T.	0	4	NO	1	T		Ť	1	T							4
	071	NO			A	H	T	1	1	1								1	1
	072	NO			A	£-	1					1							A
	073	NO			A	Ε.	Ť	1		1								1	<b>A</b>
	074	NO.			A	×	F.	1											4
	081	NO			<b>A</b>	0	÷	<b>A</b>	×	E-		1							•
	091	NO			4	C	H	<b>A</b>	Ö	E-1		1							1
	111	NO -			A	၀	×	<b>A</b>	o	×	T	T							•
				AO.	AOT High Density Filter Assembly Compatibility	Dens	ity Fi	llter A	Assem	bly C	ompa	tibilit	Þ.						
6011856	000					×	1												1
																			•
×	R	Required per print	d per	print															
C	O	Compatible: as good or better than print requirement. See ECP flow chart.	ble: a	is goo	d or b	etter	than p	print 1	requir	remen	t. Se	e ECI	MOIJ d	char.	<b>.</b> ;				
8	M		0000	1	4	-	1	The same			-		-	6 00	J	411.0			

(AOT-CCRD mounting compatibility is required. Reference ECP 422.)

mbly

DESCRIPTION	AOT high density filter asse (sun filter)	AOT reticle lamp change BREAK-IN 612 RETRO 604 through 611	AOT reticle knob change BREAK-IN 612 RETRO 604 through 611	AOT eyeguard plug BREAK-IN 612 RETRO 604 through 611	AOT counter moisture proof and illumination	BREAK-IN 612 RETRO 604 through 611	LIA-8 modifications AFFECTS 602 ONLY	LM-2 modifications AFFECTS 608 ONLY	LM-3 modifications AFFECTS 605 ONLY	AOT pressure seal protection other flammability fixes BREAK-IN 612 RETRO 605 through 611	Conical sunshade and radar shield assembly for AOT BREAK-IN 618	RETRO 605 through 607, 609 through 617	AOT harness protective shiel BREAK-IN 619 RETRO 605 through 607, 609 through 618	Taping of AOT cable assembl RETRO 605 through 618
ECP	512	539	540	542	543		582	596	618	633	657		697	780
DESCRIPTION	Reticle mount and objective lens assembly	Vacuum testing of AOT BREAK-IN 603 Connecting relay assembly	BREAK-IN 602 Thermal instrumentation BREAK-IN 602 ONLY	Corrosion protection of exposed beryllium BREAK-IN 602	Blacken lens edges BREAK-IN 603	Incorporate eyepiece heaters BREAK-IN 603	Change pressure seal material BREAK-IN 603	Incorporate eyepiece locking lever BREAK-IN 603	Reposition eyepiece locking lever BREAK-IN 606 RETRO 605	Modify lens bousing BREAK-IN 605 RETRO 604	CCRD mounting change BREAK-IN 606 RETRO 605	Improved pinning methods BREAK-IN 604	Incorporate shield to eliminate light scatter BREAK-IN 609 RETRO 605 through 608	
ECP	173	197	301	318	320	321	353	360	410	421	422	454	473	

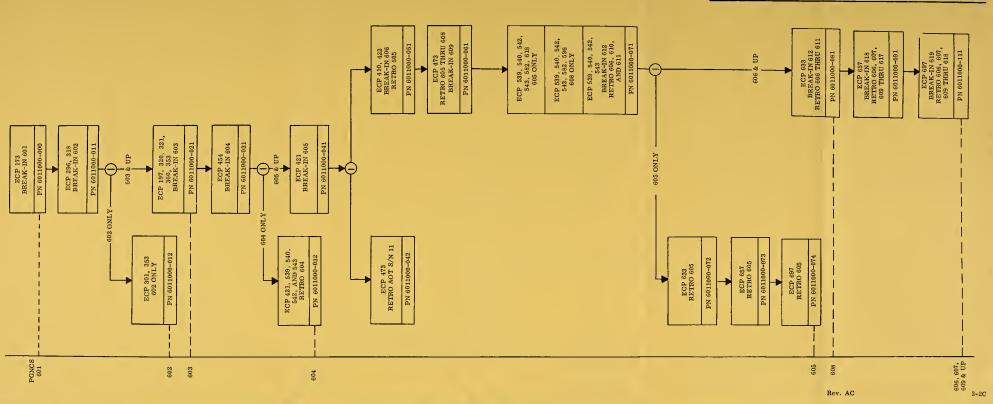


Table 3-I. AOT Compatibility (She

Table 3-IA. CCRD Compatibility (Sheet 1 of 2)

SYSTEM SERIAL NUMBERS 500 091 101 111 121 131 141 614					Required per print Commatthle; as good or better than print requirement. See ECP flow chart.	Not as good as print requirement, but can be used for testing. See ECP flow chart.
021 021 031 041 031 061 051 061 051 061	NO T ON	C NO T	ON C T NO	C NO X	d or better than print requ	t requirement, but can be
011 021 031	F ON	C	C NO	x NO X	Required per print	ot as good as prin
COMPONENT PART NUMBER	6014512 011	031	051	071	X C	

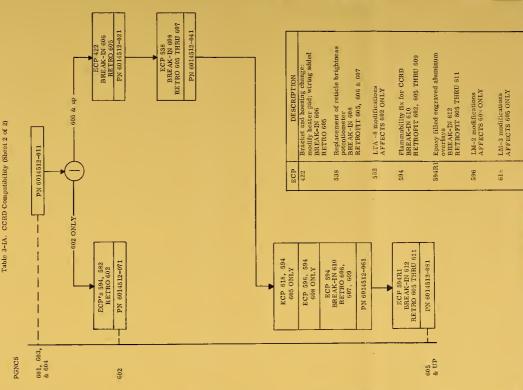
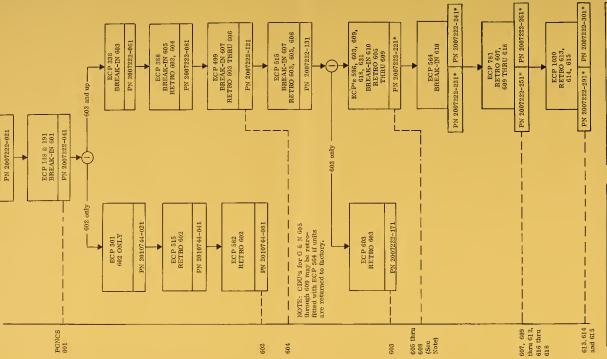


Table 3-IB. CDU Compatibility (Sheet 1 of 2)

2007222 041 X T T X T T X T T X T T X T T X T X T			DASHN	UMBERS	DASH NUMBERS FOR PNGOISOOO	015000						SYSTEM	SERIAL P	SYSTEM SERIAL NUMBERS						
041   X   T	NUMBE	. a	109	021/602	8/	18	/8	18	18	18	18	2	\= @	72	813	10	\g	919	129	619
061   C   T   X   T   X   T   X   T   X   T   X   T   X   T   X   T   X   T   X   T   X   T   X   X	2007222	041	×	T																1
131   C   T   X   T		190	O	H				1			Ť	T	T						T	1
121   C   T   X   T		180	O	H			Ī		Ť	1	1	1	1	1	Ť			T	1	A
131   C   T   X   C   T     221   C   T   C   C   X     221   C   T   C   C   X     221   C   T   C     221   C   T     221   C     221   C		121	C	T	T	×	H	1	T		1	1	T	T	1	Ī	T	T		1
171   C		131	C	H	1	O	E	T	T	T	+	Ť	T		T	Ť	T	T	T	1
221   C   T   C   C   X   X   X   X   X   X   X   X		171	C	H	×	Ö	H	T	1	Ť	+		T	T	T	1	Ī	T	T	1
231   C   T   C   C   T   T   T   T   T   T		221	၁	T	O	O	×	T	T	T	T	Ī		T	Ť	T	T	T	T	1
251   C   T   C   C   T   T   T   T   T   T		241	C	H	O				Ť	T	A	**	T	Ī	Ť	T		T	T	1
251   C   T   C   X   X   X   X   X   X   X   X   X		251	C	T	C			T	Ť	A	×		T	<b>A</b>	E	H	H	×	Ť	1
291   C   T   C   X   X   X   X   X   X   X   X   X		261	C	E	C				1	A	×		T	<b>A</b>	F	Т	L	×	T	1
301   C   T   C   C   X   X   X   X   X   X   X   X		291	၁	Η	O				Ť		+			<b>A</b>	×	×	×	O		1
08.		301	C	H	၁						T			<b>A</b>	×	×	×	O		1
08.	2010744	021		H					T	1	Ť	Ť	T	T	T	Ī	T		T	1
088		041	O	H					1	T	+	Ť	T	T	Ť	T	T	T	Ī	1
		081	O	×	H			T	T	1	1	T	İ		T	T	T		T	A
	×	28	equire	d per	print															
	C	Ö	ompat	ible:	as god	od or l	etter	than	print 1	requi	emen	t. Se	e ECI	MOH C	chart					
	T	Z	ot as	good a	s prir	ıt requ	lirem	ent, b	ut can	be u	sed fo	r test	ing.	See E	CP fle	w ch	art.			
	ON		ANNO	T be 1	sed.															

ECP

191 301 336



of 2)

Table 3-IB. CDU Compatibility (Shect

٦				7							
		DESCRIPTION	LM-2 modifications AFFECTS 608 ONLY	Capacitor replacement in CDU MSA and quadrature rejection module BREAK-IN 610	RETROFIT 603, 605 THRU 609	Elimination of CDU DAC saturation during coarse align mode BREAK-IN 610 RETROFIT 605 THRU 609	LM-3 modifications AFFECTS 605 ONLY	Replace RTV-102 with RTV-109 ECP 631 should be incorporated in	PN 2007222-221. Incorporation of ECP 631 does not cause part number change. It may be included in lower part number assemblies.	CDU bolt change RETROFIT 609 THRU 618	Replace 1010274 transformer in ECDU modules to increase reliability RETROFIT 613, 614, 615, and spares.
_	'	ECP	596	603		609	618	631		781	1030
		DESCRIPTION	Transformer change in CDU CDU mode module change	Add thermal sensors 602 ONLY	Change potting material BREAK-IN 603	Corrosion and outgassing protection BREAK-IN 605 RETROFIT 603, 604	Addition of damper plate BREAK-IN 607 RETROFIT 693 THRU 606	Modify coarse system modules BREAK-IN 607 RETROFIT 602, 603, 605, 606	Implementation of flat pack specifications ND 1002359A and ND 1002358B BREAK-IN 610	LTA-8 modifications AFFECTS 602 ONLY	s 2007232-241, 261, and 301 require les 2007129-051, 2007140-041, and 41-041. If the shove CDU's do not all three modules their PN's are

499

\*CDU's 2007222-941, 261, and 301 require modules 2007124-041. If the above CDU's do not have all three all three modules, their P/N's are 2007222-221, 251, and 291, respecively. CDU's without ECP 564 are completely incredangeable with CDU's containing ECP 564.

515

564\*

582

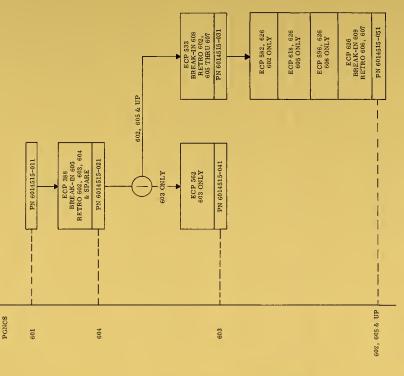
Table 3-IC. IMU and PTA Compatibility (Sheet 1 of 2)

_	- CO	<b>A</b>	*	A	*	A	A	A	A	4	A	A	A	A	4	A	A	A	Ī
	1		†	Ť	t	†	$\dagger$	Ť	+	t	Ť	†	+	$\dagger$	$^{\dagger}$	t	t	†	1
	1919		†	Ť	Ť	Ť	Ť	†	Ť	Ť	Ť	†	×	b	1	1	Ť	+	1
	51 615		1	T	T	Ť	Ť	Ť	Ť	Ť	Ť	Ť	H	×		T	†	Ť	1
	10		Ť		T	T	T	Ť	Ť	$\dagger$	Ť	Ť	T	×	T	Ť	t	Ť	i
	131		†	+	†	+	Ť	†	t	t	Ť	t	<u></u>	×		†	╁	t	1
JMBERS	121		+	+	+	$\dagger$	†	$\dagger$	+	$\dagger$	$\dagger$	+	Ā	<u> </u>	+	$\dagger$	$\dagger$	+	1
SYSTEM SERIAL NUMBERS	100	+	$\dagger$	+	+	+	+	$^{+}$	$\dagger$	+	T.	+	$\dagger$	+	+	$\dagger$	t	t	1
STEM S	93	$\dagger$	+	+	t	+	+	+	+	$\dagger$	A	$^{+}$	$\dagger$	$^{+}$	$^{+}$	$\dagger$	$\dagger$	$\dagger$	
) S	101 608	+	+	+	+	+	+	+	+	+	+	$^{+}$	+	+	+	+	+	+	1
1	88	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	
	109 109	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	
	909	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	1
	190 503	+	+	+	+	+	+	+	+	-L	*×	T	×	Ü	+	+	+	+	
0	150	+	+	+	+	+	+	_		_	_	_	_	_	-	+	+	+	1
1601300	2/	T	T	Ţ	T	T	T	×	S	C	C	O	O	0	T	Η	Η	×	-
FOR PR	031											_				_	_		
UMBERS	021	I	T	Ţ	Ţ	Ţ	T	H	Η	H	۲	Τ	Ţ	H	T	T	T	×	
DASH NUMBERS FOR PREDISOOD	103	×	C	×	Ö	Ö	Ö	Ö	Ö	ပ	Ö	Ö	ပ	ပ	Ö	Ö	Ö	ပ	
TRAG		110	021	120	041	051	190	170	180	160	101	111	121	131	120	031	190	180	
TOAS TARACCAMOS	NUMBER	6007001													2010747				

Compatible: as good or better than print requirement. See ECP flow chart.

Not as good as print requirement, but can be used for testing. See ECP flow chart. CANNOT be used.

Table 3-ID. Interconnect Harness Group Compatibility (Sheet 2 of 2)



DESCRIPTION	Corrosion and outgassing protection BREAK-IN 605 RETROFIT 602, 603, 604 & SPARE	Incorporate uplink wires into harness "A" BER AK-IN 608 RETROFIT 62., 665 thru 607 & TWO SPARES	Replacement of LM-1 harness lacing tape G & N 603 ONLY	LTA-8 modifications AFFECTS 602 ONLY	LM-2 modifications AFFECTS 608 ONLY	LM-3 modifications AFFECTS 605 ONLY	Modification of LEM barness group for flammability protection BREAK-IN 609 FRINGFIT 602, 603*, 605 FRU 608
ECP	388	533	562	582	969	618	626

Table 3-IE, LGC Compatibility (Sheet 1 of 2)

2003100 01	1	ľ			1						STATEM	SERIAL	SYSTEM SERIAL NUMBERS	0			
2003100		109	021	031	103	1000	909	109/	909	609	101	118	121	131	15/0	151	191
2003100	011 thru	T	H		No												<b>A</b>
2003100	190	Ü	υ		No												
2003100	071	ပ	×		No												
2003100	180	×	۲		No												
2003100	160	υ	O		No												1
2003200	011	No	1		No										$oxed{\int}$		
2003200	021	No	1		No			T									1
2003200	031	O	H		H												1
2003200	041	Ö	۲		Į.						1						1
2003200	051	Ö	Ę		T						T						1
2003200	190	υ	H		×									T			1
2003993	011	υ	H		O	۲	ပ	Ţ						T			1
2003993	021	O	H		Į.									Ţ			1
2003993	031	ပ	Ţ		1	1	1	T		T				T			1
2003993	041	O	T		Ţ		T							Τ			1
2003993	051	Ö	Ţ		×		T			T				T			1
2003993	190	O	H		×					T			1				¥
×	Re	equire	Required (Select one of above)	ect on	e of a	(avod											
O	ర	mpat	Compatible: as good or better than requirement. See ECP flow chart.	as goc	od or	better	than	requi	ireme	nt. S	ee EC	JP fle	w che	urt.			
T	ž	ot as	Not as good as requirement, but can be used for testing.	s requ	irem	ent, k	out car	n pe n	ped fc	or tes	ting.		See ECP flow chart.	flow c	hart.		
ON	Ö	ANNO	CANNOT be used.	.bed.													

DESCRIPTION	Incorporation of plastic pads under tray A&B covers	RETROFIT C1 and C2 Wiring change to accommoda	auxiliary memory unit BREAK-IN C8	Addition of jumper wires in t BREAK-IN C3 RETROFIT C1 and C2	Random workmanship vibrati BREAK-IN C1	Manufacture test connector jumpers to ground certain ga	BREAK-IN C8	Paint exposed surfaces on mi spacer BREAK-IN C3 BRETHOFFT C1 and C2	Redesign power supply to ren 28 vdc regulator RRFAK-IV CS	Cut pins on AGC power supply remove 28 vdc regulator BREAK-IN C6 RETROPER C1 than G5	Implementation of flight processes	Implementation of flight proce	ND-1002341 and new dode Correction of computer noise	problem Standby change on computer* BREAK-IN C12 RETROFIT C1 thru C11	Implementation of flat pac specifications ND 1002355 ND 1002358B *	BREAK-IN C13
ECP	447	452		480	470	474		478	485	486	501	505	511	518	564	
DESCRIPTION	Computer module vibration BREAK-IN C1	Aluminum to magnesium conversion of AGC trays BREAK-IN C1	Computer multilayer board layout (MLB) BREAK-IN C1	Redesign of rope & erasable drivers BREAK-IN C1	Redesign power supply module BREAK-IN C1	Redesign of erasable memory BREAK-IN C1	Thermal instrumentation 602 ONLY	Computer wiring changes BREAK-IN 601	Sense amplifier thresbold voltage stability change BREAK-IN C1	Alarm module temperature stabilization of warning integrator and improved oscillator fall alarm BREAK-IN C1	Improved power supply module relays BREAK-IN C1	Clear circuit driver modification BREAK-IN C1	Strobe adjustment BREAK-IN C1	"Clear rope" driver circuit modification BREAK-IN C3 RETROFIT C1 and C2	Replacement of short screws BREAK-IN C3 RETROFIT C1 and C2	
CP	92	26	24	22	82	653	101	22	124	151	898	. 201	103	140	143	

\*LGC Con

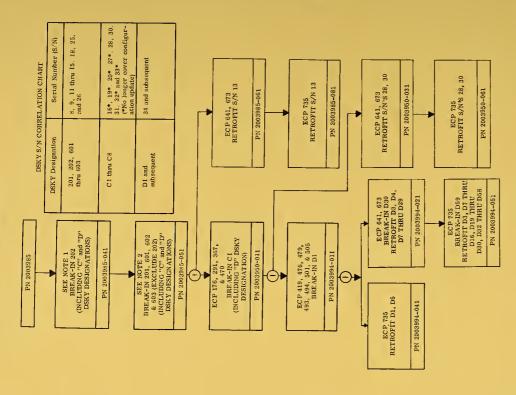
			_	
Tray A	2003092-041 -051 or -061	2003092-041 or -061	2003892-011 2003092-041	
Power	2003200-051 2003121 or 2003892-011 2003092-041 2003888 -051 or -051	2003993-021 2003121 or 2003892-011 2003092-041 -041 2003888	2003892-011	
Logic Module	2003121 or 2003888	2003121 or 2003888	2003888	
DDT	2003200-051	2003993-021	2003993-031 2003888	

Addition of jumper wires in tray A BERKHING SIREKHING SI	Replace RTV-102 with RTV-109. ECP 631 should be incorporated in PN 2003933-031 and above. ECP 631 does not fleet part. mumber charge. It may be included in other part number assemblies.	Alarm module modification, V-fail detection BREAK-IN C32, C4, C5, C6, C C9, C10, C12, C23, C24, C13 thru C22, C25 thru C37
4774 4774 485 505 505 504 504 604	631	719

3-2M

Table 3-IF. DSKY Compatibility (Sheet 1 of 2)

	918	4 4 4 4 4 4 4 4 4	_		-
	<u>ē</u> /8	111111			
	151				
	100			ır.	
1	131			ow ch	
UMBERS	219			charr PP fic	
SERIAL P	119			tiow	
SYSTÉM SERIAL NUMBÉRS	101			ECP	,
	609			Compatible: as good or better than requirement. See ECP flow chart. Not as good as requirement. But can be used for testing. See ECP flow chart.	
П	809			ed for	
	2000			equire he us	
$\ \cdot\ $	18			han re	
	198			tter t	
000	60.08	***************************************		or be	
DASH NUMBERS FOR PN6015000	8			good	ģ.
ERS FOR	200			3: as	CANNOT be used.
NUMB	8	7 7 7 6 6 × 7 7 7 7 7 7 7 7 7 7 7 7 7 7	per	roo	OT b
DASH	109	H H H M O O O O O O O O	Required	ompa	ANN
1040		021 031 061 061 001 011 061 061	H	O Ž	Ö
Take Talacource	NUMBER	2003985 2003985 2003950 30, 31 2003994 2003994	×	O F	NO



## NOTES

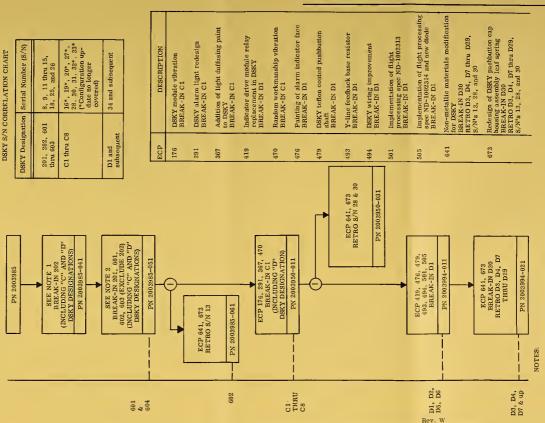
- Potted modules & housing change.
   No ECP number
- Housing change. No ECP number

DESCRIPTION	DSKY wiring improvement BREAK-IN D1	Implementation of flight processing spec ND-1002313 BREAK-IN D1	Implementation of flight processing spec ND-1002314 and new diode BREAK-IN D1	Non-metallic materials modification for DSKY BREAK-IN D30	KEINO D3, D4, D7 thru D29, S/N's 13, 28, and 30	Redesign of DSKY pushbutton cap housing assembly leaf spring BREAK-IN D30 BFTED D3 D4 D7 fbm D39	S/N's 13, 28, and 30 Addition of safety glass to cover	DSKY EL and LI indicators BREAK-IN D59 RETROFIT D1, D3, D5, D7 thru D16, D19 thru D30, D32 thru D58, S/N's 13, 28, and 30
ECP	494	201	505	641		673	735	
DESCRIPTION	DSKY module vibration BREAK-IN C1	DSKY alarm light redesign BREAK-IN C1	Addition of light duffusing paint to DSKY BREAK-IN C1	Indicator drive module relay replacement in DSKY BREAK-IN D1	Random workmanship vibration BREAK-IN C1	Painting of alarm indicator face BREAK-IN DI	DSKY teffon coated pushbutton shaft BREAK-IN D1	Y-line feedback base resistor BREAK-IN D1
ECP	176	291	367	419	470	476	479	193

Table 3-IG. LGC Group Installation Kit Compatibility (Sheet 1 of 2)

TOMOUNT DAD	_	DASH NU	DASH NUMBERS FOR PREDISODO	OR PNEC	00000				1		SYSTEM	SERIAL	SYSTEM SERIAL NUMBERS	2			
NUMBER		109	021	031	2000	051	909	100	981	609	101	10	1219	151	100	151	919
6004000	000	×		1		NO											1
<u> </u>	011	ON	T	1		NO											1
	021	ON		1		H	T	1	NO	H							1
	031	NO		1		NO		1	×	NO							
	041	NO		1		×	1	NO		NO							1
	051	NO		1		NO	1	×	NO	×							1
×	Re	quire	Required per print	print					1								
ပ	ပိ	mpati	Compatible: as good or better than print requirement. See ECP flow chart.	1S goo	d or b	etter	than	print	requi	remer	ıt. Se	e EC	P flow	v char	نہ		
H	No	t as g	Not as good as print requirement, but can be used for testing. See ECP flow chart.	s prin	t requ	irem	ent, b	ut can	n pe n	sed fo	or tes	ting.	See F	CP fi	ow ch	art.	
ON	CA	CANNOT be used.	T he 11	- Pos													

Table 3-1F. DSKY Compatibility (Sheet 2 of 2)

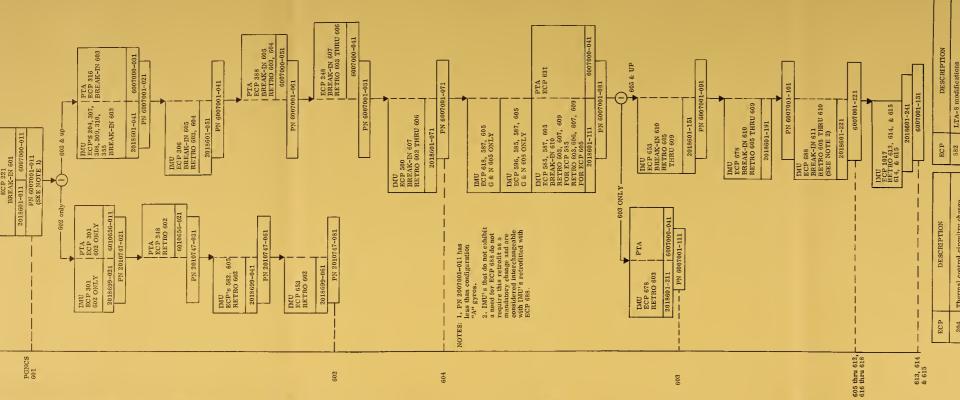


1. Potted modules and housing change.

No ECP number.

Table 3-IG. LGC Group Installation Kit Compatibility (Sheet 1 of 2)

_					
	919	↑ ↑ ↑ ↑			
1	151			ır.	
	100			w cha	
	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		tre tr	P flo	
PBERS	612		mol	e EC	
L NG	2/		20	. Se	
SERIA	110		3 00	ting	
SYSTEM SERIAL NUMBERS	101		*	or tes	
П	603	t o x	, and an	sed for	
П	909	ON X ON	-	be u	
$\ \cdot\ $	109	<b>1 1 1 1</b>	1	ut car	
П	909		thon.	nt, b	
$ \cdot $	0031	ON ON H ON X	Required per print	Not as good as print requirement, but can be used for testing. See ECP flow chart.	
9000	041		3	requ	
DASH NUMBERS FOR PNECIBOOO	031	4 4 4 4 4	nrint 2000	print	ed.
BERS FO	\ 8		Required per print	od as	CANNOT be used.
SH NUR	601	X O O O O O	lired	as go	NOT
$\vdash$	5 /		Kedi	Not	CAN
COMPONENT PART	œ	000 0111 021			
PONEN	NUMBER	000	× (	) H	NO
900		6004000			



DESCRIPTION	LTA-8 modifications AFFECTS 602 ONLY	PIP preamplifier capacitor replacement BREAK-IN 610 RETROFIT 603, 607, and 609	HUG gyro end cap replacement, ECP 587 should be incorporated in PN 6007001-081 and higher, incorpora- tion of ECP 587 does not cause part	number changes. It may be included in Iower part number assemblies.	LM-2 modifications AFFECTS 608 ONLY-	BREAK-IN 610 RETROFIT 602, 603, 605 thru 607	LM-3 modifications AFFECTS 605 ONLY	Replace RTV-102 with RTV-109 ECP 631 should be incorporated in PN 6007001-081 and higher. Incorpora- tion of ECP 631 does not cause part	numher changes. It may be included in lower part number assemblies.	Modification of IMU wiring to reduce IRIG pre-amp oscillation BREAK-IMO 102, 605 thru 609	IRIG end cap change BREAK-IN 610	RETROFIT 603, 605 thru 609  Modification of IMU to reduce	Sporary Sporar	Replace blower motor in IMU to
ECP	582	080	587		596	}	618	631		653	678	688		1017 &
DESCRIPTION	Thermal control circuitry change, BREAK-IN 603	Z axis IRIG rotation BREAK-IN 601	Pulse torque power supply change. BREAK-IN 607 RETROFIT 602 thru 606	Thermocouple addition	Mount harness "B" cable clamp on IMU BREAK-IN 605 RETRO 603, 604	Middle axis assembly clamp changes BREAK-IN 603	Stable member heat transfer change BREAK-IN 603	PIP Temperature reduction and temperature alarm test BREAK-IN 603	IMU cross coupling change BREAK-IN 603	Potting voids BREAK-IN 603	IRIG change BREAK-IN 603	Corrosion and outgassing protection BREAK-IN 605 RETROFIT 603, 604	PIP preamplifier change BREAK-IN 607 RETROFIT 603 thru 606	
ECP	204	221	248	301	306	307	308	309	310	316	355	888	200	

LEM PRIMARY GUIDANCE, NAVIGATION, AND CONTROL SYSTEM

ND-1021042 MANUAL

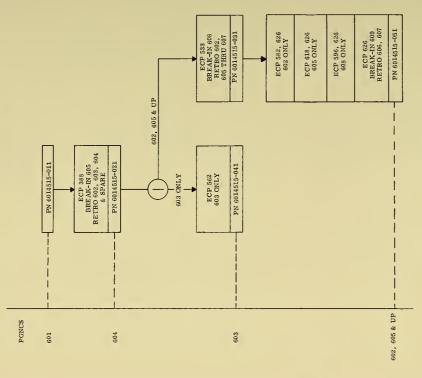
3-21

Rev. AJ

ole 3-ID, Interconnect Harness Group Compatibility (Sheet 1 of 2)

COMPONENT PART	DASHN	DASH NUMBERS FOR PREDISODO	FOR PN6	0012000						SYSTEM	SYSTEM SERIAL NUMBERS	NUMBER						
	109	021	031	041	605	908	021,	909	603	101	119	121	131	41 614	151	919	11/6/17	181
011	ж	T -																1
021	၁	H	A	×	T								T			T		1
031	ပ	T-	A	O	H													1
041	၁	E	×	ပ	€-										T	T		1
051	O	×	0	A	×						T		T	T	T			1
																		}
H	Required per print	ad per	print															
0	Compatible: as good or better than print requirement. See ECP flow chart.	ible:	as go	od or	better	r than	print	requi	remer	nt. Se	e EC	P flow	char	ند				
Z	Not as good as print requirement, but can be used for testing. See ECP flow chart.	good a	ıs pri	nt req	uiren	ent, 1	but ca	n be r	sed fe	or tes	ting.	See E	CP fi	ow ch	art.			
ON	CANNOT be used.	T he	poor.															

Table 3-ID. Interconnect Harness Group Compatibility (Sheet 2 of 2)



\*NOTE: Retrofit of G & N 388 663 with ECP 626 is non-mandatory.

No.   No.	Tool Tubicouron	7000	DASHN	DASH NUMBERS FOR PN6015000	OR PNG	013000						SYSTEM	SERIAL	SYSTEM SERIAL NUMBERS	8			
0211 0211 0311 0411 0611 0611 0611 0611 0611 0611 06	NUMBER		\000 000	78	18	73	100	\g	100	1909	1609	019 101	$\equiv \bigvee$	121	131	191	151	1919
021 041 041 041 041 041 041 041 04	03100	011	T	T		No-				П								A
031 041 041 041 041 041 041 041 041 041	03100	021	[-	Н		No	T											4
041 041 041 041 041 041 041 041 041 041	03100	031	н	H		No												<b>A</b>
051 061 071 081 091 071 071 071 071 071 071 071 07	03100	041	[-	H		No				T	T	T						<b>A</b>
061 081 081 081 081 081 081 081 081 081	03100	051	H	۲		No					7							A
091 091 091 091 091 091 091 091 091 091	03100	061	Ü	C		No	1											A
091 091 021 021 021 031 031 041 041 041 041 041 041 041 041 041 04	03100	071	Ö	×		No	1			T								<b>A</b>
091 021 021 041 051 021 031 041 041 041 041 041	03100	081	×	H		No	1			T		T						A
0111 0511 0511 0611 0611 0611	03100	160	C	ပ		No	T											<b>A</b>
021 031 041 041 021 031 041	03200	011	No-	•		No												A
041 041 051 011 031 031 041	03200	021	No-	1		No												A
041 021 021 031 041 10	03200	031	C	H		E	1											<b>A</b>
051 021 031 041 041	03200	041	C	H		F	1	T		T						T		A
001 0031 0041 0041	03993	051	Ö	F		×	Ť	T	1	T		T						<b>A</b>
031	03993	011	C	T		C	H	O	H	1								<b>A</b>
041	03993	021	C	Ľ		T.	1									T		<b>A</b>
04	03993	031	Ü	۲		×	T	T	T	T						Ţ		A
	03993	041	Ü	H		×				T								A
	×	Ř	equire	d (Sel	ect or	e of	(avoda											
	O	ŭ	ompat	ible:	as go	od or	better	than .	redni	ireme	nt. S	ee E(	OP fle	w cha	art.			
	Н	Ž	ot as	good a	s req	lirem	ent, k	ont ca	n be u	sed fo	or tes	ting.	See	ECP :	flow c	hart.		
	ON	Ü	ANNO	T be u	sed.													

LGC Compatibility (Sheet 2 of 2)

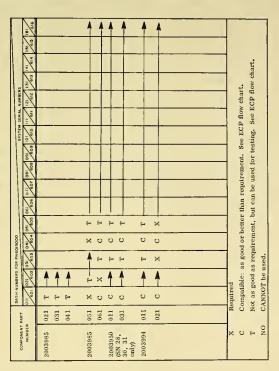
_																
DESCRIPTION	Incorporation of plastic pads under tray A&B covers BREAK-IN C3	RETROFIT CI and C2 Wiring change to accommodate	auxiliary memory unit	Addition of jumper wires in tray A BREAK-IN C3 RETROFIT C1 and C2	Random workmanship vibration BREAK-IN C1	Manufacture test connector jumpers to ground certain gate	BREAK-IN C8	Paint exposed surfaces on mid-tray spacer BREAK-IN C3 RETROFIT C1 and C2	Redesign power supply to remove 28 vdr regulator RREAK-IN CS	Cut pins on AGC power supply to remove 28 vdc regulator BREAK-IN C6 RETROFIT C1 thru C5	Implementation of flight processing spec. BREAK-IN C8	Implementation of flight processing spec ND-1002341 and new diode	Correction of computer noise SCAFAL	problem Standby change on computer* BREAK-IN C12 RETROFIT C1 thru C11	Implementation of flat pack specifications ND 10023594 & ND 100258B *	BREAK-IN C13
ECP	447	452		460	<b>#</b> 20	474	į	478	485	486	201	505	511	518	564	
DESCRIPTION	Computer module vibration BREAK-IN C1	Aluminum to magnesium conversion of AGC trays BREAK-IN C1	Computer multilayer board layout (MLB) BREAK-IN C1	Redesign of rope & erasable drivers BREAK-IN C1	Redesign power supply module BREAK-IN C1	Redesign of erasable memory BREAK-IN C1	Thermal instrumentation 602 ONLY	Computer wiring changes BREAK-IN 601	Sense amplifier threshold voltage stability change BREAK-IN C1	Alarm module temperature stabilization of warning integrator and improved oscillator fall alarm BREAK-IN C1	Improved power supply module relays BREAK-IN C1	Clear circuit driver modification BREAK-IN C1	BREAK-IN C1	"Clear rope" driver circuit modification BREAK-IN C3 RETROFIT C1 and C2	Replacement of short screws BREAK-IN C3 RETROFIT C1 and C2	
ECP	176	226	254	257	258	259	301	322	324	351	368	402	£0.#	440	443	

GC Configuration for ECP 518 & 564

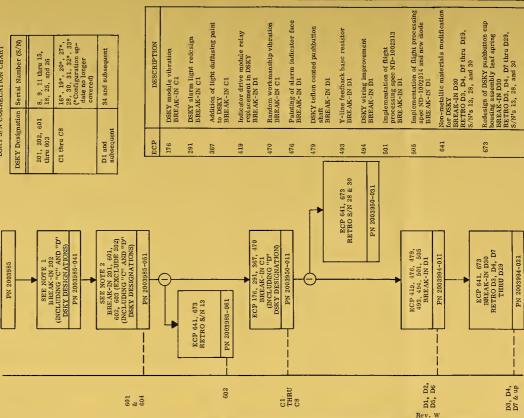
Tray A	2003092-041 -051 or -061	2003092-041 or -061	2003892-011 2003092-041
Power Supply	2003200-051 2003121 or 2003892-011 2003092-041 2003888 -051 or -061	2003993-021 2003121 or 2003892-011 2003092-041 -041 2003888 or -061	2003892-011
Logic Module	2003121 or 2003888	2003121 or 2003888	2003888
DDT	2003200-051	2003993-021	2003993-031 2003888

3-2M

Table 3-IF. DSKY Compatibility (Sheet 1 of 2)



# 16\*, 19\*, 20\*, 27\*, 28, 30, 31, 32\*, 33\* (\*Configuration up-date no longer Serial Number (S/N) DSKY S/N CORRELATION CHART 8, 9, 11 thru 15, 18, 25, and 26 covered DSKY Designation 201, 202, 601 thru 603 C1 thru C8 SEE NOTE 1 BREAK-IN 202 (INCLUDING "C" AND "D" DSKY DESIGNATIONS) PN 2003985-041 PN 2003985



Pottcd modules and housing change. No ECP number,

NOTES:

Housing change. No ECP number. ci.

Table 3-IG. LGC Group Installation Kit Compatibility (Sbeet 1 of 2)

ı	919	<b>^ ^ ^  ^ ^ ^</b>			
	151			art.	
	141			ow ch	
	131		char	CP fl	
HUMBERS	121		wo II o	See E	
SERIAL	18		ECF	ing.	
SYSTEM SERIAL NUMBERS	101		Sec.	r test	
	1609	H NON X	ement	ed fo	
	9091	0 × 0	equir	pe us	
	203/20	A A A	rint r	ıt can	
	909		han p	nt, bu	
1	8	NO X	tter	reme	
2000	041 051		or be	requi	
N PNEO	031	<b>* * * * *</b>	print s good	print	sed.
BENS P	021		per j	od as	pe n
DASH NUMBERS FOR PREGISORO	109	X ON ON ON ON	Required per print Compatible: as good or better than print requirement. See ECP flow chart.	Not as good as print requirement, but can be used for testing. See ECP flow chart.	CANNOT be used.
		0010 0021 0021 0041	S S	Not	CA
COMPONENT PART	NUMBER		×υ	H	ON

Table 3-IG. LGC Group Installation Kit Compatibility (Sheet 2 of 2)

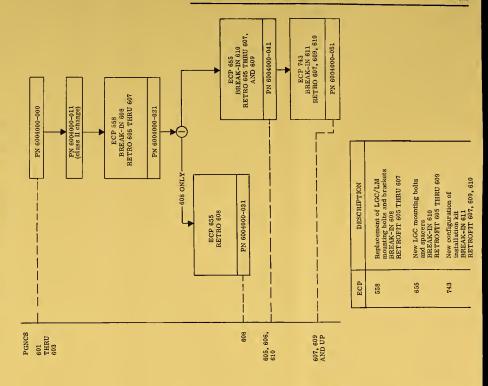


Table 3-IH. Jumper Module (Aurora - PN 2021101) Compatibility

	919	<b>† † †</b>						
	151		uters.					
	141		comp	Use o				
s	131		"C"	ters.				
NUMBER	121		B4 o	ndwo				
SYSTEM SERIAL NUMBERS	1119		n slot	"C" c				
SYSTEM	101		s or i	B6 of npute:			ting.	
	609		puter	and "C		ıt.	or tes	
	909		" com	ots B5 the "C		remer	sed fc	
	1000		pre C	in sle nage		requi	n pe n	
	909		of "1	odule an dar		than	ut car	
١	803		and Be	ots c		etter	ent, b	
	203		B5, 2	ese sl		d or b	urem	
	031		s B4,	in th		s goor	s requ	sed.
I	209/		n slot:	ot us	Ф	ble: a	ood a:	be u
Carolina in Caroli	103	* × ×	* Can be used in slots B4, B5, and B6 of "pre C" computers or in slot B4 of "C" computers.	CAUTION: Do not use 2003076-011 module in slots B5 and B5 of "C" computers. Use of 2003076-011 modules in these slots can damage the "C" computers.	Required	Compatible: as good or better than requirement,	Not as good as requirement, but can be used for testing.	CANNOT be used.
_		021	n be	0-940 0016-0	Re	ပိ	No	CA
COMPONENT PART	NUMBER	2003076	* Ca	2003 2003	×	O	E	ON

Table 3-1J. Rope Module (Aurora Program Assembly) Compatibility

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1		1					-	t	1			
H	"	131		Ī				T	1			
	NUMBER	121			Ī			T	1			
1	SYSTEM SERIAL NUMBERS	139				1		Ī	1			
	SYSTEM	101									ting:	
	ĺ	160				Ī		Ī	1	ţ.	r tes	
		809	I			Ī				remer	sed fo	
П		000 000		Ī		Ī				requi	n pe n	
		909	ĺ	I		I				than	ut car	
		031				I				etter	ent, h	
016000		1000							]	d or !	uirem	
FOR PN6		03								s goo	s requ	sed.
DASH NUMBERS FOR PNEOISOGO		021	-				Ì		P	ble:	g pool	r be u
DASH		601		F	<b>;</b>	<	5	<	Required	Compatible: as good or better than requirement.	Not as good as requirement, but can be used for testing:	CANNOT be used.
3070	PAR		1	011	100	170	100	100	Re	ő	No	
Page Page County	COMPUNENT	NOMBER		2021101					×	ဝ	T	NO

Aurora Program		Mc	Module Part Number and Location	ber and Location	no	
Number	Module B1	Module B2	Module B3	Module B4 (See Note 1)	Module B5 (See Notes 1 and 2)	Module B6 (See Notes 1 and 2)
2021101-011 (Aurora 85)	2003053-061	2003053-071	2003053-061 2003053-071 2003053-081 2003076-021 2003076-021	2003076-021	2003076-021	2003076-021
2021101-021 (Aurora 88) (See Note 3)	2003053-061 or 2003972-011	200353-061 2003053-171 2003053-181 or or or 2003972-011 2003972-091 2003972-111	2003972-011 2003972-091 2003972-111 2003972-111 2003976-021 2003976-021 2003972-091 2003970-091 2003970-091 2003970-091 2003970-091 2003970-091 2003970-091 2003970-091 200397	2003076-021	2003076-021	2003076-021
2021101-031 (Aurora 88)	2003972-011	2003972-091	2003972-011 2003972-091 2003972-111 2003076-021 2003076-021 2003076-021	2003076-021	2003076-021	2003076-021

NOTES: 1. Refer to table 3-IH for jumper module compatibility.

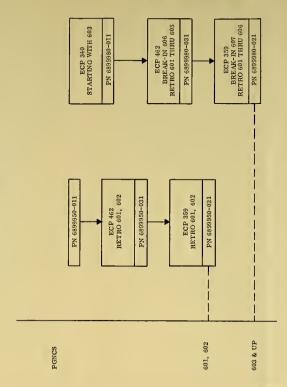
2. Use of modules in slots B5 and B6 is optional.

When 2021101-021 assembly contains all 2003972 configuration modules in slots B1, B2, and B3, the set shall be identified as 2021101-031.

Table 3-IK. Nav Base Compatibility (Sheet 1 of 2)

	919	A	4	<b>A</b>	A	<b>A</b>	<b>A</b>			Γ			
	91 (19		$\dagger$	+	+					 1		ırt.	
	918		T			T	T				ئد	ow cha	
	131										v char	CP fi	
SYSTEM SERIAL NUMBERS	121										P flov	See I	
SERIAL	119										ee EC	ting.	
SYSTEM	101										nt. S	or tes	
	160										ireme	pesr	
	190							 			redn	n pe	
	109/										print	but ca	
	909										than	ent,	
1	603										bette	uiren	
015000	9041										ro bo	at req	
FOR PN6	031	NO -	NO-	NO	NO	×	- ON			 print	as go	s pri	ised.
MBERS	021	A	1	1	<b>A</b>	1	<b>A</b>			d per	ible:	good a	T be 1
DASH NUMBERS FOR PNEOISODO	109	_T	×	H	C	C	C			Required per print	Compatible: as good or better than print requirement. See ECP flow chart.	Not as good as print requirement, but can be used for testing. See ECP flow chart.	CANNOT be used.
PART		011	021	031	011	021	031			E	Ö	Z	
COMPONENT PART	NUMBER	6899950	6899950	6899950	0866689	0866689	0866689			×	၀	H	ON

Table 3-IK. Nav Base Compatibility (Sheet 2 of 2)

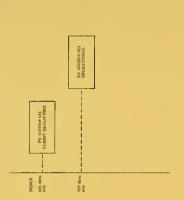


DESCRIPTION	Nav base redesign STARTING WITH 603	Replacement of IMU mounting holts BREAK-IN 607 RETRO 601 thru 606	Addition of ground strap to LM any base BREA-IN 606 BETRO 601 thru 605
ECP	340	359	462

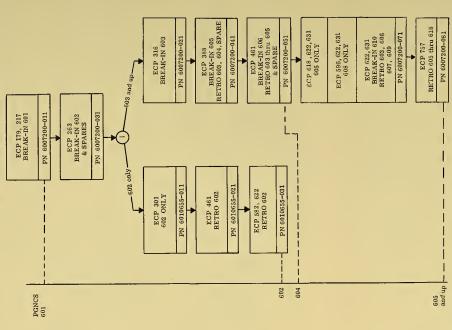
Table 3-IL. PSA Compatibility (Sheet 1 of 2)

ò	ISH NU	DASH NUMBERS FOR PN6015000	OR PN60	000010						SYSTER	SYSTEM SERIAL NUMBERS	NUMBE	Sa			ľ	ŀ
109		203/	603	604	051	606	109/2	1808	100 mg	101	100	121	131	100	161	101	617 181
×		H		F													Ŧ
C		۲		T	T			T								Ī	Ŧ
	Ç	н		T													Ŧ
		н		T												Ţ	Ŧ
		(H	_	×	H											T	Ŧ
-		6-		Ü	T.												Ŧ
	Ö	E		O	×												Ŧ
	E	A		H													-
	-	<b>A</b>		Ţ													Ŧ
	E	×		E													<del></del>
0	uire	Required per print	print														
t H	as g	ole: a	as god s prin	od as	or be	tter ti ent, 1	Compatible: as good as or better than print requirement. See ECP flow chart. Not as good as print requirement, but can be used for testing. See ECP flow ch	n be u	squire	or tes	. Sec sting.	See	flow	ECP flow chart. See ECP flow chart.	hart.		
A	TONI	CANNOT be used.	sed.														

Table 3-LJ. Signal Conditioner Assembly Compatibility (Sheet 2 of 2)







DESCRIPTION	LM-2 modifications AFFECTS 608 ONLY	LM-3 modifications AFFECTS 605 ONLY	Non-metallic materials flammability modification for PSA	RETROFIT 602, 603, 605 and up	Replace RTV-102 with RTV-109. ECP 631 should be incorporated	In PN 5007.200-0/1 and above. ECP 631 does not affect part number change. It may be included in other part number sesemblies.	Design changes to correct LEM PSA reverse power problem	MEXICALL OOD HIR OLD
ECP	296	618	622		631		757	
DESCRIPTION	G and N filter change BREAK-IN 601	Delete signal conditioner power supply assembly	BREAK-IN 601 New helicoil and screw BREAK-IN 602 and spare	Thermal instrumentation BREAK-IN 602	Potting voids in header BREAK-IN 603	Corrosion and outgassing protection BREAK-IN 605 RETROFIT 603, 604, spare 1	Change gimbal servo amplifier BREAK-IN 606 RETROFIT 602 thru 605	LTA-8 modifications AFFECTS 602 ONLY
ECP	179	217	263	301	316	388	461	582

Table 3-IM. Signal Conditioner Assembly Compatibility (Sheet 1 of 2)

	1616	<b>^ ^ ^ ^ ^</b>				
	151			art.		
	141		د	ow ch		
	131		char.	CP fi		
SYSTEM SERIAL NUMBERS	121		P flow	See E		
SERIAL	119		e EC	ting.		
SYSTEM	101		ıt. Se	r tes		
	603	ON N F X	remer	sed fc		
	1809	H X O N	requi	pe u		
	1000	<b>^ ^ ^ ^ ^</b>	rint	ut car		
1	909	ON F X	than p	ent. b		
	903	F X	etter	ireme		
2000	100	× U	l or b	requ		0 90
R PN60	031	* 4	rint s good	print	ed.	0 400
ABERS FC	021	F ×	per pole: a	od as	pe us	do me
DASH NUMBERS FOR PNEOISOOO	109	× 0 0 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0	Required per print Compatible: as good or better than print requirement, See ECP flow chart.	Not as good as print requirement. but can be used for testing. See ECP flow chart.	CANNOT be used.	O de C to also as a state of O
_		021	Co	No	CA	0
TRAS THEOREM	NUMBER		×v	⊣	NO	à

Non-metallic materials flammability modification for SCA BREAK-IN 611 RETRO 602, 603\*, 605 THRU 610

LM-3 modifications AFFECTS 605 ONLY

618

Table 3-IM. Signal Conditioner Assembly Compatibility (Sheet 2 of 2)

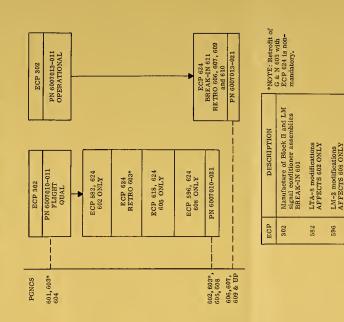


Table 3-IN. Signal Conditioner Assembly Installation Kit Compatibility (Sheet 1 of 2)

	616	<b>A A</b>				
	181				art.	
	141				ow ch	
s	131			char	CP fi	
SYSTEM SERIAL NUMBERS	121			P flow	See E	
A SERIAL	119			se EC	ting.	
SYSTE	101			nt. Se	or tes	
	603	-ON X		reme	sed f	
1	809	× ½		requi	n be 1	
	109	<u> </u>		print	but ca	
	909	N X		than	ent,	
1	0051	<u> </u>		petter	uiren	
DASH NUMBERS FOR PNEOISODO	100			od or	nt req	
FOR PN	031		brind.	as go	as pri	used.
UMBERS	021		ed bez	ible:	good a	T be
DASH	109	× Z	Required per print	Compatible: as good or better than print requirement. See ECP flow chart.	Not as good as print requirement, but can be used for testing. See ECP flow chart.	CANNOT be used.
PART			pe;	0	z	
COMPONENT PART	NUMBER	6007021	×	ပ	H	CN

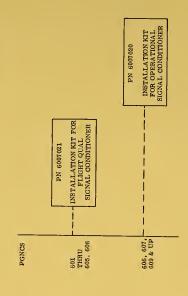
Table 3-I. LEM PGNCS Components

Component	Part Number	Location
Nav base	6899950 6899980	Attached to LEM structure in unpres- surized compartment above astronauts' heads by means of nav base support.
PSA	6007200 6010655	Mounted on coldplate on lower section of after crew compartment wall below CDU.
Signal conditioner assembly (SCA) Flight qualification Operational	6007010-011 6007013-011	Attached to top of PSA.

(Sheet 3 of 3)



Table 3-IN. Signal Conditioner Assembly Installation Kit Compatibility (Sheet 2 of 2)





# 3-2 PGNCS INTERCONNECT HARNESS GROUP (LEM)

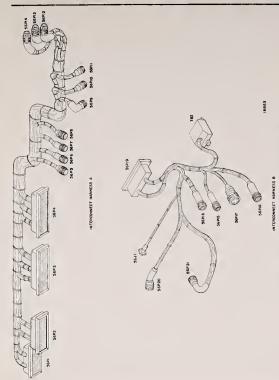
The PGNCS interconnect harness group (composed of interconnect harnesses A and B) interconnects the components of the PGNCS and provides the electrical interface between the PGNCS and other LEM systems. The IMU and PTA are interconnected by harness B. Harness A interconnects the PSA, CDU, LGC, and signal conditioner. The two harnesses are connected to each other by vehicle cables. Table 3-II lists the harness connectors and the components or cable to which they are mated. Figure 3-1A illustrates the PGNCS interconnect harness group.

MANUAL

Table 3-II. PGNCS Harness Interconnections

PGNCS Harness Connector	Component	Component Connector
	Harness A	
56P1	Signal conditioner	30Л1
56P2	PSA	45J19
56P3	CDU	40J53
56P4	LGC	05A1J1*
56P5	LEM spacecraft harness	J221
56P6	LEM spacecraft harness	J220
56 <b>P</b> 7	LEM spacecraft harness	J219
56P8	LEM spacecraft harness	J222
56P9	LEM spacecraft harness	J218
56P10	LEM spacecraft harness	J217
56P11	LEM spacecraft harness	J223
56P12	LEM spacecraft harness	J224
56P13	LEM spacecraft harness	J215
56P14	LEM spacecraft harness	J216
	Harness B	
56P15	LEM spacecraft harness	J226
56P16	LEM spacecraft harness	J227
56P17	LEM spacecraft harness	J228
56P18	LEM spacecraft harness	J225
56P19	PTA	35A2J19
56P20	IMU	35A 1J2
56P21	IMU	35A1J1
56J1	LEM spacecraft harness	P230

<sup>\*</sup> May be designated A51



Rev. J

Figure 3-1A. PGNCS Interconnect Harness Group

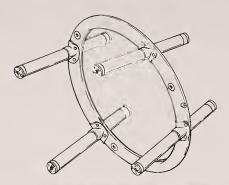


## 3-3 NAVIGATION BASE ASSEMBLY

The navigation base assembly (nav base), figure 3-2 and 3-2A, is a lightweight mount which supports, in critical alignment, the IMU and AOT. The nav base, constructed of one inch diameter, aluminum alloy tubing, weighs approximately three pounds. It consists of a center ring supporting four legs which extend from either side. The ring is approximately 14 inches in diameter and each of the four legs is approximately ten inches long. The IMU is mounted to the ends of the four legs on one side of the ring. The AOT and the abort sensor assembly are mounted to the opposite ends of the legs. The nav base is bolted to the LEM structure above the astronauts' head by three mounting pads on the center ring. An electrical grounding strap is attached to the center ring and to the LEM structure when the nav base is installed in the LEM.

# 3-4 INERTIAL MEASURING UNIT

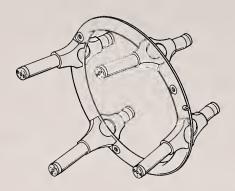
The IMU (figure 3-3) is a three gimbal system designed for movement of the LEM about all axes of the gyro-stabilized inner gimbal (stable member). To provide lightweight, rigid construction, the stable member is machined from a beryllium block and the gimbals are constructed of an aluminum alloy. The weight of the IMU is approximately 42 pounds, and the gimbal case is approximately 12.5 inches in diameter.



15245A

Figure 3-2. Navigation Base Assembly, P/N 6899950

Three Apollo II IRIG's hold the stable member in a stabilized condition. Accelerations along any component of any of the three orthogonal axes of the stable member are sensed by one or more of the three 16 PIP accelerometers. Intergimbal assemblies physically support the gimbals and pass electrical signals between them. The temperature of the IMU is maintained at the desired level by a system of heaters, blowers, and coolant passages. The IMU is pressurized to aid in convection cooling.



17511

Figure 3-2A. Navigation Base Assembly, P/N 6899980

3-4.1 STABLE MEMBER. The stable member, or inner gimbal, is suspended by two intergimbal assemblies inside the middle gimbal. It is free to rotate without restriction about the inner gimbal (IG) axis. Holes are machined in the beryllium block to receive the three Apollo II IRIG's and three 16 PIP's. Accelerometer preamplifiers, stable member, temperature control circuitry and thermostats, a ducosyn transformer, and two safety thermostats are all attached to the stable member.

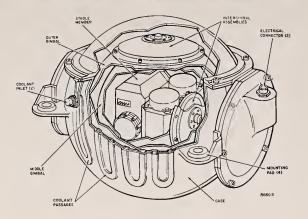


Figure 3-3. Inertial Measuring Unit



3-4.1.1 Gyroscopes. The three gyroscopes (gyros) on the stable member are Apollo II RNIG types. Figure 3-4 shows the location of the gyros on the stable member.

Ducosyns are used for magnetic suspension of the gyro rotor and for signal and torque generation. The signal generator ducosyn is located at one end of the float; the torque generator ducosyn is located at the other end.

The gyro wheel assembly operates as a hysteresis synchronous motor. The hub of the wheel is made of beryllium and the rim is made of heavy steel. This method of construction concentrates the weight at the rim, giving the wheel a high inertial moment.

3-4.1.2 <u>Accelerometers.</u> The LEM IMU uses three 16 PIP devices for sensing acceleration. Figure 3-4 shows the orthogonal placement of the 16 PIP's on the stable member. The 16 PIP is basically a cylindrical float with a pendulous mass unbalance and is pivoted with respect to a case. Ducosyns are located at each end of the float for magnetic suspension and signal and torque generation.

3-4.1.3 Stable Member Mounted Electronics. Table 3-III gives the locations and functions of electronics modules which are mounted in the 1MU.

3-4, 2 MIDDLE GIMBAL. The middle gimbal is suspended by two intergimbal assemblies inside the outer gimbal. It, in turn, supports the stable member. Slip ring assemblies in the intergimbal assemblies provide a means of carrying electrical signals between the outer gimbal and the stable member.

3-4.3 OUTER GIMBAL. The outer gimbal is similar in configuration to the middle gimbal, being suspended inside the supporting gimbal, or case, by two intergimbal assemblies. The outer gimbal has two thermostatically controlled axial-flow blowers mounted in its walls to force air from the vicinity of the middle gimbal to the walls of the case, where heat is carried away by a coolant solution circulating through passages in the case.

3-4.4 SUPPORTING GIMBAL. The supporting gimbal (case) is a spherical enclosure which supports the three gimbals described in the preceding paragraphs. The outer gimbal is suspended inside the case by two intergimbal assemblies which allow complete freedom of rotation. The walls of the case contain coolant passages through which a water-glycol solution is circulated to dissipate heat generated by inertial components and electronic modules. Two quick-disconnect fittings connect the coolant passages to the LEM coolant supply. The case is surrounded by insulating material to prevent condensation of moisture on the coolant passages.

Electrical interface between the IMU and the remainder of the PGNCS is accompleted by two electrical connectors on the case. A precision resolver alignment assembly module and a blower control relay are mounted on the resolver inter-gimbal assembly of the outer gimbal. Their functions are described in table 3-III. The resolver alignment assembly is accessible from outside the case.

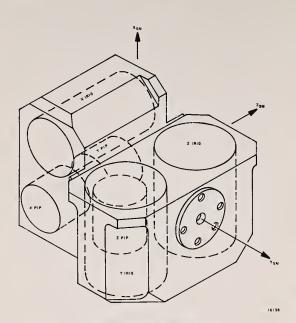


Figure 3-4. IMU Stable Member

Table 3-III. Locations and Functions of IMU Electronics

Module or Component	Part Number	Location and Function
Blower control module assembly	2007171 (system 601 and 602) 2007172 (system 603)	Stable member (SM): Removes power from blower control relay in response to request from blower control thermostat.
Blower control thermo- stat and heater assem- bly	2018635 (system 601 and 602) 2018825 (system 603)	SM: Controls on-off action of blower motors on outer gimbal.
Temperature control module assembly	2007064	SM: Applies power to gyro, accelerometer, and stable member beaters in response to request from temperature control thermostat.
Temperature control thermostat and heater assembly	2018637	SM: Controls operation of tempera- ture control module to maintain proper beat in inertial components.
Stable member heater assembly (2)	2018641	SM: Supplement heat generated by inertial component heaters.
Safety thermostat (2)	1001485	SM: Disable all IMU heaters in the event of an extreme overbeat condition.
Temperature alarm module assembly	2007170	SM: Signals LGC that an overbeat or underheat condition is present.
Temperature alarm thermostat assembly	2018636 (system 601 and 602)	SM: Controls operation of temperature alarm module assembly.
Temperature alarm thermostat and beater assembly (high)	2018823 (system 603)	SM: Controls high temperature over heat condition and operation of tem- perature alarm module.
Temperature alarm thermostat and beater assembly (low)	2018824 (system 603)	SM: Controls low temperature under heat condition and operation of tem- perature alarm module.

(Sheet 1 of 2)

Table 3-III. Locations and Functions of IMU Electronics

Module or Component	Part Number	Location and Function
Ducosyn transformer assembly	2007019	SM: Reduces 28 vac to 2 volts and 4 volts for signal generator excitation of accelerometer and gyro ducosyns, respectively.
PIP preamplifier assembly (3)	2007060 2021269	SM: Amplifies signals generated by accelerometer signal generator. Also provides 45 degree phase shift from reference voltage.
Precision resolver alignment assembly	2007001	Outer gimbal resolver intergimbal assembly: Compensates for design anomalies in intergimbal assembly resolvers.
Blower control relay	1010353-10 (system 601 and 602) 1010353-13 (system 603)	Outer gimbal resolver intergimbal assembly: Applies power to blower motors at request of blower control module assembly.

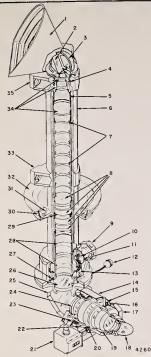
(Sheet 2 of 2)

3-4.5 INTERGIMBAL ASSEMBLIES. The intergimbal assemblies serve five basic purposes: the duplex ball bearings support the gimbal with a minimum of friction, the torque motor drives the gimbal in response to an error signal, the multispeed resolver furnishes signals which represent the angular disposition of the gimbal, the slip rings allow passing of electrical signals from the stable member to the external connectors, and the gyro error resolver (inner gimbal only) transforms gyro error signals into gimbal angle error signals.

#### 3-5 ALIGNMENT OPTICAL TELESCOPE

The AOT (figure 3-5) is a manually operated, periscopic, optical instrument located in the forward structure of the LEM. It is mounted on the nav base with the shaft axis parallel to the LEM X axis, and the upper portion of the shaft protruding from the top of the LEM.

Physically, the AOT is an L-shaped structure formed by the perpendicular intersection of two major assemblies. These assemblies are the telescope shaft and the



- 1. Sunshade
- 2. Head prism 3. Head prism housing
  - assembly
- 4. Ball bearings
- 5. Inner housing assembly
- 6. Outer housing assembly
- 7. Light baffles (7)
- 8. Relay lenses
- 9. Shaft positioning knob
- 10. Shaft positioning gear
- 11. Detent disc spring
- 12. Pl connector to CCRD 13. Shaft gear and slotted detent
- 14. Heater protective cover
- 15. Worm and gear housing
- assembly
- 16. Focus control handle
- 17. Reticle positioning knob
- 18. Rubber eyeguard
- 19. Eyepiece lens assembly
- 20. Reticle drive worm gear
- 21. Angle counter and cover
- 22. Reticle drive gear
- 23. Ball bearings
- 24. Reticle and cover ring
- 25. Mirror
- 26. Pressure sealing window
- 27. Ball bearing
- 28. Light baffles (4)
- 29. Aperture
- 30. Flameguard bellows
- 31. Rubber pressure seal
- 32. Pressure sealing vehicle
- 33. Nav base and ASA mounting pads (2)
- 34. Objective lenses
- 35. Nav base and ASA mounting pads (2)

42602C

telescope eyepiece. The major assemblies are jointed by a hortzontal flange joint at the base of the telescope shaft assembly. In general, structural components such as housings and mounts are machined beryllium, spacers are aluminum, and threaded parts that engage beryllium are made of corrosion resistant steel. On AOT 6011000-041 and above, a radar shield is mounted on the prism shield plate to keep light reflected by the rendezvous radar antenna from entering the AOT optical system. On AOT's 6011000-073 and -091, the prism shield and radar shield are removed and replaced with the conical sunshade and radar shield are semoved and restatached to the inner housing assembly.

3-5.1 TELESCOPE SHAFT ASSEMBLY. The telescope shaft assembly consists of a stationary outer housing assembly and a rotatable inner housing assembly. It contains the shaft positioning mechanism assembly, most of the AOT optics, and a prism shield.

The inner housing assembly is bearing mounted within the outer housing assembly with the vertical axes of both assemblies coincident. This mounting permits the inner housing assembly to be rotated through 360 degrees about the shaft axis. Six detent positions are provided to lock the shaft at each 60 degrees of rotation. Orientation of the inner housing assembly is accomplished by manually turning the shaft positioning knob (figure 3-5A). By positioning the shaft, the head prism (mounted in a fixed position to the inner housing assembly) is positioned to the desired field of view or behind the protective prism shield.

3-5.1.1 Outer Housing Assembly. The outer housing assembly is a beryllium cylinder approximately 27 inches long with a 3-inch bore diameter and a wall thickness of about 0.100 inch. It houses the shaft positioning mechanism and shaft bearings. The outer wall of the cylinder is flanged to accept the rubber pressure seal and flame guard bellows that interface with the outer wall of the LEM bulkhead. Four machined mounting pads, which are used to mount the AOT to the nav base, extend at right angles from the outer wall of the cylinder.

3-5.1.1.1 Shaft Positioning Mechanism. The shaft positioning mechanism consists of a hexagon knob and bevel gear mounted on a common shaft with a pressure seal interposed between them, and a cantilevered detent disc spring with a ball bearing welded on the free end. The shaft positioning mechanism mates with a bevel gear and slotted detent mounted around the outer periphery of the inner housing assembly. The purpose of the shaft positioning mechanism is to provide a means of manually positioning the optios head prism, attached to the inner housing assembly, to each of three viewing positions and a fourth protective position. Each of the three viewing positions if (L), forward (F), and right (R), are set 60 degrees from each other while the prism protective position, closed (CL), is set 180 degrees from the forward position. Two additional positions, LR and RR, which are not used, are located at 60 degrees on either side of the CL position. A look is provided at each position by the welded ball bearing as it slides into the 60 degree spaced grooves of the inner housing assembly slotted detent. For AOT's 6011000-073 and -091, the prism shield is removed and all six viewing positions are utilized.

3-5.1.1.2 Prism Shield. The prism shield is attached to the upper end of the outer housing assembly by two bolts on AOT's 6011000-081, 072, and below. All units above

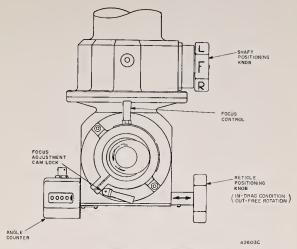


Figure 3-5A. AOT Controls

the 6011000-081 configuration utilize prism shields furnished as GSE. This provides the required protection against damage whenever the conical sunshade and radar shield assembly is not installed. The GSE prism shields, together with the transparent prism and head protection cover, comprise the AOT protective cover set, part number 6014329. This unit primarily functions as a protective shield for the optics head prism against such hazards as micrometeorites, radiation, and dust. The prism shield also acts as part of a labyrinth seal that alds in reducing the evaporation of the shaft ball bearing lubricant. With the head prism facing the rear of the LEM, the shaft closed (CL) position, the prism is completely enclosed by the prism shield. A spacer is mounted between the prism shield and outer housing assembly. This spacer is machined to allow a clearance of only 0.0035 (±0.0015) inch between the inner wall of the prism shield and the head prism mounted.

3-5.1.2 Inner Housing Assembly. The inner housing assembly is a beryllium cylinder which is stepped externally to provide seating and retaining surfaces for the shaft ball bearings and internally for seating some of the shaft optics. A bevel gear and slotted detent, used in positioning the inner housing assembly in the previously described viewing and protective positions, is mounted about the lower periphery of the cylinder. Most of the AOT optics are contained within or mounted atop the inner housing assembly. The optics consist of the head prism, objective lenses, relay lenses, and two sets of light baffles. All of the optics are centrally aligned, axially located, and carried in azimuth rotation about the shaft axis with the cylinder. A special wave washer at the lower end of the shaft provides a predetermined load on the shaft ball bearings.

3-5.1.2.1 Head Prism Housing Assembly. The head prism housing assembly, consists of the head prism, prism housing, and prism mount. It is mounted to the objective lens housing assembly on top of the inner housing assembly. The prism housing and mount are machined beryllium and are held to each other by three bolts. The prism, which is inserted between the housing and mount at 45 degree angle, is held firmly in place by the adjustable force of a leaf spring and epoxy. The leaf spring, located in a recess in the prism housing, is forced to bear down on the rear (hypotenuse) surface of the prism. A U-shaped element, extending upward from the prism mount along the lower face of the prism, acts as a forward retaining surface for the prism. The element also serves as an aperture defining the optics lower field of view. The prism thousing assembly is to gather the impinging light rays of the 60 degree field of view. The prism then refracts these rays through a circular passage in the prism mount, concentric with the optical centerline, to impinge on the first element of the objective lens housing assembly.

3-5,1.2.2 Objective Lens Housing Assembly. The objective lens housing assembly, to which the head prism housing assembly is mounted, its mounted to the upper end of the inner housing assembly cylinder by six bolts. The assembly consists of two doublet lenses, the aspherical field lens, spacers, and retaining rings. The retaining rings hold these optics in radial and axial position. The purpose of the objective lens housing assembly is to minify the light rays received from the head prism by 5 power, and focus these rays at the first focal plane of the AOT. The first focal plane is at the exit side of the aspheric field lens.

3-5.1.2.3 Relay Lens Housing Assembly. The relay lens housing assembly is precisely positioned axially inside the stepped lower portion of the inner housing assembly cylinder. The relay lens housing assembly is held in place by a spacer retained against the stepped inner surface of the cylinder above the assembly and below, by a long spacer and a threaded retainer which mates with the lower end of the cylinder. The assembly consists of two identical lens cells and a spacer held together by a threaded coupling ring. The lens cells are power matched and mutually focused. The purpose of the relay lens housing assembly is to collect the minified image light rays from the objective lens housing assembly and focus them at the second AOT focal plane. This focal plane is coincident with the telescope eyepiece assembly reticle in a vacuum environment for AOT 6011000-021 and above, and in an air environment for AOT 601000-021.

3-5.1.2.4 Conical Sunshade and Radar Shield Assembly. The conical sunshade and radar shield assembly is supplied for installation on AOT's 6011000-073 and 6011000-091. The assembly consists of sunshade and radar shield, clamps, shims, and attaching hardware (1, figure 3-5) for attachment to the inner housing assembly. The assembly is shipped and stored in its own shipping container for installation on the AOT after it has been installed on the spacecraft. The function of the assembly is to prevent stray light which is reflected off the skin of the spacecraft and other reflecting surfaces from entering the optics of the AOT. The assembly makes it possible for the astronaut to perform star sightings without having the reflected light blanking out the light emitted from the stars.

3-5.2 TELESCOPE EYEPIECE ASSEMBLY. Mounted on the lower end of the telescope shaft assembly, the telescope eyepiece assembly is the reticle positioning, angle readout, and target-reticle image viewing portion of the AOT. The assembly consists of a mirror and window housing assembly, a worm and gear housing assembly, and a lens housing and eyequard assembly.

3-5.2.1 Mirror and Window Housing Assembly. The mirror and window housing assembly is a beryllium, 90 degree elbow with two cylindrically flanged ends. It contains an image deflecting mirror and pressure sealing window.

The mirror is machined from 1/2 inch beryllium, heat treated, nickel plated, aluminized, and optically polished. It is mounted in the elbow at 45 degrees to the horizontal eyepiece. This unit provides a means of diverting the target image from the vertical optical centerline of the shaft optics to the horizontal optical centerline of the eyepiece optics.

The window is mounted in a packing ring which is seated in a groove inside the upper portion of the assembly. This unit acts as a seal between the upper AOT components, exposed to the environmental conditions outside the LEM, and the eyepiece optics. Having no optical qualities, the window transmits the target image without change from the relay lens housing assembly directly to the mirror.

3-5.2.2 <u>Worm and Gear Housing Assembly</u>. The worm and gear housing assembly is a beryllium casing containing the reticle and counter drive gear mechanism. AOT reticle, and angle counter. This assembly is mounted to the pressurized end of the mirror and window housing assembly and serves as a mounting receptacle for the eyepiece tens assembly.

The reticle and angle counter drive gear mechanism consists of a transverse worm shaft connected at one end to the angle counter and at the opposite end to the manually operated hexagon control knoh. On AOT 6011000-662 and above, the reticle positioning knob has been equipped with a drag mechanism to prevent free rotation of angle counter when hand is removed. (See figure 3-5A.) The worm shaft meshes with the reticle drive gear. This mechanism provides a means of manually positioning the reticle and transmitting that position to the counter where it is read out in terms of angular displacement.

The counter is a continuous readout counter. The counter provides angular readouts from 000.00 degrees to 359.99 degrees. The resolution of the counter is \$0.01

degree (equivalent to ±36 arc seconds). To preclude the possibility of fogging and corrosion, AOT 6011000-062 and above include a hermetically sealed counter with wedge lighting for ease in viewing.

The reticle is positioned at the second focal plane between two plano-plano (glass) dises. The reticle pattern is etched on the surface of one dise and covered by the other disc for protection. The reticle discs are secured with epoxy in a cover ring which is then clamped at three points in the drive gear for planar adjustment. The reticle drive gear, mounted on ball hearings in the housing assembly, provides precision positioning of the reticle in coincidence with the angle counter readout.

In AOT 6011000-021 and above the reticle is positioned so it is in focus under vacuum conditions. The difference in indices of refraction for vacuum and air under normal conditions causes the target to focus at a plane that is not coincident with the reticle when the AOT is used in an earth environment. When in an earth environment, either target or reticle can be brought into focus with the eyepiece, but both cannot be brought into focus simultaneously.

Ten miniature lamps are mounted about the periphery of the reticle to supply the reticle with edge lighting. For AOT 6011000-062 and above, the ten miniature lamps have been painted red to preclude false star indications caused by imperfections in the reticle. A star appears white, while reticle imperfections appear red. To preclude the possibility of fogging because of the presence of moisture and low temperatures, AOT 6011000-021 and above include an electrical heater on the eyepicce assembly. On AOT's 6011000-051 and above, a heater protective cover and reticle lamp protective cover have been installed.

3-5.2.3 Lens Housing and Eyeguard Assembly. The lens housing and eyeguard assembly is a beryllium cylinder containing the eyepiece lens assembly and focusing mechanism, and a rotatable rubber eyeguard. The assembly is inserted into and attached to the worm and gear housing assembly. This assembly is the image exit portion of the AOT.

The eyepiece lens assembly consists of three lens doublets of 5 power. This power is matched to the objective lens power providing an image exit power of unity. The eyepiece lenses are contained in a cylindrical aluminum adapter that is attached to the movable focus control handle. The aluminum adapter moves the eyepiece lenses axially in the housing when driven by the manually operated focus control handle it thus focuses the viewed image to the exit pupil. The focus control handle protrudes from a helical slot in the lens housing. In AOT 6011000-021 and above, a focus adjustment cam lock (located below and to the left of the eyepiece) can be swiveled, rotating a cam to lock the focus adjustment in a selected position. When the handle is returned to the in-line position, the cam lock is released.

A rotatable eyeguard is fastened to the end of the eyepiece lens assembly. It is made of non-toxic synthetic rubber and is axially adjustable for head position. The adjustment allows for differences in facial contours. The rotatable eyeguard is used when the astronaut takes sightings through the AOT with his face mask opened.

A fixed eyeguard is cemented to the image exit end of the long eye relief (LER) eyepiece lens assembly (figure 3-5B) in AOT 6011000-041 and above. It is made of non-toxic synthetic rubber in an annular shape. The rotatable eyeguard is removed from the AOT when the astronaut takes sightings with his face mask closed. During these sightings, the fixed eyeguard prevents marring of the face mask when pressed against the eyepiece lens assembly.



Figure 3-5B. AOT Eveguard Assemblies

3-5.2.4 AOT High Density Filter Assembly. The AOT high density filter assembly (figure 3-5C) is supplied as a piece of auxiliary equipment to be used in the Apollo mission. The assembly consists of a retainer assembly and high density filter. The retainer assembly contains two lever assemblies mounted on a flexible pivot. The lever assemblies grip the threaded portion of the fixed eyequard when installed in place of the rotatable eyequard. (See figure 3-5B.) The function of the assembly is to prevent damage to the astronaut's eyes by accidental direct viewing of the sun.

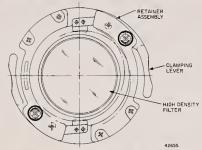


Figure 3-5C. AOT High Density Filter Assembly

## 3-6 COMPUTER CONTROL AND RETICLE DIMMER ASSEMBLY

The computer control and reticle dimmer assembly (CCRD) (figure 3-6) provides the astronaut the capability of adjusting the brightness of the AOT reticle lamps when taking a star sighting and of marking his target with a MARK-X or MARK-Y pushbutton to obtain the optical angular measurements. The CCRD is approximately 3-3-8 inches high, 4-3/6 inches wide, and 2-1/2 inches deep and weighs approximately three pounds. The CCRD is mounted by means of a bracket to the right side of the AOT eyepice assembly on PGNCS systems P/N 6015000-051 mounted on the spacecraft AOT guard assembly on PGNCS systems P/N 6015000-051

Two momentary pushbutton switches, MARK-X and MARK-Y, are used to send discrete signals to the LGC to indicate the time a star crosses the X or Y line on the AOT reticle. A third pushbutton, REJECT, is used to notify the LGC that the previously transmitted mark discrete was incorrect. The pushbuttons are illuminated by a lighting panel consisting of two electro-luminescent lamps.

The reticle dimming circuit consists of a thumbwheel controlled potentiometer which protrudes from the side of the CCRD, two diodes, a control transistor, and a transformer.

The CCRD has two electrical connectors: J1 which mates with the AOT harness and P1 which connects to the LEM harness.

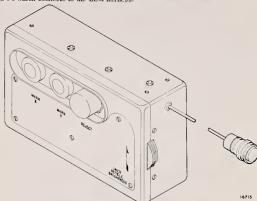


Figure 3-6. Computer Control and Reticle Dimmer

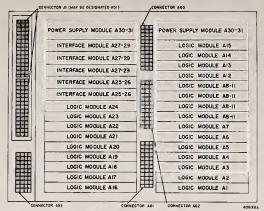


Figure 3-10. Logic Tray A

3-9.1 LOGIC TRAY A. The logic tray A assembly (figure 3-10) contains 31 modules: 24 logic, 5 interface, and 2 power supply modules. All modules are mounted on the tray and then potted with a silastic compound for LGC, part number 2003100, and with a foam for LGC part numbers 2003200 and 2003993. Table 3-VIA gives the part number, function, and location of all modules in logic tray A.

The logic tray A assembly has three intertray connectors (A61, A62, and A63) and two intersystem connectors on the rear. The 360 pin rear connector, J1, connects the LGC to the main 28 wdc power source, to the DSKY, to other components of the PGNCS, and to other LEM systems. The 144 pin rear connector, A52, provides interface with ground support equipment for LGC testing.

LGC's modified by ECP 518 and containing tray A, part number 2003092-041, have wires removed that were used for inhibiting signals STRT1, STRT2, and ALGA; however, the capability for inhibiting STRT1 and ALGA still exists in the GSE.

3-9.2 TRAY B. The tray B assembly (figure 3-11) contains 17 modules, including 6 rope modules. Eleven modules are potted into the tray in a manner similar to that in logic tray A; the six rope modules are plug-in units located at the front of the LGC. The tray B assembly has three intertray connectors (B61, B62, and B63) which interface with those on the logic tray A assembly. Table 3-VIA-1 gives the partnumber, function, and location of all modules in logic tray B.

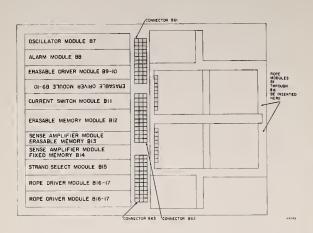


Figure 3-11. Tray B

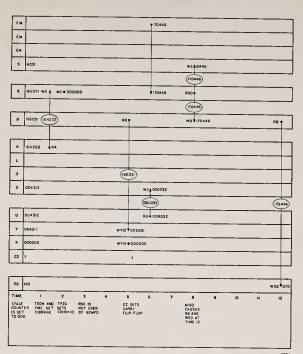


Figure 4-90. Subinstruction BZMF0 with Negative Quantity, Data Transfer Diagram

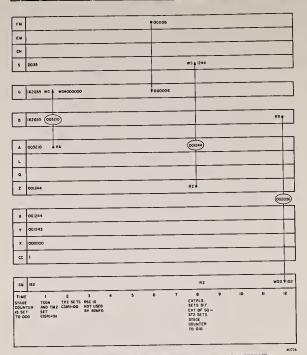


Figure 4-91. Subinstruction BZMF0 with Implied Address Code EXTEND,
Data Transfer Diagram

FM

EM	• 000DZ						00002							
СН						-								
s	0521				WS <b>4</b> 65									
				-		-								
G	170521	wg obbc	100	<b>♦</b> 00000	2		RG				00000	2		
	1						(000002)	4.						
В	170521		WB & 012345	•R8			WB ♥ 0000	202	RB •	wa	000000	2		
		000000	012345					006534		1	(	00000		
А	012345	RSC	на• (	012345							٧	NA 9 0000	00	
L	001700	RSC •	١	WL +012345										
0		RSC .							0000	02) 600	005)			
z	006354	RSC -						RZ •						
U	006534									RU	000002			
Υ	006533								WY TO	000002				
x	000000								WY •	000000				
cı	1									0				
													_	
so	170													
TIME	-	2	3	4	5	6	7	6	9	10		11	12	
STAGE COUNT IS SET TO OC	TER	RSC IS INHIBITED BYADDRESS 0521 IN 3	TSGN SETS CIBR)*OX			FIXED MEMORY STROBE IS INHUBITED BY ADDRESS 0521 IN S	TSON2 SETS C(BR)+00			TSGN SE CIBR) + OF STI SEYS STAGE CO TO OO! NEACON INHBITS AROUND CARRY	UNTER			

Figure 4-92, Subinstruction MPO with Two Positive Numbers, Data Transfer Diagram

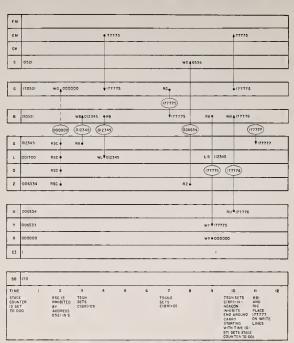


Figure 4-93. Subinstruction MP0 with Positive Number in A and Negative Number in E, Data Transfer Diagram

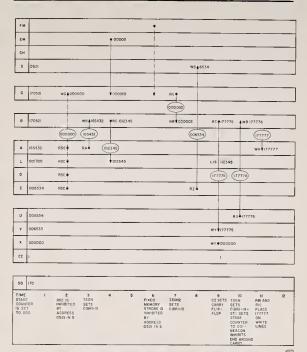


Figure 4-94. Subinstruction MP0 with Negative Number in A and Positive Number in E. Data Transfer Diagram

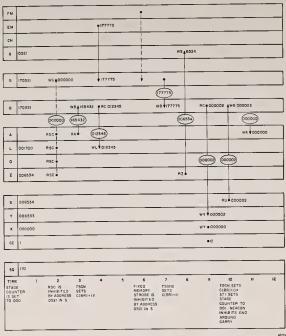


Figure 4-95. Subinstruction MP0 with Two Negative Numbers, Data Transfer Diagram

FM												
ЕМ												
СН												
Ś	6534											
G	177775	L2G0 • 024712	L2G0 • 0	45162	L2GD (	051234	MCRO 4	012247	L260 4	062450	L2GD • 0	34512
в	000002	RB	RB		RB 4		RC •	177775	RB e		RB	
А	000000		000000	WALS 4		WALS.	00000)	WALS 4	071224	WALS 4 016	245	
L	012345	WALS 02LS	022471	WALS 02LS	024516	WALS G2LS	005123	WALS G2LS	77777	WALS G2LS 000	0000	
Q	000	002)	00000	2)	600	005	m	75	6000	XOS	00000	9
Z	006534	000	000	0000	@	600	004)	(1777	77)	(00000)		
U	000002	RU	200000	RU♠	\$00000	RU e	000004	Ru	177777	RU • 000	001 0	00002
Y	000002	WY 00000	2 WY 0	00002	WYD ¥	000004	WY .	177775	wy	000002	w	20002
×	000000	A2X 00001	00 A2× • 0	00000	A2x •	000000	A2× •	000001	A2X •	177777	A2x • 0	0000
CI	0 •	0	•0		_ •	0	•		_ •	0	•0	
_												
	170			_								
TIME STAGE COUNT IS SET TO OO!		2	3	4	5	6	7 CI SETS CARR: FLIP- FLOP	8	9	STI AND ST2 SET STAGE COUNTER TO OH	11	12
		_										40777

Figure 4-96. Subinstruction MPI, Data Transfer Diagram

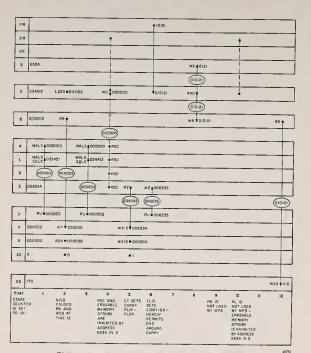


Figure 4-97. Subinstruction MP3, Data Transfer Diagram

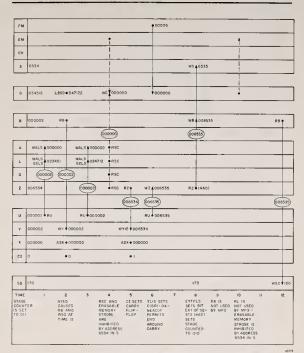


Figure 4-98, Subinstruction MP3 with Implied Address Code EXTEND,
Data Transfer Diagram

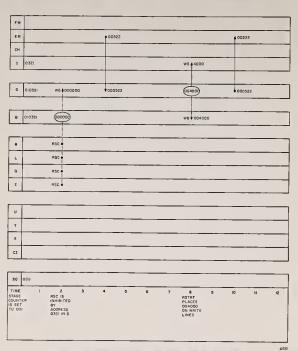


Figure 4-99. Subinstruction GOJ1, Data Transfer Diagram

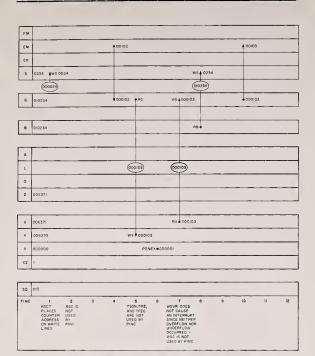


Figure 4-100, Subinstruction PINC, Data Transfer Diagram

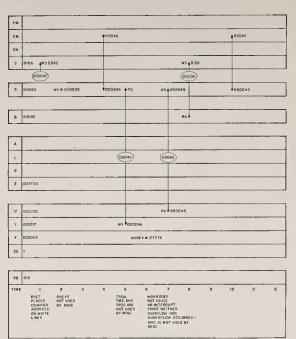


Figure 4-101. Subinstruction MINC, Data Transfer Diagram

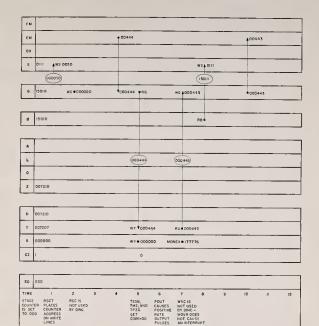


Figure 4-102, Subinstruction DINC with Positive Quantity, Data Transfer Diagram

SINCE NEITHER OVERFLOW NOR UNDERFLOW OCCURRED

SET C(BR)+QQ RATE

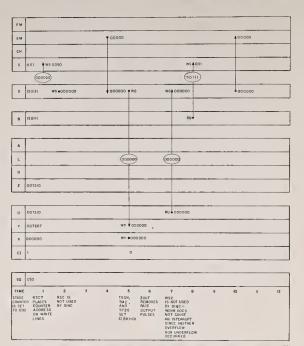


Figure 4-103. Subinstruction DINC with Plus Zero, Data Transfer Diagram

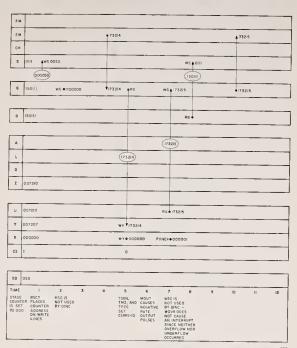


Figure 4-104. Subinstruction DINC with Negative Quantity, Data Transfer Diagram

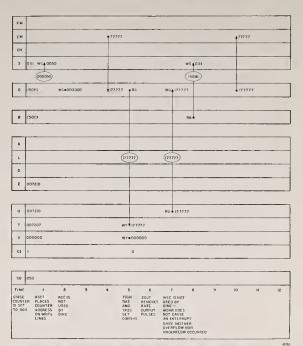


Figure 4-105. Subinstruction DINC with Minus Zero, Data Transfer Diagram

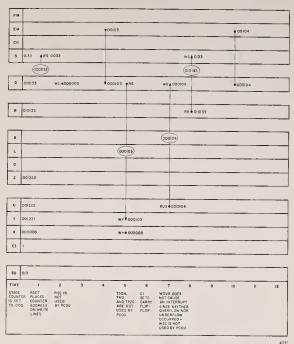


Figure 4-106. Subinstruction PCDU, Data Transfer Diagram

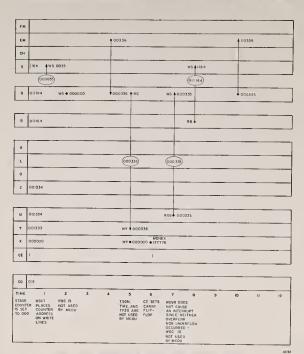


Figure 4-107. Subinstruction MCDU, Data Transfer Diagram

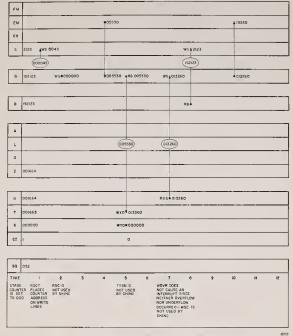


Figure 4-108. Subinstruction SHINC, Data Transfer Diagram

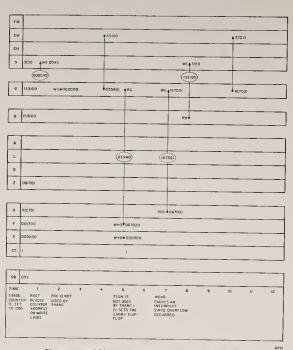


Figure 4-109. Subinstruction SHANC, Data Transfer Diagram

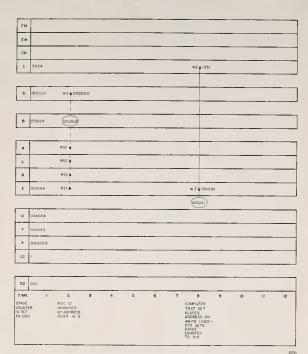


Figure 4-110. Subinstruction TCSAJ3, Data Transfer Diagram

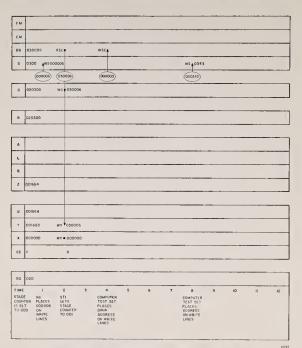


Figure 4-111. Subinstruction FETCH0, Data Transfer Diagram

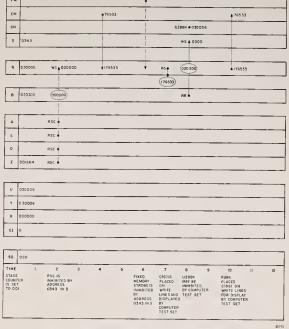


Figure 4-112. Subinstruction FETCH1, Data Transfer Diagram

FM	İ										
ЕМ											
СН	030006	RSC •	wsc.								
s	0400 #WS000	0006					WS 40246				
	(000006)	030006	(00000)				000246				
e	020400	W6 ₹ 030006									
8	020400										
Δ											
L											
0											
Z	001600			_							
U	001600										
Y	ODI577	WY 030006									
×	000000	WY • 000000									
CI	1	0									
-,											
	020										
TIME TAGE OUNTE S SET TO OO!	ON WRITE	STESETS STAGE COUNTER TO OO!	4 COMPUTER TEST SET PLACES BANK AUGRESS ON WRITE LINES	5	6	7	8 COMPUTER TEST SET PLACES ADDRESS ON WRITE LINES	9	10	11	ıs

Figure 4-113. Subinstruction STOREO, Data Transfer Diagram

20794

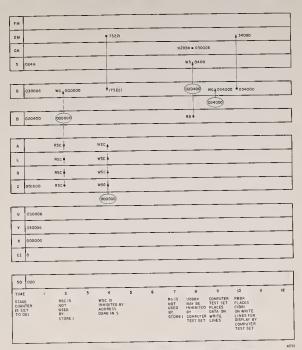


Figure 4-114. Subinstruction STORE1, Data Transfer Diagram

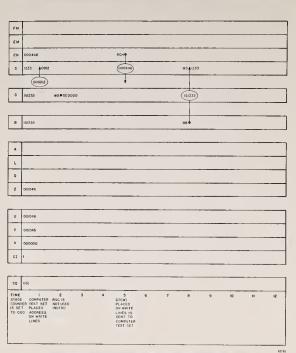


Figure 4-115. Subinstruction INOTRD, Data Transfer Diagram

_								
FM								
EM								
СН	001335		RCH •	WCH <b>4</b> 176	442			
s	3102 4 0014		(001335)		ws <b>4</b> 3102			
	000014			176442				
G	153102				(53102)			
8	153102				RB •			
A								
L								
0								
z	001077							
U	001077					_		
Y	001076							
×	100000							
CI	1							
so	053							
STAGE COUNT IS SET TO OO!	PLACES USED BY	3 4	5 C(CH) PLACED ON WRITE LINES IS SENT TO COMPUTER TEST SET	COMPUTER TEST SET PLACES OF ON WRITE LINES	8 :	9 10	n	12

Figure 4-116. Subinstruction INOTLD, Data Transfer Diagram

4-5.3 TIMER. The timer generates all timing functions required for operation of the computer. In addition, the timer is the primary source of all timing and sync signals for all the spacecraft systems.

4-5.3.1 Timer Functional Description. Timer operation contains the functional areas indicated in figure 4-117. These functional areas include the oscillator, clock divider logic, scaler, time pulse generator, and the sync and timing logic. The oscillator is a crystal controlled, modified Pierce oscillator design that generates a source frequency of 2.048 mc for the clock divider logic. Temperature compensated components in the oscillator circuit maintain a high degree of stability and assure an extremely accurate output frequency to the clock divider logic.

The clock divider logio is further subdivided into the main clock divider, ring outcomer, and strobe pulse generator. The 2.048 mc input from the oscillator is applied to the main clock divider. The main clock divider, divides the input frequency by two and generates the following outputs: clear, write, and read control pulses (CT, WT, RT) which are applied to the central processor to produce the signals necessary to clear, write into, and read out the flip-flop registers; 1.024 mc gating pulses (PHS2, PHS3, PHS4, OVFSTB, TT) which are used throughout the computer; the master clock signal (CLK), a 1.024 mc output used to synchronize the other spacecraft systems; and signal (Q2A which is applied to the oscillator alarm circuit in the power supply to indicate oscillator activity. In addition, the main clock divider supplies signals (RINC A and RING B) to drive the ring counter, and signals (EVNSET and ODDSET) to the time pulse generator. These latter outputs occur at a 512 kc rate, a result of further division of the 1.024 mc gating rate within the main clock divider.

The ring counter generates outputs (P01 through P05) at a 102.4 kc rate. The outputs are 5 mierosecond pulses used for gating and for deriving other timing functions in the computer. Ring counter outputs are also used to derive the strobe pulses (SB0, SB1, SB2, SB4) from the strobe pulse generator. These outputs also occur at a 102.4 kc rate and are 3 microseconds in width with the exception of SB4, which is a 2 mierosecond pulse.

The scaler consists of 33 identical divider stages. The stages are cascaded so that the frequency division is successive. The first stage, driven by signal  $\overline{P01}$  from the ring counter, generates outputs at a rate of one-half the input or 51.2 kec. This output and the remaining outputs through stage 17 (0.78125 pps) are used for timing and gating. The outputs appear as signal outputs from flip-flop circuits (FS01, etc.), and 10 microsecond pulse outputs (F01A, etc.) at the same frequency as the associated stage. Stages 6 through 19 and 20 through 33 form a 28 bit real time word (CHAT01 through CHAT14, CHBT01 through CHBT14) which indicates time intervals up to 23.3 hours.

The time pulse generator, consisting of 12 flip-flop circuits, generates timing pulses  $\overline{101}$  through  $\overline{112}$ . This sequence of timing pulses defines one MCT within the LGC, or a period of 11.97 microseconds, in which word flow takes place. The time pulse generator is driven by inputs  $\overline{EVNET}$  and  $\overline{ODDET}$  from the main clock divider.

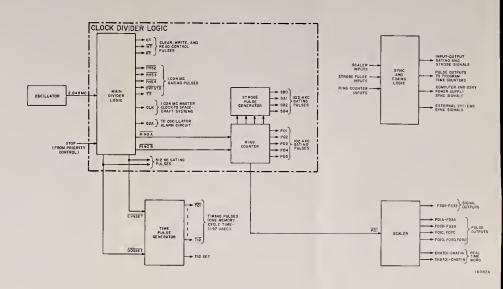


Figure 4-117. Timer, Functional Diagram



Signal ODDSET can be inhibited by signal STOP from priority control. Signal STOP, an input from the CTS during preinstallation system and subsystem tests, inhibits the time pulses from being generated thus preventing word flow in the computer. This feature allows individual memory cycle times to be observed during tests.

The sync and timing logic consists of a gating complex which generates various outputs foruse within the computer, and synchronization signals for systems external to the computer. The inputs to, and outputs from, this section are extensive, and are grouped by function in figure 4-117.

The ring counter, strobe pulse generator, and the scaler supply inputs to the sync and timing logic. These inputs are used to derive gating and strobe signals for the input and output channels, pulse outputs for the program time counters in memory, and synchronization signals for the computer and DSKY power supplies and for systems external to the computer.

During standby operation, the oscillator, clock divider logic, and the scaler appearative and generate the signals associated with these functional areas. However, the significant outputs during this mode of operation are the real time word from the scaler and the synchronization signals to the other spacecraft systems. The real time word continues to be accumulated during standby, and the external systems synchronization signals continue to be generated.

4-5.3.2 Oscillator Detailed Description. The computer oscillator (figure 4-118) generates a master clock frequency of 2.048 mc. The basic oscillator circuit, consisting of crystal Y1, and transistor Q1 and associated components, is a modified Pierce oscillator design. Variable inductor L1, in series with the crystal, compensates for frequency drift due to component aging. The crystal output is amplified by transistor Q1, which operates as a class A amplifier that drives buffer stage Q2. The sinusoidal output of stage Q1 is applied to pulse shaper Q3 and, through capacitor C7, to a dc feedback network. The output of the feedback network controls the peak-to-peak output level of stage Q1. The resultant 2.048 mc square wave output of stage Q3 is amplified by output stage Q4, and is applied to the clock divider logic.

The collector supply voltage for stages Q1 and Q2 is obtained from the +14 volt output (B PLUS) of the power supply. This voltage is applied through resistor R5 and is regulated by zener diode CR1 (rated at 9 volts). The +4 volt power supply output is furnished directly as the collector supply for stages Q3 and Q4.

Two resistor networks (R4, R6, R10, R9, R12 and R2, R3, R7, R8, R11), in conjunction with thermistors RT1, RT2, and RT3 and varicap CR2, comprise the temperature compensation network which improves the stability of the computer oscillator. The regulated output voltage of diode CR1 is applied across the two resistor networks, the outputs of which are applied across varicap CR2. The varicap is a reverse-biased diode that introduces capacitance into the circuit. Any changes in temperature cause a corresponding change in the reverse bias across the varicap thus varying the effective capacitance in series with crystal Y1, which is also affected by the change in temperature.



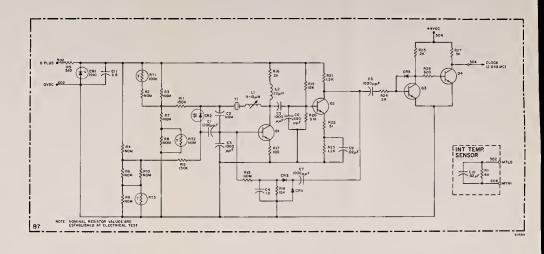


Figure 4-118. Computer Oscillator, Schematic Diagram



4-5.3.3 Clook Divider Logic Detailed Description. The clook divider logic consists of the main clock divider, ring counter, and strobe pulse generator. The main clook divider (figure 4-119, sheet 1) generates outputs at the basic clook rate of the system, 1.024 mc. In addition, 512 kc outputs drive the ring counter and the time pulse generator. The 2.048 mc CLOCK input from the oscillator is applied to the first main clook divider circuit consisting of gates 37101 through 37106. Gates 37101 through 37104 are interconnected in a manner similar to the basic filp-flop circuit of the LGC. Gates 37105 and 37106 function as a filp-flop; however, gates 37101 through 37104 do not. The waveforms in figure 4-19 indicate that an output occurs from only one of the four gates at each positive and negative transition of the clock input. The other three gates remain in ZERO state. Unlike a flip-flop, in which one side is ZERO while the other side is a ONE and vice-versa, this circuit resembles a ring counter. The outputs of these four gates (37101 through 37104) are used to derive the clear control signal (CT), read control signal (RT), and the three 1.024 mc gating pulses (PHS2, PHS3, and PHS4) which are 0.25 microseconds wide.

The outputs from gates 37102 and 37103 drive FF37105-37106, which is alternately set and reset at 1.024 mc rate. The write control signal (WT) and the 1.024 mc master clock (CLK) signal to the spacecraft systems are derived from this flip-flop output. Any failure of the computer oscillator would be most directly indicated by the output of the first main clock divider circuit. Thus, signal Q2A is applied to the oscillator alarm circuit in the power supply to indicate oscillator activity. The output is from an extended NOR gate which has its collector load in the alarm circuit. Figure 4-119 illustrates the timing relationship between the clear and write control signals. The 0.25 microsecond clear pulse is coincident with the first 1/4 microsecond of the 0.5 microsecond write control signal. The read control signal is 0.75 microsecond wide. All three of these control signal outputs are applied to the central processor for clearing, writing into, and reading out of the flip-flop registers. The clear pulse (CT) is used also to derive the overflow strobe signal (OVFSTB), a 1.024 mc gating signal, This output is shown wider than the clear pulse since some propagation delay undoubtedly exists to stretch this pulse slightly beyond 0.25 microsecond before FF37148-37149 resets.

The inverted output of gate 37101 drives the second main clock divider circuit which consists of gates 37111 through 37114 and FF37117-37118. Outputs from this circuit drive the ring counter (RING A, RING B) and the time pulse generator (ODDSET, EVNSET). The outputs occur at a 512 kc rate, and are 90 degrees out of phase with each other (see figure 4-119). This main clock divider circuit is identical in operation to the first main clock divider circuit. Each of the gates 37111 through 37114 generates in succession an output on each transition of the output of gate 37107. Output pulses from gates 37112 and 37113 alternately set and reset FF37117-37118. No output signals are derived from this flip-flop. The outputs to drive the ring counter and the time pulse generator are obtained from gates 37111 and 37114. Signals RING A and ODDSET from 37111 occur coincidentally, and RING B and EVNSET from 37114 occur coincidentally. Signal ODDSET, applied to the time pulse generator, can be inhibited by input STOP from priority control, which prevents any outputs from the time pulse generator and subsequently inhibits word flow in the computer. This feature can be



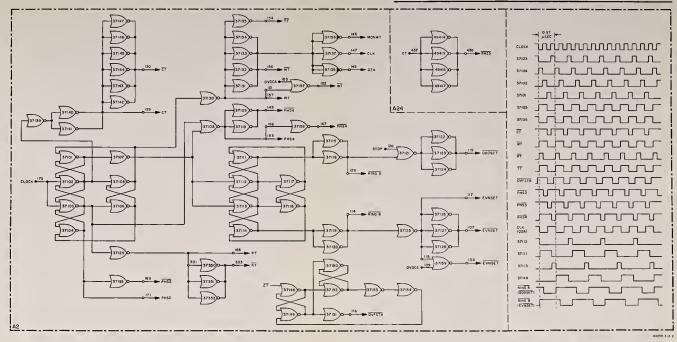


Figure 4-119. Clock Divider Logic (Sheet 1 of 2)



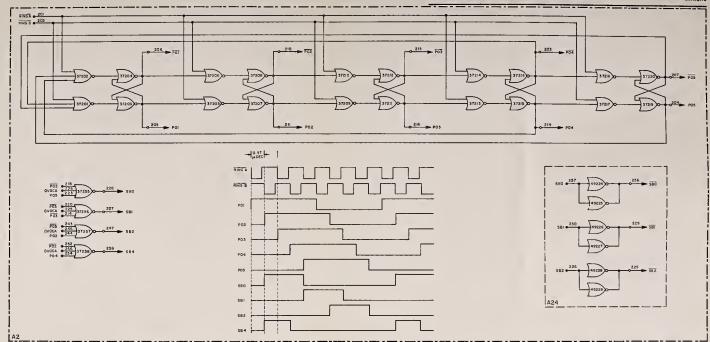


Figure 4-119. Clock Divider Logic (Sheet 2 of 2)



employed during pre-installation system and subsytem tests as a result of a monitor stop (MSTP) input from the CTS.

The ring counter (figure 4-119, sheet 2) consists of five flip-flop circuits with outputs labeled P01 through P05 (and P01 through P05). The ring counter is driven by inputs (RING A and RING B) from the main clock divider. Each of these inputs, described previously, occurs at a 512 kc rate. The ring counter does not accomplish a division-by-two. Rather, the division by the fives stages results in five symmetrical outputs, each at a rate of 102.4 kc and 5 microseconds in width. Successive outputs occur 1 microsecond apart; for example, P02 occurs 1 microsecond after P01 etc.

Strobe pulses SB0, SB1, SB2, and SB4 are generated by signals PO2 through PO5 (and complements) from the ring counter. These strobes are 3 microsecond pulses occurring also at a rate of 102.4 kc, (with the exception of SB4 which is 2 microseconds wide). Strobe signals SB0, SB1, and SB2 are inverted by gates on module A24 (see figure 4-119).

4-5.3.4 Scaler Detailed Description. The scaler, figure 4-120, consists of 33 identical divider stages. The stages are cascaded to provide successive frequency division of the input to the scaler. Stage 2 runs at half the rate of stage 1, stage 3 at half the rate of stage 2, etc. Each of these stages is identical in operation to the main clock divider circuit in the clock divider logic. The input to the scaler, signal POI from the ring counter, occurs at a rate of 102.4 kc. It is applied to stage 1 located on module A2 (the remaining stages of the scaler are located on module A1). Stage 1 divides this input by two and generates outputs at a rate of 51.2 kc. There are five outputs available from stage 1): four pulse outputs (F014 through F01D) from the input gates (37221 through 37224), and one flip-flop output (F87325-37226).

The pulse outputs of stage 1 are 5 microseconds wide. The period of the flipfloop output is approximately 20 microseconds; since the output waveform is symmetrical, the transitions are 10 microseconds apart. The output of the stage 1 flip-flop is the input to stage 2 of the scaler. Stage 2 divides the input by two and generates outputs at a rate of 25.6 kc. Three outputs are available from stage 2: two pulse outputs (F02A, F02B), and the flip-flop output (F802). The pulse outputs of this stage and all subsequent stages of the scaler, regardless of frequency, are 10 microseconds wide. This width is established by the 10 microsecond input from stage 1 to stage 2 and the fact that a pulse output, not the flip-flop output, feeds stage 3 (F02A). The same is true of the output from stage 3 to stage 4 (F03A) and of the succeeding scaler stages.

Figure 4-121 illustrates the output waveforms from stages 1 and 2 of the scaler. outputs from stage 2 are typical of the outputs from the remaining stages of the scaler, with the exception of stages 5, 7, and 9. Stages 5 and 9 have one additional pulse output (F05D, F09D) and stage 7 two additional pulse outputs (F07C, F07D). These outputs are generated by gates on module A24 as indicated in figure 4-120.

Most of the pulse outputs designated A and B, which are positive going, are inted by gates contained in other modules. These gates, and the modules in which they are located, are also illustrated in figure 4-120.



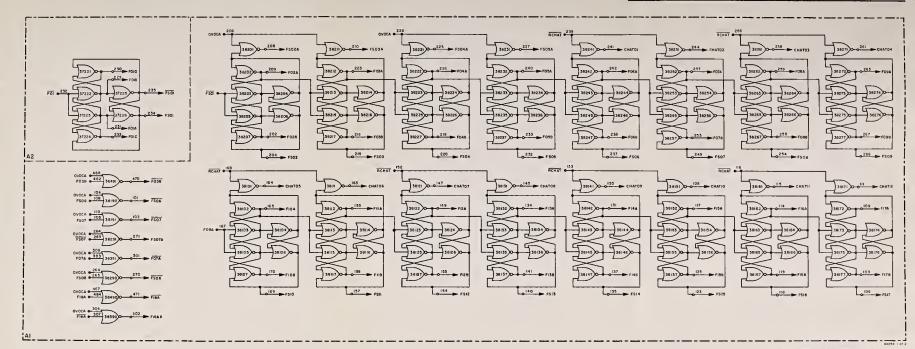


Figure 4-120. Scaler (Sheet 1 of 2)



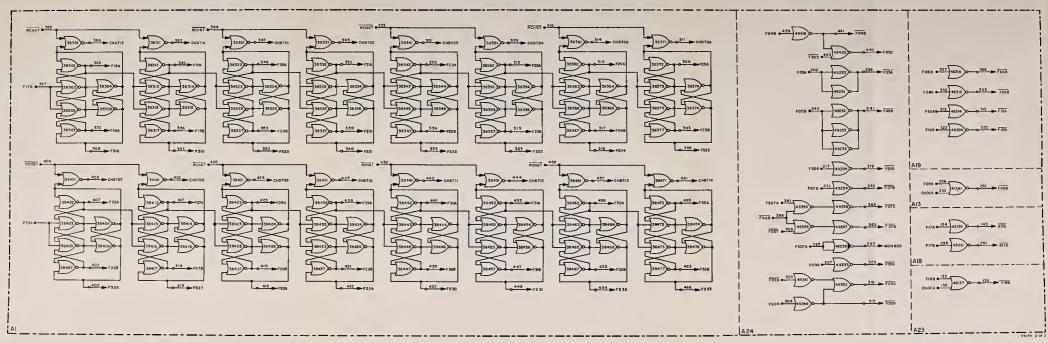


Figure 4-120. Scaler (Sheet 2 of 2)



40592a 1 of 3

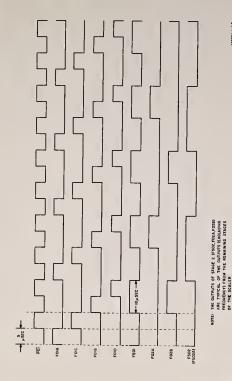


Figure 4-121. Scaler Waveforms (Sheet 1 of 3)



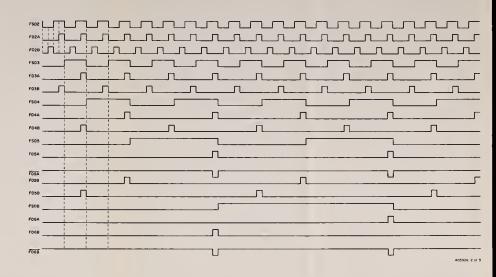


Figure 4-121, Scaler Waveforms (Sheet 2 of 3)



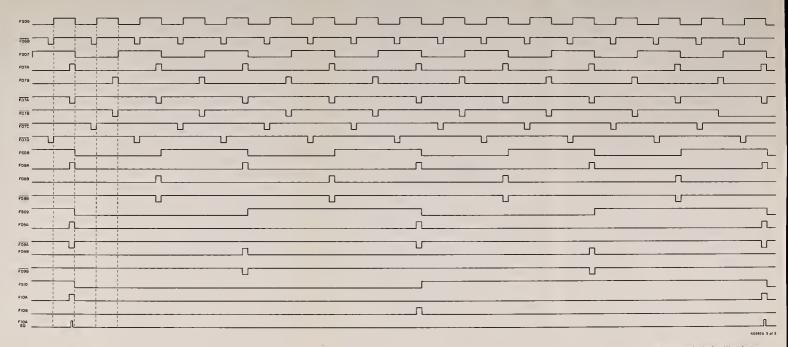


Figure 4-121. Scaler Waveforms (Sheet 3 of 3)



The outputs from stages 1 through 17, at rates from 51.2 kpps to 0.78125 pps, are primarily used to derive timing, synchronization, and gating signals for the LGC and other systems. Table 4-VIII lists the frequency, period, and polarity of the outputs of these stages.

The output of stages 6 through 33 provides an indication of real time in the form of two 14 bit words addressable as two channels that are similar to the channels of the input-output section of the LGC. Stages 6 through 19 provide the 14 bit word to the low order channel CHAT01 through CHAT14, while stages 20 through 33 provide the 14 bit word to the high order channel CHBT01 through CHBT14. The two channels together indicate time intervals up to 23.3 hours, in 624 microsecond increments. Both words are formed by the flip-flop outputs of the respective stages, gated by a read channel signal (RCHAT or RCHBT). Read signal RCHAT, generated under program control as a function of octal address 0004, causes the low order bits (stages 6 through 19) to be placed on the write lines in the central processor; read signal RCHBT, generated under program control as a function of address 0003, causes the high order bits (stages 6 through 3) to be placed on the write lines.

4-5.3.5 Time Pulse Generator Detailed Description. The time pulse generator, consisting of twelve flip-flop circuits, generates timing pulse outputs TOI through TI2. This sequence of pulse outputs defines one MCT within the computer and occupies an interval of exactly 11.97 microseconds, or approximately 12 microseconds. Within this interval, access to memory and word flow take place within the computer.

Each of the timing pulses is generated by an associated flip-flop circuit shown in figure 4-122. The odd numbered outputs (TOI, etc.) are gated by signal ODSET from the clock divider logic; the even numbered outputs (TO2, etc.) are gated by signal EVNSET. Only one pulse output occurs at one time. Consider an initial condition in which signal Ti2 SET is generated. This signal occurs after timing pulses TOI through TII have all been generated. The set output of flip-flops TOI through TII are ORed through gates 37355, 37356, 37357, and 37358. When all these inputs are ZERO, output Ti2 SET is a ONE (coincident with EVNSET) and sets the Ti2 flip-flop (FF37302-37303). The flip-flop reset output is gated by signal EVNSET generating signals T12 and Ti2. Signal MT12 is made available to the CTS when this unit monitors the LGC during tests. When signal ODDSET occurs (0.97 microsecond later), the TOI flip-flop reset output is fed back to reset the Ti2 flip-flop. Simultaneously, signal ODDSET gates the flip-flop reset output generating signals TO1 and TO1. Signal EVNSET occurs 0.97 microsecond after ODDSET and the TO2 flip-flop sets, which in turn resets the Ti0 flip-flop.

The remaining timing pulses are generated in this manner except for the T12 output. Since T12 is generated as a function of the T12 SET signal, there is no feedback from the T12 filp-flop to reset the T11 filp-flop. The T11 filp-flop is set when output T10 and ODDSET are coincident, and reset when signal EVNSET is coincident with the set output (one logic ZERO) of the T10 filp-flop.



Table 4-VIII. Scaler Outputs (Stages 1-17)

Output	Frequency	Period	Pulse Polarity
FS01, FS01 F01A, F01B, F01C, F01D	51.2 kpps	19.5 μ sec.	- Positive
FS02, FS02A F02A, F02B	25.6 kpps	39.0 μ sec.	- Positive
FS03, FS03A F03A, F03B F03B	12.8 kpps	78.0 µ sec.	Positive Negative
FS04, FS04A F04A, F04B F04B	6.4 kpps	156 µsec.	Positive Negative
FS05, FS05, FS05A F05A, F05B, F05D F05A, F05B	3.2 kpps	312 µsec.	Positive Negative
FS06, FS06 F06A, F06B F06B	1.6 kpps	624 u sec.	Positive Negative
F807, FS07, F807A F07A, F07B F07A, F07B, F07C, F07D	800 pps	1.25 msec.	Positive Negative
FS08, FS08 F08A, F08B	400 pps	2.5 msec.	Positive Negative

(Sheet 1 of 2)

MANUAL

Table 4-VIII. Sealer Outputs (Stages 1-17)

Output	Frequency	Period	Pulse Polarity
F809, F809 F09A, F09B, F09D F09A, F09B	200 pps	5.0 msee.	Positive Negative
F10A, F10B F10A, F10B	100 pps	10 msec.	Positive Negative
FS11 F11A, F11B	50 pps	20.0 msec.	- Positive
FS12 F12A, F12B	25 pps	40.0 msec.	- Positive
FS13 F13A, F13B	12.5 pps	80.0 msec.	- Positive
FS14 F14A, F14B	6.25 pps	160 msec.	Positive
F815 F15A, F15B	3.125 pps	320 msee.	- Positive
FS16 F16A, F16B	1.5625 pps	640 msee.	- Positive
F817 F17A, F17B F17A, F17B	0.78125 pps	1.3 sec.	Positive Negative

NOTE: Aii puise outputs (F01A, F01B etc.) are 10  $\mu$  sec, wide regardless of frequency.

(Sheet 2 of 2)

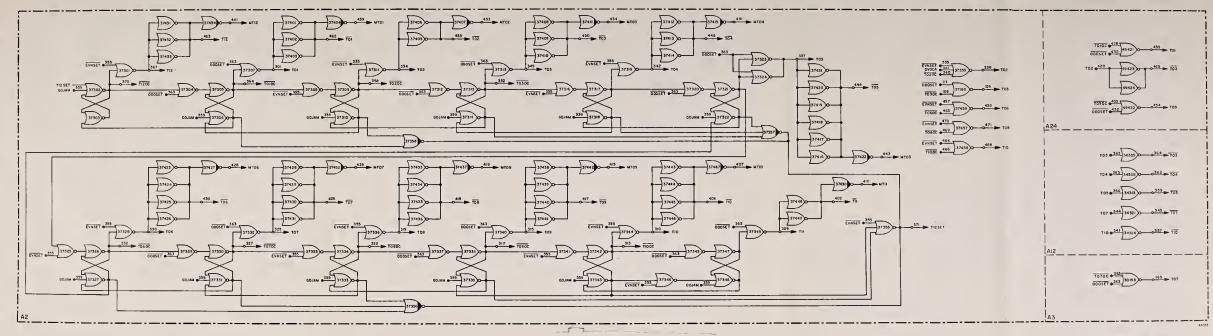


Figure 4-122. Time Pulse Generator Logic



The waveforms for the time pulse generator are shown in figure 4-123. Inputs ODDSET and EVNSET each occur at a 512 kpps rate, but are 90 degrees out of phase with each other. Consequently, even though the driving inputs are 0.75 microsecond wide, the effective drive rate of both inputs combined is twice the rate of the input. The period between each ODDSET and EVNSET pulse is 0.97 microsecond. However, time pulse outputs TOI through TI2 are 0.75 microsecond wide.

Signal GOJAM forces the time pulse generator to indicate T12 time by resetting the T1 through T11 flip-flops, and setting the T12 flip-flop. Forcing the time pulse generator in this manner enables the cycling to be restarted beginning with T01, after a condition occurs which initiated GOJAM.

Additional drive for several of the timing pulse outputs is provided by gates located on modules A2, A3, A12, and A24. These gates are illustrated in figure 4-122. The outputs (for example, T01 from gate 49421 on A24, T02 from gate 37359 on A2, etc.) are in parallel with the outputs developed by the flip-flops on module A2.

4-5.3.6 Sync and Timing Logic. The sync and timing logic, figure 4-124, generates synchronization, timing, and gating pulses for use within the computer subsystems, and synchronization pulses for systems external to the computer. These signals are developed as a function of the ring counter, strobe pulse generator, and scaler outputs.

The synchronization outputs to the external systems as well as the oscillator, clock divider logic, and the scaler outputs are generated both during normal operation and during standby. The gates on modules A1, A2, and A24 are controlled so that the supply voltage is uninterrupted when the computer is switched to standby operation. The sync and timing logic output waveforms are illustrated in figure 4-124A.

4-5.4 SEQUENCE GENERATOR. The sequence generator contains the order code processor, command generator, and control pulse generator. The sequence generator executes the instructions stored in memory by producing control pulses which regulate the data flow of the computer. The manner in which the data flow is regulated among the various functional areas of the computer and between the elements of the central processor causes the data to be processed according to the specifications of each machine instruction.

The order code processor receives signals from the central processor, priority control, and peripheral equipment. The order code signals are stored in the order code processor and converted to coded signals for the command generator. The command generator decodes these signals and produces instruction commands. The instruction commands are sent to the control pulse generator to produce a particular sequence of control pulses depending on the instruction being executed. At the completion of each instruction, new order code signals are sent to the order code processor to continue the execution of the program.



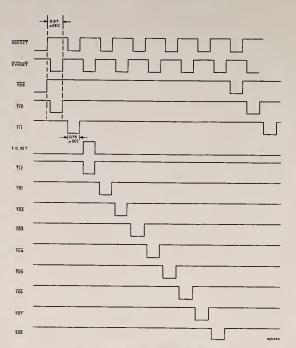


Figure 4-123. Time Pulse Generator Waveforms

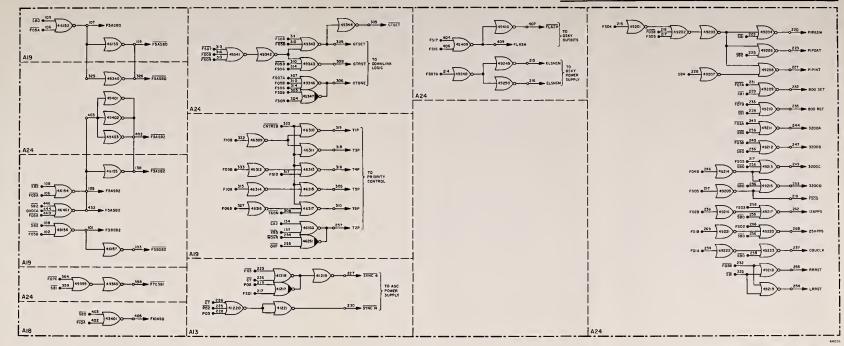


Figure 4-124. Sync and Timing Logic



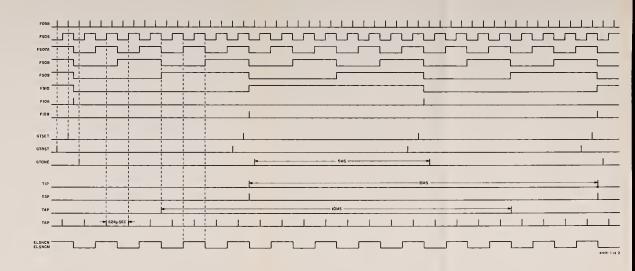


Figure 4-124A. Sync and Timing Logic Waveforms (Sheet 1 of 2)



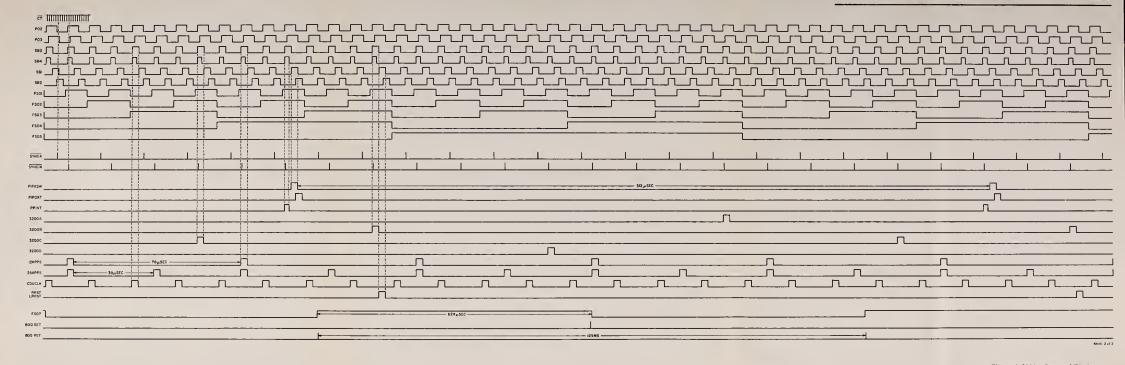


Figure 4-124A. Sync and Timing Logic Waveforms (Sheet 2 of 2)



4-5.4.1 Order Code Processor. The order code processor (figure 4-125) consists of the register SQ control, register SQ and decoders, and stage counter and decoders. The register SQ control is regulated by special purpose control pulse NISQ from the control pulse generator. Control pulse NISQ produces clear and write signals for register SQ and initiates a read signal for register B. The clear, read, and write signals place the order code content of register B onto the write lines and into register SQ. The order code signals from the priority control and the peripheral equipment pertain to start, interrupt, and transfer control to specified address instructions. These order code signals cause the register SQ control to produce the clear signal. If the order code signal is start or transfer control to specified address, no further action occurs because the order code for each of these instructions is binary 0 000 000. If the order code signal is interrupt, register SQ is set to 1000 111. Other special purpose control pulses provide regulatory functions within the register SQ control during interrupt and some address-dependent instructions.

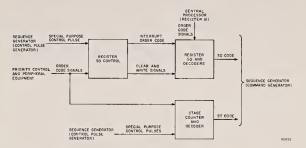


Figure 4-125. Order Code Processor, Block Diagram

Register SQ is a seven-bit register with only six of its bit positions (16 and 14 through 10) connected to the central processor write lines. The seventh (high-order) bit position is the extend bit. This high-order bit position is used for extending the order code field; it contains a logic ZERO for basic instructions and a logic ONE for extracode, channel, and interrupt instructions. Bit positions 16, 14, and 13 produce the SQ signals. At any time, only one of the eight possible SQ signals is present to indicate the octal number specified by these bit positions. Bit positions 12 and 11 contain the quarter code. These bits are decoded into one of four QC signals to indicate the octal number specified by these two bit positions. Bit position 10 is not used for basic and extracode instructions; however, it is used for the channel and interrupt instructions.

The stage counter is a three-stage Gray counter especially adapted for various counts other than the Gray code. Most instructions are several MCT's long and use the two low-order bits of the stage counter. The stage counter controls the length of each instruction. The stage counter always starts an instruction with count 000, Then it may be advanced to 001, 010, or 011 by special purpose control pulses ST1 and ST2 from the control pulse generator. The Gray code count is used for the divide instruction. Control pulse DVST advances the counter through the states 000, 001, 011, 111, 110, and 100. Then control pulse ST2 sets the stage counter to 010 to complete the divide instruction. The content of the stage counter is decoded into the ST code signals. Some of the ST code signals reflect the standard binary count from octal 0 through 3, and others reflect the Gray code count of octal 0, 1, 3, 7, 6, and 4. The order code signals from the priority control and the peripheral equipment set the stage counter to a particular state in a manner similar to that in which register SQ is set. The interrupt order code signal sets the stage counter to 000, the start order code signal sets it to 001, and the transfer control to specified address signal sets it to 011. The outputs of register SQ and stage decoders are sent to the command generator where they are used to produce subinstruction and instruction commands.

4-5,4,2 Command Generator. The command generator (figure 4-126) contains the subinteraction decoder, instruction decoder, and the counter and peripheral instruction control. The subinstruction decoder receives the SQ and ST code signals from the order code processor. These signals represent the order codes of all machine instructions and are decoded into subinstruction and instruction commands. For example, channel instruction WOR has a binary order code 1000 101 and stage code 000. The SQ code signals SQEXT, SQ0, QC2, and SQR10 are combined with ST code signal ST0 to produce subinstruction command WORO.

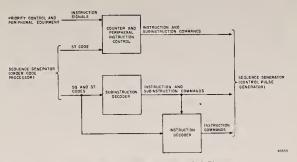


Figure 4-126. Command Generator, Block Diagram

The instruction decoder receives the coded signals from the order code processor indition to certain subinstruction commands. It produces signals called instruction commands. An instruction command is used for two or more subinstructions as compared to a subinstruction command which is used for only one subinstruction. For example, instruction command CI generates a combination of control pulses shared by subinstructions NDX0 and NDXX0. Instruction command ICI is produced by signals SQEXT, SQ5, and ST0 for subinstruction NDX0 or by signals SQ5, QC0, and ST0 for subinstruction NDXX0. Other instruction commands are produced from subinstruction commands. For example, IC8 is produced by ORINg DXCH0 with LXCH0.

The counter and peripheral instruction control receives instruction signals from the priority control and the peripheral equipment. These signals are applied to separate circuits which control the individual counter and peripheral instructions. The instruction signals from the priority control pertain to counter locations and the instruction(s) associated with each location. For example, signal C31A is interpreted as counter 31 address. The content of this location can only be changed by instruction DINC whose sub-instruction command is produced by the counter and peripheral instruction control. Another example is signal C42P, interpreted as counter 42 positive increment or signal other example is signal C42P, interpreted as counter 42 positive increment or signal

C42M, counter 42 negative increment. The peripheral equipment supplies instruction signals such as MREAD and MLOAD for the fetch and store instructions, respectively. While the particular instruction is being executed, the counter and peripheral instruction control stores the input signals in the same way that order code signals are stored by register 80. Since some of the peripheral instructions are several MCT's long, they use the ST code signals. The subinstruction and instruction command outputs of the command generator are used by the control pulse generator in conjunction with time pulses T01 through T12 to produce action pulses.

4-5.4.3 Control Pulse Generator. The control pulse generator (figure 4-127) contains the crosspoint generator, control pulse gates, and branch control. The crosspoint generator receives instruction and subinstruction commands from the command generator and branch commands from the branch control. The crosspoint generator produces an action pulse when a command signal and a time pulse are ANDed. This action is called the crosspoint operation. For example, action pulse 5XP12 is produced from subinstruction command DASO and time pulse T05. Many instructions use identical action pulses. When this is the case, several command signals such as TCO, TCFO, or IC4 will produce the same action pulse during time period T01. The branch commands are used to change the action pulse that normally is produced at a given time. For example, when certain conditions exist, a branch command will produce action pulse 8XP6 in addition to another action pulses ormally produced attime period T08. The action pulses are supplied to the control pulse gates which convert them to specific control pulses for use in instruction execution.

The control pulse gates perform the Boolean NOR function. There is one gate for each control pulse. These gates split the action pulses into as many control pulses as

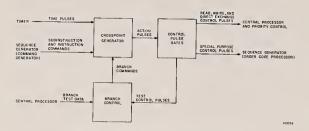


Figure 4-127. Control Pulse Generator, Block Diagram

are required for a particular operation. For example, action pulse 3XP6 is converted to control pulses RZ and WQ. Some of the control pulses produced by the control pulse gates are used by the sequence generator. These include the special purpose control pulses which control the operation of the order code processor and the test control pulses which are applied to the branch control. The other control pulse groups, namely the read, write, and direct exchange control pulses are used in the central processor and the priority control. The purpose of each control pulse is described in paragraph 4-5. 2, Machine Instructions.

The branch control is connected to the write lines of the central processor. Data which is placed onto the write lines by read control pulses is tested in the branch control. The branch control contains two stages. Branch I normally tests for sign and branch 2 tests for full quantities such as plus or minus zero. Both branches test for positive and negative overflow and have the overflow bits written directly into the branch register. Positive overflow is 01 where branch I is the high order bit. Negative overflow is 10. The branch commands sent to the crosspoint generator affect the action pulses at given times. The branch control also contains the special instruction flip-flop which controls the execution of RELIMT, INHINT, and EXYEND instructions.

4-5.4.4 Register SQ Control. The register SQ control (figure 4-128) is regulated by special purpose control pulse NISQ from the control pulse generator. Control pulse NISQ causes the register SQ control to produce clear signal CSQG, read signal RBSQ, and write signal WSQG. These signals place the order code (content of register B) onto the write lines and into register SQ at the beginning of each new instruction. The order code signals applied to the register SQ control from the priority control (GOJAM and RUPTOR) and peripheral equipment (MTCSAI) pertain to start, interrupt, and transfer control to specified address instructions, respectively. A distinct priority is associated with each of these three instructions. Interrupt and transfer control to specified address instructions can never be requested when the computer is forcing the execution of the start instruction, which has the highest priority. Certain peripheral instructions occupy the next level of priority, followed by the counter instructions and in turn the transfer control to specified address instruction, which has priority over the interrupt instruction; all six of these instruction categories have priority over basic instructions. In addition, the interrupt instruction cannot be executed when the next instruction being called is an extracode instruction. The register SQ control establishes this priority. It also provides signals to force register SQ to the 0 000 000 state for start and transfer control to specified address instructions, and state 1 000 111 for the interrupt instruction. The register SQ control is able to inhibit the processing of all subsequent interrupts when specified by the program and will permit only one interrupt to be processed at a time. Certain monitor functions built into the register SQ control may be used when the computer is connected to the peripheral equipment.

When control pulse NISQ is applied to the set side of the NISQL flip-flop (figure 4-128), the NISQL flip-flop will set, provided signal STRTFC is not present. Control pulse NISQ is produced during time period T02 or T08 depending on the subinstruction which produces the control pulse. Once the NISQL flip-flop is set, it remains set until signal INKBT1 or STRTFC is produced. Signal INKBT1 occurs at time period T01 when

no counter incrementing is in progress as indicated by the absence of signal INKL. Signal STRTFC may occur anytime during an MCT if produced by signal GOJAM or at a time period predetermined by the peripheral equipment if produced by signal MTCSAL.

Signals CSQG, RBSQ, and WSQG are produced during time period Ti2 provided that the NSQL flip-flop is set and signal RPTFRC is not present. The clear, read, and write signals are phased by the clear timing signal CT, the read timing signal RT, and the write timing signal WT, respectively. When the start or transfer control to specified address instruction is to be executed, the NISQL flip-flop is reset and signals RBSQ and WSQG are inhibited. However, signal CSQG is produced by signal STRTFC and forces the SQ register to the 0 000 000 state. If signal RPTFRC is present, signals CSQG, RBSQ, and WSQG are not produced. Signal RPTFRC is applied to register SQ and forces it to the 1 000 111 state.

The priority centred supplies signal RUPTOR to the register SQ control when the interrupt instruction is to be executed. Signal RUPTOR may be inhibited in the register SQ control by several conditions, one of which is the programmed interrupt inhibit called INHINT. The INHINT condition is established by executing instruction INHINT whose order code is 00, 0004. This instruction produces signal INHPLS which is applied to the set side of the INHINT flip-flop (figure 4-128). The INHINT flip-flop will set provided signal GOJAM is not present at the application of signal INHIPLS. Once the flip-flop is set, it remains set until signal GOJAM or RELPLS is produced. Signal RELPLS is produced by instruction RELINT which releases the interrupt inhibit condition. Instruction RELINT has the order code 00.0003. Signal MINHL from the INHINT flip-flop is connected to an indicator on the peripheral equipment. This indicator lights when the INHINT flip-flop is set.

Another condition which inhibits signal RUPTOR is the interrupt in progress (IIP) condition. The IIP condition is established during the execution of the interrupt instruction to indicate that an interrupt is in progress. Subinstruction RUPTO produces signal KRPT which is applied to the set side of the HP flip-flop (figure 4-128). The HP flipflop will set, provided signal GOJAM is not present at the application of signal KRPT. Signal KRPT is an action or crosspoint pulse (9XP1) produced during time period T09 of subinstruction RUPTO. Once the IIP flip-flop is set, it remains set until signal GOJAM or 5XP4 is produced. Signal 5XP4 is produced by subinstruction RSM3 which is executed at the completion of an interrupt sequence. Subinstruction RSM3 is part of the RESUME instruction (order code 05.0017) which returns control to the program that was being executed before the interrupt occurred. Signal 5XP4 is also an action or crosspoint pulse which is produced during time period T05. Signal MIIP from the IIP flip-flop is connected to the peripheral equipment. A switch on the peripheral equipment will permit signal MIIP to light an indicator and to cause a monitor T12 stop. This causes the time pulse generator (which produces signals T01 through T12) to stop at time period T12 until it is released by the peripheral equipment. The peripheral equipment can supply signal MNHRPT to the register SQ control. This signal is produced by a switch closure and inhibits signal RUPTOR. Signal OVNHRP inhibits signal RUPTOR for all multiply subinstructions preceding MP3 while the accumulator is being used in double-precision operations.



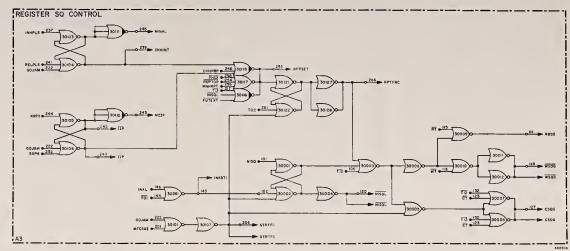






Figure 4-128. Register SQ Control, Logic Diagram





Signal FUTEXT is produced by the register SQ and decoder circuits. This signal is present when the next instruction to be executed is an extracode instruction. Signal is FUTEXT is produced when instruction EXTEND or NDX is executed and occurs at time period T08 or T10, respectively. Signal RUPTOR is inhibited by the future extend condition because this condition cannot be re-established when returning to the interrupted program through instruction RESUME. The order codes for instructions EXTEND and NDX which establish the future extend condition are 00.0006 and 15, respectively.

Signal RUPTOR will cause the RPTFRC flip-flop to set at time period T12 subject to the phasing of signal PHS2. A new instruction must be in the process of being called in order for the RPTFRC flip-flop to set. This condition is established by signal NISQL. The RPTFRC flip-flop will set only if signal STRTFC is not present at the same time the set signal is present. The flip-flop is reset at time period T02 or when signal GOJAM or MTCSAI is present.

4-5.4.5 Register SQ and Decoders. Register SQ is a seven-bit register which stores the content of the extended order code field as each instruction is being executed. The content of register SQ and decoders produces signals SQEXT, SQ0 through SQ7, QC0 through QC3, and SQR10. These signals are used by the command generator to produce subinstruction and instruction commands.

Register SQ (figure 4-129) is connected to the central processor by write line signals W116 and W114 through W110. The register SQ control produces signal R8SQ which places the order code content of register B onto the write lines. It also produces signal CSQC which clears register SQ and WSQG which writes the new order code into register SQ. Signal CSQC does not clear the SQEXT bit position. This bit position is set when an extracode instruction is to be executed and is controlled by the FUTEXT flipflop.

Special purpose control pulses EXTPLS and EXT are applied to the set side of the FUTEXT flip-flop. The flip-flop will set provided signal STRTFC is not present at the application of signals EXTPLS or EXT. Signal EXTPLS is produced at time pulse T08 by instruction EXTEND. The order code for the EXTEND instruction is 00.0006. Signal EXT is produced at time pulse T10 of subinstruction NDXXI. The FUTEXT flip-flop remains set until signal INKBT1 or STRTFC is produced. Signal INKBT1 occurs at time pulse T01 when no counter incrementing is in progress.

The SQEXT flip-flop can be set at time pulse T12 provided the NISQL and the FUTEXT flip-flops are set. If signal STRTFC is present, the NISQL and FUTEXT flip-flops will be reset and their outputs will cause the SQEXT flip-flop to reset also. Signal RPTFRC also sets the SQEXT flip-flop provided a new instruction is being called and signal STRTFC is not present. Once the SQEXT flip-flop is set, it remains set until the next basic instruction is executed. The resetting of the SQEXT flip-flop is accomplished when signal FUTEXT is not present and signals NISQL and T12 are.

When the start or transfer control to specified address instruction is to be executed, signal STRTFC resets the SQEXT flip-flop as specified in the preceeding paragraph. It

also produces signal CSQG which clears bit positions 16 and 14 through 10 of register SQ. As a result, register SQ is forced to the 0 000 000 state which causes the execution of instruction GOJ or TCSA depending on the state of the stage counter. When the interrupt instruction is to be executed, signal RPTFRC sets bit positions SQEXT and 12 through 10 and resets bit positions 10, 14, and 13 of register SQ. As a result, register SQ is forced to the 1 000 111 state which causes the execution of instruction RUPT.

Signals MSQEXT, MSQ16, and MSQ14 through MSQ10 are connected to indicators on the peripheral equipment so that the content of register SQ can be monitored at any time.

The SQ decoder produces signals SQ0 through SQ7 from the outputs of bit positions 14, and 13 of register SQ. These signals are used in the command generator together with signals SQETT, QC0 through QC3, and SQR10 to produce subinstruction and instruction commands. Signals SQ0 through SQ7 are inhibited by signal INKL signal INKL is produced when a counter instruction is being executed. When signal INKL is present, no commands can be produced other than those for the counter and peripheral instructions.

The QC decoder produces signals QC0 and QC3 for the outputs of bit positions 12 and 12 register SQ. These signals are also used to produce subinstruction and instruction commands and are not inhibited by counter incrementing.

4-5.4.6 Stage Counter and Decoder. The stage counter and decoder (figure 4-130) is regulated by special purpose control pulses ST1, ST2, DVST, RSTSTG, and TRSM from the control pulse generator and by order code signals GOJAM and MTCSAI from the priority control and peripheral equipment, respectively. The stage counter is used as a storage device which is forced to a different state after the execution of each subinstruction. The stage counter remains in a given state for one MCT, the duration of every subinstruction. The stage counter is forced through various counts depending on the instruction being executed. Most instructions are two MCT's long and are completed by executing subinstruction STD2. As a result, the stage counter is advanced through states 000 and 010. Some instructions are three MCT's long and are completed by executing subinstruction STD2. The stage counter states for these instructions are 000, 001, and 010. Other combinations of states are simply 000 for the transfer control instruction, 000 and 001 for the index instructions, 000 and 011 for the RESUME instruction, and 000, 001, and 011 for the multiply instruction. The divide instruction is seven MCT's long. Gray code counts 000, 001, 011, 111, 110, and 100 are used to enumerate six MCT's of this instruction. The seventh MCT is controlled by state 010 which is that of subinstruction STD2.

The stage counter contains three primary level flip-flops A, B, and C, and three secondary level flip-flops STG1, STG2, and STG3, respectively. The secondary level flip-flops are set to the state of the primary level flip-flops at time pulse T12 for most instructions. For the divide instruction, the transfer of states occurs at time pulses T03 and T12. The primary level flip-flops are reset at time pulse T01 to establish the state 900.

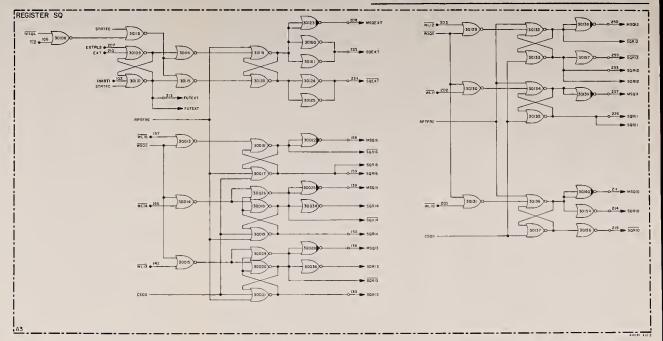


Figure 4-129. Register SQ and Decoder, Logic Diagram (Sheet 1 of 2)

REGISTER SQ

EQUATION

PUTENT JENTPLS GENT) STRIFT LINKETT STRIFT FUTENT

RL14 WIGG CIGG +SORIS CIGG RPTFRC

MLIS MSOC CSOC + SORIS CSOC APTERC

SORTE WELL MEDG CEOR + SORTE CEOR RETERC

SQRIZ MLIZ MSQG CSQG + MPTFMC + SQRIZ CSQG

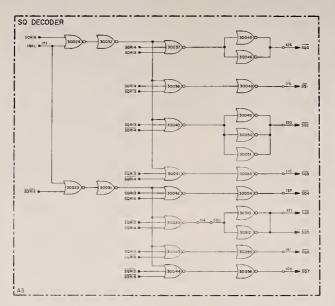
SORII - BLII WSQG CSQG + RPTFAC + SQRII CSQC

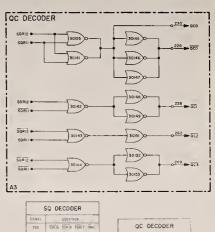
SQRIO | WLIO WSQG CSQC + MPTFRC + SQRII CSQG

FUTERT MISQ TIZ+RPTERC MISQL TIZ STRTEC

SIGNAL







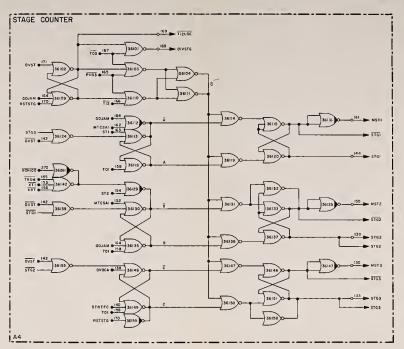
	6Q DI	ECDO	DER	
SIGNAL		EQUAT	HON	
200	30R16	SQR14	SQRIS	INKL
192	SURIE	5QR14	\$QR13	INKL
5Q2	SQ R16	50,814	50 R13	3000
503	30 R16	5QR14	\$0,813	PAKE
192	SQRIE	SQRIA	\$QR13	INKL
5Q5	91802	50R14	50R13	WKL
306	SQR16	SQR14	50 R13	SHILL
507	SORTE	SQRII	3QR13	INKL

Figure 4-129. Register SQ and Decoder, Logic Diagram (Sheet 2 of 2)



STAGE COUNTER						
SIGNAL	EQUATION					
A	STI +(GDJAM +MTCSAI) TOI +OVST STG3 +A TOI					
В	STZ GOJAN +NTCSAL TOL+OVST SYGL GOJAN +NORTOD X67 XT1 TRSM GOJAN TOL+O TOL GOJAN					
С	OVST STG2 STRTEC +C TOI STRTEC - RETETE					
TIZUSE	DVST GOJAN + TIZUSE GOJAN ŘŠŤSTG					
0	TIZ TIZUSE PHS3 + TO3 TIZUSE PHS3					
STGI	A 0+STG1   A + 0					
5TG2	8 0+ STC2 8+D					
STG3	C 0+5TG3 (C+0)					

	STAGE DECODER					
SIGHAL	EQUATION	Ī				
SYO	STG3 STG2 STG1	Ī				
STO2	STOS STGE STGE INKL					
513	STGS STG2 STG1					
STID	STES STEE STEE					
ST1376	STID + ST376					
ST376	\$TG2 (\$TG1 + \$TG3)					
ST3764	\$7376 4574					
ST4	5163 <u>\$162</u> \$161					



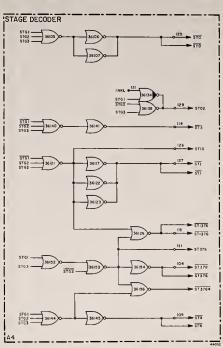


Figure 4-130. Stage Counter and Decoder, Logic Diagram



The stage counter can establish state 001 three ways. When the start instruction is to be executed, signal GOJAM sets flip-flop A and resets flip-flop B. Flip-flop C is reset by signal STRTFC. Control pulse STI sets flip-flop A (at time pulse T10) and control pulse DVST sets the flip-flop (at time pulse T02) provided that flip-flop STG3 is not set during the Gray code count sequence.

The state 010 can only be produced in one way, by control pulse ST2 which sets flipflop B at time pulse T08 or T10 depending on the subinstruction which produces the control pulse.

The state 011 can be produced four ways. When the transfer control to specified address instruction is to be executed, signal MTCSAI sets flip-flops A and B and signal STRTFC resets flip-flop C. During the execution of subinstruction MP1, control pulses ST1 and ST2 are produced at time pulse T10. These control pulses set flip-flops A and B and cause the execution of subinstruction MP3. During the execution of instruction RESUME, control pulse TRSM sets flip-flop B at time pulse T05. Instruction RESUME is an address-dependent instruction consisting of subinstructions NDN3 and RSM3. The content of register S must be octal 0017 for control pulse TRSM to set flip-flop B. At time pulse T10 of subinstruction NDN4, control pulse ST1 sets flip-flop A thereby establishing the state 011 for subinstruction RSM3. During the execution of the divide instruction, control pulse DVST sets flip-flop A thereby flop STG3 is not set. Flip-flop B is set by DVST provided flip-flop STG1 is set. Since flip-flop STG2 is not set when control pulse DVST is produced, flip-flop C remains reset, thus establishing state 011.

States 111, 110, and 100 are established by control pulse DVST at time pulse TO2 of instruction divide. Flip-flops A. B, and C are set provided that flip-flop STG3 is not set and flip-flops STG1 and STG2 are set, respectively. This establishes state 111. States 110 and 100 are established in a similar way and are dependent on the states of flip-flops STG1, STG2, and STG3.

The contents of filp-flops A, B, and C are transferred to filp-flops STG1, STG2, and STG3, respectively, at time pulse T12 if the T12USE flip-flop is not set. The transfer is subject to the phasing of signal PHS3. The T12USE flip-flop is set at time pulse T02 by control pulse DVST provided signal GOJAM is not present. Once the flip-flop is set, it remains set until reset by control pulse RSTSTG (which occurs at time pulse T08 of subinstruction DV4) unless signal GOJAM occurs first. When the T12USE flip-flop is set, the contents of the primary level flip-flops are transferred to the secondary level flip-flops at time pulse T03 according to the phase of signal PHS3. Signal DIVSTG is also produced at time pulse T03 under these conditions. When the secondary level flip-flops are set, they cannot be reset unless signal D is present. Signals MST1, MST2, and MST3 are connected to lights on the peripheral equipment to indicate the state of the stage counter.

The stage decoder (figure 4-130) produces signals ST0, ST1D, STD2, ST3, ST4, ST1376, ST376, and ST3764. This signal group is the decoded output of the stage counter

and is used in conjunction with signals SQEXT, SQ0 through SQ7, QC0 through QC3, and SQR10 to produce subinstruction and instruction commands. Signals ST0, ST1D, STD2, ST3 and ST4 are produced when the stage counter is set to states 000, 001, 010, 011, 011, 011, ond 100, respectively. Signal ST376 is produced when the stage counter is in state 011, 111, or 110. Likewise, signal ST376 is produced when the stage counter is set to state 001, 011, 111, or 110, and signal ST3764 is produced during states 011, 111, 110, or 100,

4-5, 4.7 Subinstruction Decoder, The subinstruction decoder receives the SQ and ST code signals from the order code processors and produces signals called subinstruction and instruction commands. Signals SQEXT, SQ0 through SQ7, QC0 through QC3, and SQR10 comprise the SQ code signals. Signals ST0 through ST4, ST376, ST1376, and ST3764 comprise the ST code signals. The SQEXT and SQR10 signals represent the high and low order bits, respectively, of register SQ. Signals SQ0 through SQ7 represent octal quantities of through 7 respectively, in bit positions 16, 14, and 13 of register SQ. Signals SQ0 through QC3 represent octal quantities of through 7, respectively, in bit positions 12 and 11 of register SQ. The SQ and QC signals are the decoded outputs of the register SQ and decoder circuits. The ST code signals represent the state of the stage counter. For example, signal ST1 represents state 001. The ST signals are thedecoded outputs of the stage counter and decoder circuits.

The subinstruction decoder utilizes the SQ and ST code signals in producing subinstruction and instruction commands. The command signals in turn are ANDed with time pulses T01 through T12 as accessary to produce crosspoint signals. This action is accomplished in the crosspoint generator. The crosspoint signals produce the control pulses which regulate the data flow of the computer. By definition, a subinstruction command is used for only one subinstruction. For example, command STD2 is used only during subinstruction STD2. An instruction command is therefore defined as a command which is used by two or more subinstructions. For example, command IC3 is used for subinstructions STD2. TC0, and TC76. Table 4-IX lists all of the commands produced by the various SQ and ST codes. The subinstructions which relate to the specific SQ and ST codes are also listed in table 4-IX.

Figure 4-131 shows the logic circuits that produce the subinstruction commands for basic, channel, and extracode instructions. Signal CCS0 is used as an example to illustrate the production of commands. When subinstruction CCS0 is to be executed, register SQ is set to the 0 001 00X state and the stage counter is set to 000. As a result, the order code processor supplies signals SQ1, QC0, and ST0 to the command generator. Since CCS is a basic instruction, the high order bit of register SQ is a logic ZERO and signal SQEXT is not present. The circuit for basic instructions detects this condition and produces signal NEXST0. Had signal ST1 been present instead of ST0, signal NEXST0 would not be produced. Signals NEXST0, SQ1, and QC0 are then ANDed to produce subinstruction command CCS0.

The QC signals are produced by the two high order bits of the address field. Instructions which do not use the extended order code field have commands that are produced

Table 4-IX. Commands Per Subinstruction

Subinstruction	SQ Code	ST Code		
Submistruction	SQ Code	ST Code	BR1 and BR2	Commands
	BA	SIC INSTRUCT	ions	
STD2		2		STD2 IC3
TC0	00	0		TC0 IC3
CCS0	010	0		CCS0 IC12
TCF0	012 014 016	0		TCF0 IC3
DAS0	020	0		DAS0 IC10
DAS1	020	1		DAS1
LXCH0	022	0		IC8 IC9
INCR0	024	0		INCR0 PRINC
ADS0	026	0		ADS0 DAS1
CA0	03	0		IC6 IC13
CS0	04	0		IC7 IC13
NDX0	050	0		NDX0 IC1 IC13
NDX1	050	1		IC2
RSM3	050	3		RSM3

(Sheet 1 of 6)

MANUAL

Table 4-IX. Commands Per Subinstruction

Subinstruction	SQ Code	ST Code	BR1 and BR2	Commands
	BASI	C INSTRUCTION	IS (cont)	
DXCH0	052	0		DXCH0 IC8 IC10
DXCH1	052	1		IC5 IC9
TS0	054	0	į	TS0 IC9
хсн0	056	0		IC5 IC9
AD0	06	0		AD0 IC11 IC13
MASK0	07	0		MASK0 IC14
	EXT	RACODE INSTR	UCTIONS	
DV0	110	0		DV0 DIV
DV1	110	1		DVI DV1376 DIV
DV3	110	3		DV1376 DV376 DIV
DV7	110	7		DVI376 DV376 DIV

(Sheet 2 of 6)

Table 4-IX. Commands Per Subinstruction

Table 4-1x. Commands Per Subinstruction							
Subinstruction	SQ Code	ST Code	BR1 and BR2	Commands			
EXTRACODE INSTRUCTIONS (cont)							
DV6	110	6		DV1376 DV376 DIV			
DV4	110	4		DV4			
BZF0	112 114 116	0	XX X0 X1	IC15 IC17 IC16			
MSU0	120	0		MSU0 IC12			
QXCH0	122	0		QXCH0 IC9			
AUG0	122	0		AUG0 PRINC			
DIM0	126	0		DIM0 PRINC			
DCA0	13	o		DCA0 IC4 IC10 IC13			
DCA1	13	1		IC6 IC13			
DCS0	14	0		DCS0 IC4 IC10 IC13			
DCS1	14	1		IC7 IC13			

(Sheet 3 of 6)

Table 4-1X. Commands Per Subinstruction

Subinstruction	SQ Code	ST Code	BR1 and BR2	Commands
	EXTRAC	CODE INSTRUCT	rions (cont)	
NDXX0	15	0		IC1 1C13
NDXX1	15	1		NDXX1 1C2
SU0	160	0		SU0 IC11 IC13
BZMF0	162 164 166	0	XX 00 X1 1X	IC15 IC17 IC16 IC16
MP0	17	0		MP0 IC14
MP1	17	1		MP1
MP3	17	3		MP3
	СН	ANNEL INSTRU	CTIONS	
READ0	100	0		READ0 INOUT
WRITE0	101	0		WRITE0 INOUT
RAND0	102	0		RANDO INOUT
WAND0	103	0		WANDO INOUT
ROR0	104	0		ROR0 INOUT

(Sheet 4 of 6)

Table 4-IX. Commands Per Subinstruction

Subinstruction	SQ Code	ST Code	BR1 and BR2	Commands
	CHAN	NEL INSTRUCT	IONS (cont)	
WOR0	105	0		WOR0 INOUT
RXOR0	106	0		RXOR0 INOUT IC14
	INT	ERRUPT INSTR	UCTIONS	
RUPT0	107	0		RUPT0
RUPT1	107	1		RUPT1
GOJ1	00	1		GOJ1
	CC	UNTER INSTRU	CTIONS	
PINC				PINC PARTC INKL
MINC				MINC PARTC INKL
PCDU				PCDU PARTC INKL
MCDU				MCDU PARTC INKL
DINC				DINC PARTC INKL
SHINC				SHIFT INKL
SHANC				SHANC SHIFT INKL

(Sheet 5 of 6)

Table 4-IX. Commands Per Subinstruction

Subinstruction	SQ Code	ST Code	BR1 and BR2	Commands
	PERII	PHERAL INSTR	UCTIONS	
TCSAJ3	00	3		TCSAJ3
INOTED				CHINC INKL MON+CH
INOTLD				INOTLD CHINC INKL MON+CH
FETCH0		0		FETCHO MON INKL MON+CH
FETCH1		1		MON STFET1 INKL MON+CH
STORE0	:	0		FETCH0 MON INKL MON+CH
STORE1		1		MON STFET1 STORE1 INKL MON+CH

(Sheet 6 of 6)

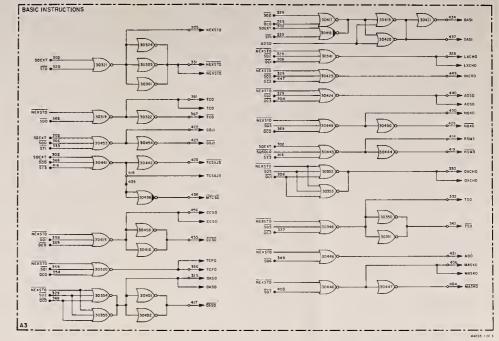




Figure 4-131. Subinstruction Decoder, Logic Diagram (Sheet 1 of 3)



SIGNAL			EQUAT	TION	
READO	SQEXT	500	QC0	<u>52810</u>	STO
RRITEO	5QEXT	500	QC0	01802	511
RANDO	SQEXT	sqo	QC1	01802	ST
WANDO	SQEXT	sgo	QC1	59810	ST
8080	SQEXT	500	QC?	01892	ST
¥089	SQEXT	500	QC2	50,810	ST
RXORO	SQEXT	500	QC3	5QR10	51
RUPTO	SQEXT	500	QC3	50810	SY
RUPT1	SQEXT	500	QCI	SQRIO	ST

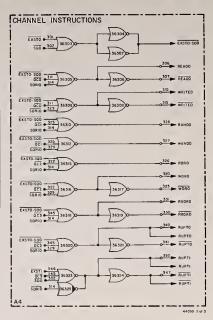


Figure 4-131. Subinstruction Decoder, Logic Diagram (Sheet 2 of 3)



EXT	RACOE	E	NS	TRUCTION	NS
SIGNAL			EQUAT	TION	
040	SQEXT	501	Q:00	510	
0V1	SQEXT	SQ 1	000	172	
0V1376	1 x 3 g2	501	QCB	511376	
D V 376	SQEXT	501	Q C 0	\$1376	
OV3764	TX3G2	501	QCD	\$73764	
OV4	TX392	1 92	000	514	
ezro	SQEXT	501	QCO	510	
WSU0	TX392	SQ 2	0 CO	\$10	
Охсно	SQEXT	sq z	QCI	570	
AUDO	SQEXT	SQ2	0 C2	\$10	
CHIO	1x392	SQ 2	Q C3	510	
DCA0	SQE XT	503	STO		
0C50	SQEXT	1 02	STO		
NO XXI	SQEXT	sQs	511		
SUO	TX392	5Q5	Q C0	5TO	
BZMF0	SQEXT	506	020	570	
MPO	SQEXT	507	570		
891	SQEXT	507	STI		
MP3	SQEXT	507	573		

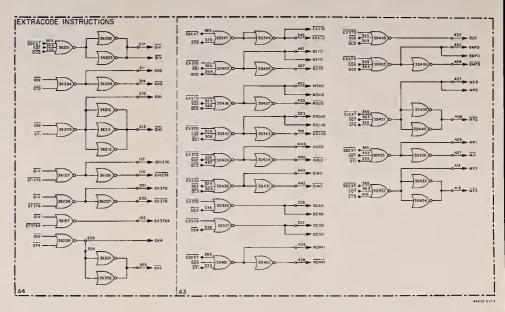


Figure 4-131. Subinstruction Decoder, Logic Diagram (Sheet 3 of 3)



without the QC signals. The basic instructions which can use any computer address are TC, CA, CS, AD, and MASK. The subinstruction commands produced without QC signals are TCO, ADO, and MASKO. Instructions CA and CS are controlled by instruction command signals from the instruction decoder.

The basic instructions which use the entire order code field are:

	(f) Dign	(9) DXCH
(1) CCS	(5) INCR	
(2) TCF	(6) ADS	(10) TS
(3) DAD	(7) NDX	(11) XCH
(4) LXCH	(8) RESUME	

These instructions have commands which are produced with aQC signal. Other important points concerning basic instructions are that signal DAS1 is an instruction command and signal LXCF0 is not used to produce crosspoint pulses.

Signal DAS1 is an instruction command because it is used for subinstructions DAS1 and ADS0. Subinstruction LXCH0 is controlled by instruction commands IC8 and IC9 which are produced by signal LXCH0. The logic diagram for basic instructions contains the circuits which produce commands TCSAJ3 and GOJ1. These commands are for peripheral and interrupt instructions, respectively, and are included here because they have order codes similar to basic instructions. Signal MTCSA is fed to the peripheral equipment.

The channel instructions and RUPT instruction are controlled by commands which produced from the entire order code content of register SQ and the content of the stage counter. For example, when subinstruction WANDO is to be executed, register SQ is set to the 1 000 011 state and the stage counter is set to 000. As a result, signals SQEXT, SQ0, QC1, and SQR10 are present and ANDed to produce subinstruction command WANDO.

The extracode instructions are also shown in figure 4-131. Special attention is given to the commands for the divide instruction because of the Gray code count used to control the commands. When instruction DV is to be executed, register SQ is set to the 1 001 00X state and the stage counter is set to 000. As a result, signals SQEXT, SQ1, and QC0, and ST0 are supplied to the subinstruction decoder. Signals SQEXT, SQ1, and QC0 are ANDed to produce instruction command DIV. In addition, signals DIV and ST0 are ANDed to produce subinstruction command DV0. Since signal DIV is produced without an ST signal, it remains for the duration of the divide instruction. It is also used to produce subinstruction commands DV1 and DV4 and instruction commands DV1376, DV376, and DV3764. Subinstructions DV1, DV3, DV7, and DV6 start at time pulse TV3 and end at the following time pulse T03. Instruction command DV1376 produces crosspoint pulses for time pulses T01 T02, and T03 whereas instruction command DV3764 is not used to produce crosspoint pulses for time pulses TV4 through T12. Instruction command DV3764 is not used to produce crosspoint pulses but it does turn off fixed memory timing during four MCT's of the divide instruction.

The remaining commands for the extracode instructions are similar to the commands for the basic instructions. Instructions DCA, DCS, NDXX, and MPdo not encroach on the address field for their order codes. As a result, the commands for these instructions do not use a QC signal. Signals BZFO, DCSI, and BZMFO are not used to produce crosspoint pulses but are used to produce Instruction command signals which control the associated subinstructions.

4-5, 4.8 Instruction Decoder. The instruction decoder receives the SQ and ST code signals from the order code processor and commands from the subinstruction decoder. The instruction decoder produces commands that are used for two or more subinstructions. These commands are ANDed with time pulses T01 through T12 as necessary to produce crosspoint pulses. Table 4-IX Ilsts the commands produced for each subinstruction. Table 4-X Ilsts the subinstructions that use a particular command for producing crosspoint pulses.

Table 4-X. Subinstructions Per Command

Command	Subinstructions	Command	Subinstructions
AD0	AD0	DIV	DV0
ADS0	ADS0		DV1 DV3
AUG0	AUG0		DV7 DV6
CCS0	CCS0	DA0	DV0
CHINC	INOTED	DV1	DV1
	INOTLD	DV4	DV4
DAS0	DAS0	DV376	DV3
DAS1	DAS1 ADS0		DV7 DV6
DCA0	DCA0	DV1376	DV1
DCS0	DCS0		DV3 DV7
DIMO	DIM0		DV6
DINC	DINC	DXCH0	DXCH0

(Shect 1 of 4)

Table 4-X. Subinstructions Per Command

Command	Subinstructions	Command	Subinstructions
FETCH0	FETCH0	IC12	MSU0
	STORE0		
		IC13	CA0
GOJ1	GOJ1		CS0
IC1	NDX0		NDX0 AD0
ICI	NDXX0		DCA0
	NDAAO		DCA1
IC2	NDX1		DCS0
102	NDXX1		DCS1
			NDXX0
IC3	STD2		SU0
	TC0		
	TCF0	IC14	MASK0
			MP0
IC4	DCA0		RXOR0
	DCS0	7015	Papa
IC5	DXCH1	IC15	BZF0 BZMF0
ICo	XCH0		BZMF0
		IC16	BZF0
IC6	CA0	1010	BZMF0
	DCA1		
IC7	CS0	IC17	BZF0
	DCS1		BZMF0
IC8	LXCH0		
ico	DXCH0	INCR0	INCR0
****	LXCH0	INKL	PINC
IC9	DXCH1	INKL	MINC
	TS0		PCDU
	XCH0		MCDU
	QXCH0		DINC
	DAS0		SHINC
	DXCH0		SHANC
IC10	DXCH0 DCA0		INOTED
	DCS0		INOTLD
			FETCH0
IC11	AD0		FETCH1
	SU0		STORE0
	CCS0		STORE1

(Sheet 2 of 4)

Table 4-X. Subinstructions Per Command

Command	Subinstructions	Command	Subinstructions
INOTLD	INOTLD	PARTC	PINC
Inot DD			MINC
INOUT	READ0		PCDU
	WRITEO		MCDU
	RAND0		DINC
	WAND0		
	ROR0	PCDU	PCDU
	WOR0		
	RXOR0	PINC	PINC
MASK0	MASK0	PRINC	INCR0
			AUG0
MCDU	MCDU		DIM0
MINC	MINC	QXCH0	QXCH0
MON	FETCH0	RAND0	RAND0
,	FETCHI		
	STORE0	READ0	READ0
	STORE1		
		ROR0	ROR0
MON+CH	INOTED		
	INOTLD	RSM3	RSM3
	FETCH0		
	FETCH1	RUPT0	RUPT0
	STORE0		
	STORE1	RUPT1	RUPT1
MP0	MP0	RXOR0	RXOR0
MP1	MP1	SHANC	SHANC
			OVING
MP3	MP3	SHIFT	SHINC
******	350110		SHANC
MSU0	MSU0	STD2	STD2
********	NDX0	3102	G I DZ
NDX0	NDXU	STFET1	FETCHI
NDXX1	NDXX1	O TELL	STORE1
MDVVI	HDAAL		

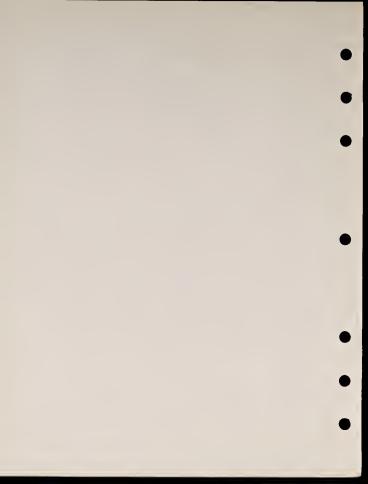
Table 4-X. Subinstructions Per Command

Command	Subinstructions	Command	Subinstructions
STORE1	STORE1	TCSAJ3	TCSAJ3
SU0	SU0	TS0	TS0
		WAND0	WAND0
TC0	TC0 TC0	WOR0	WOR0
TCF0	TCF0	WRITE0	WRITE0

(Sheet 4 of 4)

Figure 4-132 shows the logic circuits that produce most of the instruction commands for basic, channel, extracode, counter, and peripheral instructions. Two examples are used to describe how the instruction commands are produced. First, consider signal IC5 which is used for subinstructions DXCH1 and XCH0. When subinstruction DXCH1 is to be executed the order code content of register SQ is 0 101 01X and the stage counter is set to 001. As a result, signals SQ5, QC1, and ST1 are present. Since the high order bit is a logic ZERO, signal SQEXT is not present. These conditions are detected by an AND function and signal IC5 is produced. When subinstruction XCH0 is to be executed signals SQ5, QC3, and ST0 are present and signal SQEXT is not present. These conditions are also detected by an AND function and signal IC5 is produced.

The second way to produce instruction command signals is by ORing various subinstruction commands. For example, signal IC12 is produced by subinstruction command CC50 or MSU0. Another example is signal IC10 which is produced by subinstruction command DXCH0 or DASO. It is also produced by instruction command signal IC4. Commands IC16 and IC17 are dependent on branch conditions. Signal IC16 is produced by signals BZF0 and BR2 orby signals BZMF0 and either BR1 or BR2. Signal IC17 is produced when signal IC16 is not present because of improper branch conditions during subinstructions BZF0 and BZMF0.



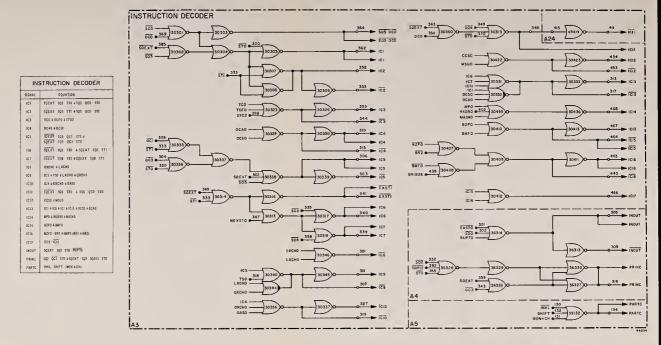


Figure 4-132. Instruction Decoder, Logic Diagram



4-5. 4.9 Counter and Peripheral Instruction Control. The counter and peripheral instruction control (figure 4-133) is regulated by signals from the priority control and peripheral equipment. The signals supplied by the priority control are the start order code signal (GOJAM), the counter OR signal (CTROR), and the various counter increment signals that request a particular counter instruction. The prime function of signal GOJAM is to take top priority by inhibiting and resetting many circuits in the counter and peripheral instruction control. Signal CTROR is used to produce the Increment signal (INKL) in addition to various strobe signals. The signals supplied by the peripheral equipment are MREAD, MLOAD, MRDCH, MLDCH for FETCH, STORE, INOTRD, and INOTLD instructions, respectively. The peripheral equipment also supplies signal MNHNC for inhibiting the counter increment operation. The counter and peripheral instruction control supplies the following subinstruction commands to the control pulse generator:

(1) STORE1	(4) PCDU	(7) SHANC
(2) PINC	(5) MCDU	(8) DINC
(2) MINIC	(6) SHINC	

It also supplies the following instruction commands:

(1) INKL	(3) MONTCH	(5) FETCHO
(2) STEET1	(4) CHINC	

The instruction command signal INKL must always be produced before a counter or peripheral instruction can be executed. Signal INKL interrupts the operation of the register SQ control, SQ decoder, and stage decoder so that no instruction or subinstruction command will be produced while the counter or peripheral instruction is being executed. Signal INKL does not destroy the order code in register SQ; it simply delays recognition of the order code until the counter or peripheral instruction has been executed.

A counter or peripheral instruction cannot be executed if a GOJAM condition exists. Signal GOJAM is applied to the set side of the GNINC flip-flop. If time pulse T01 is not present, signal GOJAM will set the GNINC flip-flop. The flip-flop will remain set until the following T01 time pulse. Signal B controls the time at which a counter or peripheral instruction can be executed. Signal B is present at time pulse T12 provided signal NISQL is also present. Signal NISQL is produced by the register SQ control. This signal is present only at the end of each instruction; its absence at time pulse T12 prevents a counter or peripheral instruction from being executed between subinstructions. Signal B is produced during the last quarter interval of time pulse T12 as indicated by the presence of signal P184.

When a counter instruction is to be executed, signal CTROR from the priority control is present. The presence of signals B and CTROR will allow a counter increment to occur provided the operation is not manually inhibited by signal MNHNC from the peripheral equipment or by signal A. Signal A is produced whenever a peripheral instruction is to be executed and gives the peripheral instructions priority over the counter instructions. If the preceding conditions are met, flip-flop C will set. The set input to

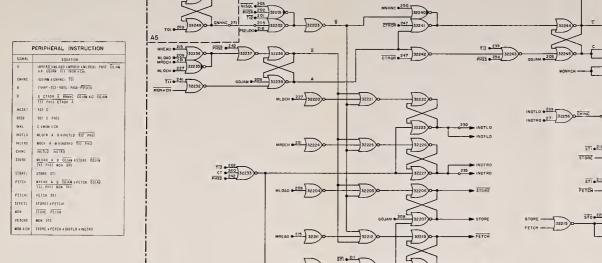
flip-flop C can be overridden by signal GOJAM if both the set and reset inputs occur at the same time. Signal C will be present for almost a full MCT, starting during the last quarter laterval of time pulse T12 and remaining until the third quarter interval of the following T12 pulse. The third quarter reset interval is controlled by signal PHSS. If additional counter incrementing is to take place, the C flip-flop will remain set. It can be reset any time by signal GOJAM or at time pulse T12 if both a counter and a peripheral instruction are requested at the same time. When this happens, signal A in addition to signals T12 and PHSS will reset the C flip-flop. At the end of all counter incrementing, the absence of signal CTROR will cause the flip-flop to reset at time pulse T12.

Signal INKL is produced directly from signal C or from signal MON+CH which indicates a peripheral instruction is being executed. Signal C also produces signal INCSET at time pulse T02 and signal RSSB during the third quarter of time pulse T07. Signal INCSET causes any counter instruction request to set the associated counter instruction flip-flop. Signal RSSB in conjunction with decoded counter addresses, resets cells in the priority control. This action terminates counter instruction requests applied to the counter and peripheral instruction control. Signal MINKL is sent to the peripheral equipment and can be used to produce a time pulse T12 stop and turn on an indicator.

Signal A is present when a peripheral instruction is to be executed. The A flip-flop may be set by signal MREAD, MLOAD, MRDCH, or MLDCH from the peripheral equipment. These signals are subjected to the timing of signal PHS2. The flip-flop remains set until the T11 timepulse, during which signal MON+CH is present. The A flip-flop is also reset by signal GOJAM, which may occur at any time.

Signal A resets the C flip-flop at the next T12 time pulse. It is also used to establish a pertipheral instruction request. A peripheral instruction cannot be executed before the completion of the current instruction. This action is controlled by signal B which is produced at time pulse T12 when the NISQL flip-flop is set. Signal A is produced by signal MLDCH, A, and B cause the INOTLD flip-flop to set. The channel load instruction is one MCT long. Therefore, the INOTLD flip-flop remains set for one MCT from the last quarter of time pulse T12 as determined by signal B to the second quarter of the following T12 time pulse as determined by reset signals T12 and PHS2. The channel read instruction is controlled by flip-flop intermined by signals BMDCH, A, and B and reset by signals T12 and PHS2. The timing of signals INOTLD and INOTRDIs identical. These signals are subinstruction commands and either one will produce instruction commands signals CHINC and MON-CH. Signal MON-CH, in turn, produces signal INKL and also causes the A flip-flop to be reset at time pulse T11.

Instructions STORE and FETCH are both two MCT's long. The STORE flip-flop is set when signals MLOAD, A, and B are all present and signal GOJAM is not present. The STORE flip-flop remains set for two MCT's. During the first MCT, the stage counter is set to the 000 state and produces signal STO. Signal STORE produces signal MON which in turn is combined with signal STO to produce instruction command signal FETCHO. During the second MCT, the stage counter is set to the 001 state and produces signal ST1. Signals STORE and ST1 are then combined to produce subinstruction command



PERIPHERAL INSTRUCTIONS

A2I

32252 32250 32209 216 STEET 210 FETCHI 220 - FETCHO 0223 → MON - MON MON+CH 3223 44095 1 of 2 Figure 4-133. Counter and Peripheral Instruction Control Logic (Sheet 1 of 2)

32248

32251

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COUNTER INSTRUCTIONS		
SIGNAL	EQUATION	
PIRC	C24A + C25A + C26A + C27A + C30A + C33P + C40P	
WINC	ICSZM & CRONE + CRIM + CRZM + CRZM + CRRM   INCSET & WING T17A	
PÇDU	1C32P 4 C33P 4 C34P 4 C35P 4 C35P 1 INCSET. +PCOU T12A	
MCDA	C37M + C33M + C34M + C35M + C36M1 INCSET + WCOU T12A	
SHIND	(C45M + C46M + C57A + C50A) LHC5ET + SHINC T12A	
SHANG	(C45P + C46P) INCSET + SHANC TIZE	
OINC	1031A + 047A + 050A + 051A + 052A + 053A + 054A + 055A + 0567   INDSET + DING   T124	

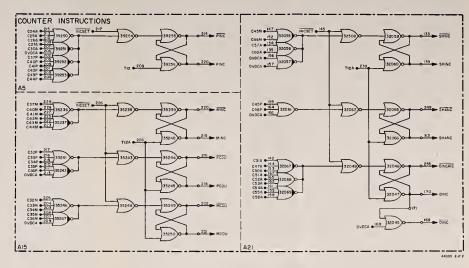


Figure 4-133. Counter and Peripheral Instruction Control Logic (Sheet 2 of 2)



signal STORE1. In addition, when signals T12, PHS2, MON, and ST1 are all present, the STOREflip-flopis reset. This condition occurs at the end of the second MCT. Signal STORE also produces signal MON+CH which resets the A flip-flop at time pulse T11. The STORE flip-flop may be reset at any time by signal GOJAM.

The FETCH flip-flop is set when signals MREAD, A, and B are present. Signal FETCH produces signals MoN and MON-CH. During the first MCT of instruction FETCH, signal MON and STO produce instruction command FETCHO. During the second MCT, signals FETCH and STI produce signal FETCHI, instruction command STFETI is produced by either FETCHI or STOREI. The FETCH flip-flop is reset at time pulse T12 when signals PHS2, MON, and STI are all present. It may also be reset by signal GOJAM. Signal MKEQDNis sent to the peripheral equipment to indicate that the computer has accepted the instruction request and to control the circuits which supply signals MKEAD, MCOAD, MRDCHI, and MLOCH.

The priority control supplies instruction signals to the counter and peripheral instruction control. The priority control contains 29 counter cell circuits, one for each counter location in erasable memory. Each counter performs a particular function. For example, time counters T1 through T5 are incremented at regular intervals to provide elapsed time data for the program. Since these counters can only be incremented, they are controlled by instruction PINC. Other counters can be incremented or decremented by instructions PINC or MINC, respectively, or by instructions PCDU or MCDU when dealing with the CDU counters. Other counters are controlled by instructions SHINC, SHANC, and DINC.

When any counter is to be updated the associated cell in the priority control is set by an incremental pulse input. The cell then produces a counter address signal. For example, if the counter at location 0024 is to be updated, cell 24 is set and counter address signal C24A is produced. The counter address signal then performs as many as two functions. First, if the counter being updated is controlled by only one instruction such as instruction PINC, the counter address signal sets the associated instruction flip-flop in the counter and peripheral instruction control. Then, as the instruction is being executed, the counter address signal produces the corresponding octal address which is placed onto the write lines and written into register 5 by control pulse action.

Since certain counters are controlled by two instructions, their counter address signals cannot be used to setan instruction flip-flopin the counter and peripheral instruction control. The cells in the priority control for these counters produce one of two signals in addition to the counter address signal. The additional signals are produced by flip-flop in the cell circuit. If a counter is to be decremented, one of the two flip-flops will be set by an incremental input. If the same counter must be incremented at later time, the other flip-flop is set by a different incremental input. The signals from these flip-flops are labeled with a P or an M to indicate a plus incrementor minus increment, respectively. For example, when counter 0337 is being incremented, signal CSTP is produced. This signal sets the PINC flip-flop in the counter and peripheral instruction control. When the same counter is being decremented, signal CSTM is produced. This signal sets the MINC flip-flop. Table 4-DX lists the counter address and instruction signals from the cells in the priority control.

Table 4-XI. Counter Cell Signals

Counter	Location	Address	Instruction	Instruction
Country		Signal	Signal	
Т2	0024	C24A		PINC
T1	0025	C25A		PINC
T3	0026	C26A		PINC
T4	0027	C27A		PINC
T5	0030	C30A		PINC
T6	0031	C31A		DINC
CDUX	0032	C32A	C32P	PCDU
			C32M	MCDU
CDUY	0033	C33A	C33P	PCDU
			C33M	MCDU
CDUZ	0034	C34A	C34P	PCDU
			C34M C35P	MCDU
TRN	0035	C35A		MCDU
		COC. A	C35M C36P	PCDU
SHAFT	0036	C36A		MCDU
1	0037	C37A	C36M C37P	PINC
PIPX	0037	C37A	C37M	MINC
D. D. D. D. D. D. D. D. D. D. D. D. D. D	0040	C40A	C40P	PINC
PIPY	0040	CHOA	C40M	MINC
n n n	0041	C41A	C40P	PINC
PIPZ	0041	CHIA	C40M	MINC
BMAGX	0042	C42A	C42P	PINC
BWAGA	0042	CTZA	C42M	MINC
BMACY	0043	C43A	C43P	PINC
BMACI	00.40	01011	C43M	MINC
BMACZ	0044	C44A	C44P	PINC
Dimico	0011	0	C44M	MINC
INLINK	0045	C45A	C45P	SHANC
11122111			C45M	SHINC
RNRAD	0046	C46A	C46P	SHANC
			C46M	SHINC
CYRO	0047	C47A		DINC
CDUX	0050	C50A		DINC
CDUY	0051	C51A		DINC
CDUZ	0052	C52A		DINC
TRUN	0053	C53A		DINC
SHAFT	0054	C54A		DINC
THRST	0055	C55A		DINC
EMS	0056	C56A		DINC
OTLINK	0057	C57A		SHINC
ALT	0060	C60A		SHINC

The cell signals which set the various counter flip-flops are shown in figure 4-133. Only one cell signal is present at a time. Each of the counter instruction flip-flops are set at time pulse TO2 as determined by signal INOSET. Signal INOSET is present only when the NISQL flip-flop is set and no peripheral instruction is being executed. The counter instruction flip-flops remain set from time pulse TO2 through T12. The control pulses required at time pulse TO3 of the counter instructions are produced by instruction command signal INKL.

4-5. 4. 10 Crosspoint Generator. The crosspoint generator receives subinstruction and instruction commands from the command generator, branch commands from the branch control, and timing pulses from the timer. It produces crosspoint or action pulses as necessary by ANDing a given command signal with the appropriate time pulse signal. The crosspoint pulses are converted into control pulses and applied to various elements of the computer for regulating data flow. Some of the crosspoint pulses are used directly as control pulses due to the function which they must perform. However, most control pulses are produced by the control pulse gates. Some crosspoint pulses are controlled by branch commands in addition to a subinstruction or instruction command. For example, subinstruction CCS0 uses branch commands during time pulses T07 and T10 as listed in table 4-VII. Machine Instructions, paragraph 4-5. 2.

Subinstruction CCS0 is a decision-making subinstruction. At time pulse T01, instruction command IC12 and time pulse T01 are ANDed to produce crosspoint pulse (XP) RL103B as shown in figure 4-134 and listed in table 4-XII. Crosspoint pulse RL103B is also produced by commands DASO, DASI, IC9, DXCHO, PIRNO, or INOUT. This pulse performs several functions. First, it is used as a control pulse to place the ten (10) low order bits of register B onto the write lines. Second, it is converted into control rules (CP) WS which enters the content of the write lines into register S.

At time pulse T02, crosspoint pulse 2B is produced and converted into control pulses RSC and WG. Signal 2B is produced involuntarily every T02 time pulse except when inhibited by subinstruction commands MP1, MP3, or DV0 or instruction commands inNOUT, IC15, and DV1376. Many subinstructions use control pulses RSC and WG at time pulse T02 as listed in table 4-VII. If the content of register S is an erasable memory address, control pulse WG clears register G and the decoded address signals inhibit control pulse RSC. Data from fixed or erasable memory may be transferred into it at a later time. If a central processor register is addressed, fixed and erasable memory timing is turned off, and the content of addressed register is copied into register G by control pulses RSC and WG. For subinstruction CCSO, the address in register S can be that of an erasable memory or central processor location. It can never be a fixed memory address because control pulse RL10BB does not place bits 12 and 11 of the address onto the write lines.

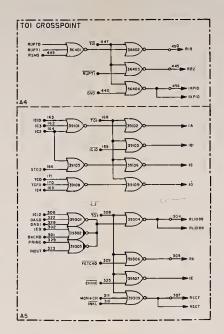
No crosspoint or control pulses are produced at time pulses T03 and T04 of subinstitution CCSO. However, the content of the addressed erasable memory location is entered into register G at time pulse T04.

Table 4-XII. Subinstruction CCS0

	BRI	Involu	ntary	ccs	30	IC12	2
Time	and BR2	XP	CP	XP	CP	XP	CP
1						RL10BB	WS
2		ZB	RSC WG				
5				5G	RG TMZ TPZG TSGN	5J	RG WB
7	xx			7D	RZ WY12		
7	X1			7XP4	PONEX		
7	1X			PTWOX			
8		8XP10	ws	8A	RU WZ		
9						9B	RB WG
10	xx			10B	ST2 WY		
10	00			10XP9	RB		
10	X0			10XP6	CI MONEX		
10	1X			10G	RC		
11				11E	RU WA		

TOI CROSSPOINT				
SICNAL	CONTROL PULSES	EQUATION		
R15	HIS WS	TO: (RSW) + RUPTO + RUPTI)		
R82	RB2	TOI RUPTI		
1XPI0	RA TMZ TSGN #8	TOL DVO		
1A	BA15	T00 (IC7+IC3+IC10)		
18	MONEX	TOL ICIO		
IC	RŽ	TGE (IC2 + 5TD2)		
10	NB	TOI (TCD +TCFD +IC4)		
MLICES	8E1DBB	TOL (ICIZ+OASD+OASL+IC9+ DXCND+ PRINC+IMDUT)		
PS.	RS BS	TON FETCHS		
1€	RS	TOI CHINC		
HSCT	RSCT	TOI INRL MON + CH		

	T02	CROSSPOINT
SIGNAL	CONTROL PULSES	EQUATION
2A	#6	TO2 SHITED
2XP3	RA 18	דעםאו עוד
20	RSC WG	TOZ   MDUT+MP1+MP3A+DV0+ICIS+OV1375}
2XP5	RC TM2 SA	T02 DVG-681
30	MISQ	T07 (IC2 + IC3 + NSM3)
OVST	DVST	TIE OLV STOE
2XP1	NISQ ZIP	T02 MP3
2XP8	STL	TOZ FETCHO



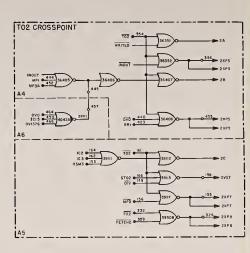


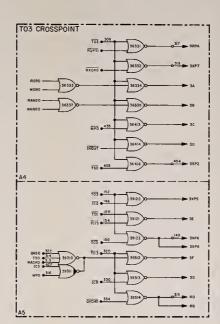
Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 1 of 10)

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	TO3 CROSSPOINT				
SIGNAL	CONTROL PULSES	EQUATION			
RRPA	RRPA WZ	TOJ RUPTI			
3XP7	RC RCH	TOS AXORO			
3A	RB.	TG3 (RORS + WORS)			
38	RC	T03 (RANDD + WARDD)			
)C	15GH	T03 MP0			
30	97	TO3 INDUT			
3XP2	TOV	T03 T50			
3XP5	RB WZ	T03 IC2			
3€	RA TMZ TSGN WG	TEI ICIS			
3875	RZ NQ	тиз тсе			
3F	RA WB	T03 (DASO + T50 + MASNO + ICS + MF0)			
10	RL T6	TOS ICS			
RQ	#6 #6	тез фхсме			

	T04	CROSSPOINT
SIGNAL	CONTROL PULSES	MOITAUGS
4.4	C1 L16	TOU TSD (BR) BRZ + BRI BRZ
48	RO WL	TO4 MPD - BRI
40	RC WL	TOI MPD BRI
4XP5	RZ WY12	T01 - T\$0
40	TSGN	TOU DVI BRZ
4XPII	RCH	TU4 INDUT
4E	RSC WC	T04 UP3
4F	RA	TON ICY
4G	TPZG	T02 IC15
411	RL TA	164 DAS0
4)	RC #A	TON MASKO
410	RL	Tel DVS
4L	¥6	T04 (0V1 + INOUT & (C2)
40	A2C	TO WON FETCH!



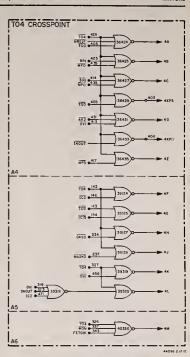


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 2 of 10)



	T05	CROSSPOINT	1	TOS CR	OSSPOINT (cont)
SIGNAL	CONTADL PULSES	CQUATION	SIGNAL	COMERCE PULSES	EQUATION
31978	RG TSGU	FOS DV4	51	RG 98	105 1012
5xP1	RU RA	TOS INDUT READ) WHITEO READS	SK	RG AZX	TOS DASI
			SL	87	tos IPRIMO + DASI + PARTO;
5A 5B	RA RA	TOS READD TOS MRITEO	5XP9	RG TSCN WYO	TOS SHIFT
5C	9CH	Tro word	28	CI	TOS SHANC
50	RA RC	105 exORO	5xF11	RG WL	TOS ICO
5€	#G #8I	TOS 150 BRI 882	5XP15	RG RQ	TOS QXCNS
SF	RIC	TOS TSO BR) BR2	5XP21	RCH	TOS CHINC
815%	th5x sy	105 OV1	5N	CI RB WY17	TOS ICIE
31P4	RG 9Z	T05 (FSM)	SP	CI RZ	T05 MP3
50	RG	TOS IPARTO + PAINO + CCSOI		8712	
	TMZ TPŽÇ		50	NG.	105 ICS
	TSCH		5.0	RC	TOS (DV) BRI + RANDS + WAN
SM	RZ	105 102	Z16	216	TOS DVI BRI
5x P12	RU St.	T05 0A50	5XP15	RB.	TOS (DVI BRI + RORG + WORG
TRSM	TRSM	105 NOXO	55	#A	TOS TSQ (BR) BR2 + BR) B

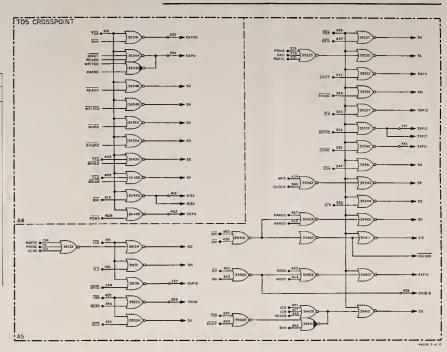


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 3 of 10)



	TO6 CROSSPOINT				
SICNAL	CONTROL PULSES	EQUATION			
8XPS	RU TOV WL	T06 DV1			
TL15	TLIS	T06 MP3			
BA .	RB #G	TOG ASM3			
68	AZX RG BY	TOS DASD			
8C	AZX CF RC WY	T06 MS20			
60	RU PZ	T06 HC10 + MP3 + IC2 + IC3 + T501			
6KP8	RU TOV WG WSC	TOS DASI			
EXP1	RZ TOV	T05 DV4			
EXP2	RA WB	TOO RECORD INCUT			
5XP10	PONER	TOS (AUGO BR) + DIMO BR) BR2 + DIMO BRI BR2 + INCR0 + PINCI			
θE	MONEX	TOS   WINC + MCDU + AUGO BRI + DINO BRI BRZ + DINC BRI BRZ1			
4XPI2	CI	TOS (PCON + MCDU)			

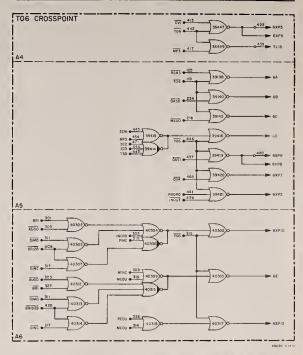
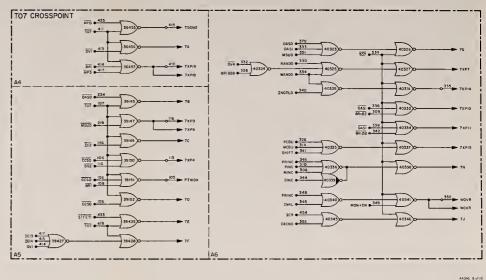


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 4 of 10)



0		то	7 CROSSPOINT
i	SEGNAL	CONTROL PULSES	EQUATION
	1SGN2	TSGNZ	10) WF0
	7.8	RSC TSGN	T07 OVI
	78919	XSA BR WY	T07 WP3 BR1
	78	R8	T07 DASO
	1XP9	RUS TSCN	TO7 MSUD
	70	AZX HG WY	TO? IC?
	7xP4	PONEX	TO7 CCSO BR7
	PIWOX	PTWOX	TO7 CCS0 BRI
i	10	HZ BYIZ	TA7 CCS0
	76	HG.	TO7 STFEE:
	JE .	#8 HC	T07 (ICL3 + ICL4 + 0V1)
į	76	NA.	T07 (DASD + OAS2 + MSUO)
ı	78.97	RC WA	T07 GV\$ (6R1+8F2)+T07 [RANGO+#ANDO]
	7XP14	MCH	TO7 HNOTED + WANDDI
1	7XP10	RBI	107 QASI (881 + 882)
ì	78711	RIC	TO7 DASI IBRI + BRZ:
	7X P15	RUS	107 (PCOU +WCOU +SHIFT)
ı	78	AU	107   PRINC + PINC + MINC + OINCI
	#0VR	WG WOYR WSC	160 IMON 4 CHI IPRINC + IIINL2
	2)	RB WC WSC	T07 (IC9 + 0 ×CH0)



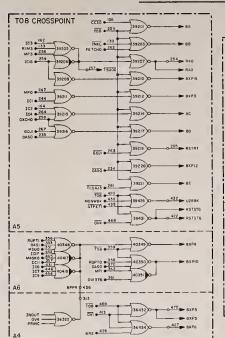
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Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 5 of 10)



	TO	08 CROSSPOINT
SIGNAL	CONTROL PULSES	EQUATION
8A	RU ¥2	TOR CCSD
18	RB	TON INKL FETCHO
RAD	RAQ WB	TOS (IC3 + RSW3 + WP) + IC16)
EXPIS	MIZO	TOS ICIE
8XP3	RZ	TOS (WPO +ICI)
ac	RU	TOS (IC2 + IC4 + DXCH8)
SD	#8	T00 (G0)1 + DAS0 + DXCH01
RSTRT	RSTRT	TOS GOJI
1XP12	RL	TOE DASO
38	ST2 WZ	TOB TCSAJ3
U2BB%	U288X	TOS WOMMEN STEETI
RSTSTG	RSTSTG TSGN	T00 0V4
8XP4	RZ ST2	TOS (RUPTI + DASI + MSUD + ICI) + MASKU +ICII + IC6 + IC7 + IC9 + INOUT + DV4 + PRINC)
0 X P 2 O	WS	TOR RUPTO DASO WPI DVISTA
EXP5	RA WY	TOS DVI
8XP6	PONEX	TOS OVI BAZ

	CONTROL	
SIGNAL	PULSES	EQUATION
9XPI	RG NG	TOS RUPTS
9A	RC WG	TOS RXORD
98	RB WG	TD9 :RUPT( \$1013 \$1012)
90	WG	TOP STORE!
90	RB WY	T09 WP0 BRI
58.	RC WY	TO9 MPD BRI
9F	CI	109 MPO (8.8) BR7 + 881 8821
\$G	RA	T09 UP3
KRPT	KRPT	TOS RUPTS
311	RB WA	TOS IIC2 + GVI BRLI
9XPS	RU TOV WSC	TOS DASO
51	RA RC BY	TO9 MASKO
5K	RC WA Z15	T09 DV4
91.	86 86	T09 DV4
SM	#C	TD9 DASI



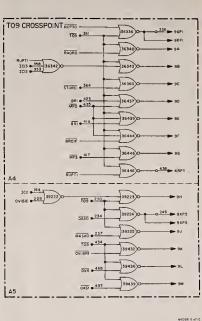


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 6 of 10)



	TIC	CROSSPOINT
SIGNAL	CONTROL	EQUATION
WPOTIO	ST1 TSCN	TIO MPC
IOA	RL.	TIO NP)
108	ST2 WY	TLD CCSO
10AP6	CI	TIO CCSO BR2
IOXP;	STI	TIO IICI +ICIO +RUPTO:
100	RA KY	TLO (DASD+WSUO BRI)
10xPF	MOMEX	TIO INSUO BRI + DASO BRI BRZ:
10XP0	PONEX	TIE UASO BRI BRZ
100	RU #B	TED (ICI4+IC2+OVI)
IOXPLO	A7X WY	TIO ICII
108	VL.	TIO (IC4+DV4 ERI + DAS) ADSO BR21
EXT	1x3	TIO NOXXI
10XP9	RB	T10   C6 + CC40 + A00 + CC10 BR1 BR2
LOF	9A	T10 (106 +107)
10G	RC	T10 (IC) + 0C50 + 5U0 + CC50 BRI BR2 + 0V4 BR11
LOXP15	SFI ST2	TIO MPI

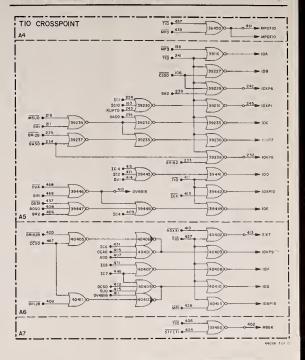


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 7 of 10)



	CONTROL	
IGNAL	PULSES	EQUATION
11A	SIC ABI	T33 MPO BRI
IIXP2	ลบร	THE MSUO
118	RC	TII MASKO
NIC	WA	T11 (MSUS 4 (C11)
IIxP6	RL WYD	TI) OVI
110	RC RG	TII 8XORG
311	RY WA	TII (CCS0+MP) BRI+QAS0+A0S0+  CII+QASI BR2

	TI2	CROSSPOINT	
SIGNAL	CONTROL PULSES	EQUATION	
12A	RU	TIZ-TIZUSE DVI	

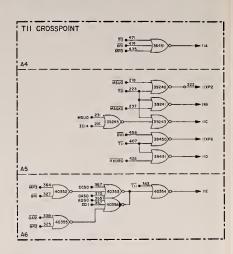
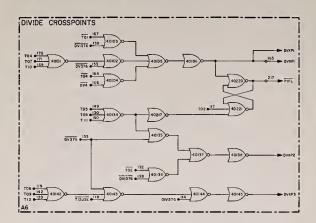




Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 8 of 10)





DIVIDE CROSSPOINTS							
SIGNAL	CONTROL PULSES	EQUATION					
DVXP1	AZX L2GD RB eyro	DVI385 T01+DV375 [T04+T07+T10] +DV4 T04					
PIFL	PIFL	DYXPI+(TO2+YO3+TO6+TIL) FIFL					
DVXP2	RG TSGU WL	DV3316 TC2+DV376 (TC5+TC8+T11)					
DVXP3	RU ¥8	DV376 (T06+T09+T12) T12USE+DIVSTO					

Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 9 of 10)

44096 9 6410



MULTIPLY CROSSPOINTS							
SIGNAL	CONTROL	EQUATION					
ZIP	A2X L2G0	ZXP7 + MP  (T0  + T0) + 105 + T07 + T09 + T01;					
M-bx-1	81	ZIP 16154 - 6074 - 6011 16154 6074 6011					
NPXP2	RYG	21P					
MCRD	WCRO	ZIP ILOZA - ILISA LOZA - LOJI					
ZIPCI	RC CI	ZIP LOZA - (LISA - LOZA LOZ) - (LISA LOZA LOZI					
MPXP3	R6	ZIP ILOZA + LISA LOZA LOZI ILISA LOZA LOZI					
ZAP	GPLS RU WALS	WP1 (102 + Y04 + Y04 + T03 + T10) +WP3 (Y01 + 103)					

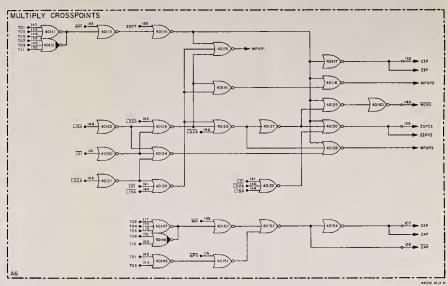


Figure 4-134. Crosspoint Generator, Logic Diagram (Sheet 10 of 10)



Attime pulse T05, crosspointpulses 5G and 5J are produced from commands CCS0 and IC12, respectively. Crosspoint pulse 5G may also be produced from command PARTC or PINC. Crosspoint pulse 5G produces control pulses RG, TMZ, TPZG, and TSGN. Control pulse RG places the content of register G onto the write lines. The branch flip-flops are set to the 00 state if register G and the write lines contain a positive quantity. Control pulse TSGN resets the branch 1 flip-flop and control pulses TMZ and TPZG reset the branch 2 flip-flop. Branch state 01 is established if register G contains a plus zero. Control pulse TSGN resets the branch 1 flip-flop and control pulse TPZG, in conjunction with the decoded output of register G, sets the branch 2 flip-flop. Branch state 10 is established if the write lines contain a negative quantity other than minus zero. Control pulse TSGN, in conjunction with signal WL16, sets the branch 1 flip-flop and control pulses TPZG and TMZ reset the branch 2 flip-flop. Finally, state 11 is established when the write lines contain minus zero. The branch 1 flip-flop is set by control pulse TSGN and signal WL16. The branch 2 flip-flop is set by signals WL16 through WL01 and control pulse TMZ. The output of the branch flip-flops are decoded into various branch command signals that are used for producing crosspoint pulses.

Crosspoint pulse 5J is converted into control pulses RG and WB. Control pulse RG is also produced from crosspoint pulse 5G, thus making one RG control pulse redundant. Control pulse RG places the content of register G onto the write lines. Control pulse WB transfers the write line information into register B, Crosspoint pulse 5J can only be produced by time pulse signal T05 and instruction command signal IC12. No crosspoint pulses are produced at time pulse T06 of subinstruction CCSO.

At time pulse T07, the state of the branch flip-flops determines what crosspoint pulses are produced. The control pulses at time pulse T07 will add plus zero, one, two, or three to the address c(Z) contained in register Z if the branch flip-flops are in state 00, 01, 10, or 11, respectively. Crosspoint pulse 7D is produced by signals T07 and CCS0 and is not dependent on the state of the branch flip-flops. Signal 7D is converted into control pulses RZ and WY12 which copy the twelve (12) low order bits of register Z into the adder register Y. Control pulse WY12 also clears adder register X and the carry flip-flop. If the branch flip-flops are in the 00 state, no further action occurs at time pulse T07 and the adder gates U contain c(Z) + 0 = c(Z). If the branch 2 flip-flop is set as it is for states 01 and 11, crosspoint pulse 7XP4 is produced. Signal 7XP4 is produced by time pulse T07, subinstruction command CCS0, and branch signal BR2. Crosspoint pulse 7XP4 is then converted into control pulse PONEX which sets bit 1 of adder register X. If the branch flip-flops are in the 01 state, no further action occurs at time pulse T07. As a result, the adder gates U contain c(Z) + 1. If the branch flipflops are in the 11 state, crosspoint pulse PTWOX is produced by signals T07, CCS0, and BR1. Signal PTWOX, which is used as the control pulse, sets bit 2 of register X. Since register X now contains octal three from the action of control pulses PONEX and PTWOX, the adder output gates contain c(Z) + 3. Had the branch flip-flops been set to state 10, only control pulse PTWOX would be produced and the output gates U would contain c(Z) + 2.

At time pulse T08, crosspoint pulse 8XP10 is produced and converted to control pulse WS. Signal 8XP10 is produced involuntarily every T08 time pulse except when inhibited by subinstruction commands RUPTO, DASO, or MP1 or instruction command DV1376. Control pulse WS is used for copying an address into register S. The address usually comes from register Z; however, It may also come from the priority control, peripheral equipment, register B or adder gates. Signals T08 and CCSO also produce crosspoint pulse 8A which is converted to control pulses RU and WZ. Control pulses RU, WZ, and WS enter the content of the adder gates U into registers Z and S. At time pulse T09, crosspoint pulse 9B is produced from signals T09 and IC12 and converted into control pulses RB and WB. Crosspoint pulse 9B may also be produced by signal RUPT1 or IC13. Control pulses RB and WB copy the content of register B into register G. This is the quantity that was originally taken out of erasable memory at time pulse memory location at time pulse T10. This action does not destroy the same data contained in register B.

Also at time pulse T10, control pulses WY and ST2 are produced from crosspoint pulse 10B. Control pulse ST2 sets the primary level flip-flops of the stage counter to 010 in preparation for subinstruction STD2. Control pulse WY clears register X and enters the content of the write lines Into register Y. If the branch flip-flops are set to state 01 or 11, no additional crosspoint and control pulses are produced. As a result, the adder gates U contain plus zero. If the branch 2 flip-flop is reset, as it is for states 00 and 10, crosspoint pulse 10XP6 is produced and converted to control pulses C1 and MONEX. Control pulse CI sets the carry flip-flop and control pulse MONEX sets register X to minus one or octal 177776. Crosspoint pulse 10XP6 is produced by signals TiO and CCSO, when signal BR2 is not present. If the quantity c(E) taken from erasable memory Is positive, the branch flip-flops will be in the 00 state. Crosspoint pulse 10XP9 will produce control pulse RB which in turn will copy the positive quantity in register B onto the write lines. Control pulse WY will then enter c(E) into register Y. The quantity c(E) in register Y, minus one in register X, and a carry bit results in c(E) -1 at the output gates U. If the original quantity in erasable memory was negative c(E), the branch flip-flops will be in state 10, and crosspoint pulse 10G will produce control pulse RC. Control pulse RC converts the negative quantity c(E) in register B into the equivalent positive quantity c(E) by gating the complement output of register B onto the write lines. As a result, the same net results are obtained as with a positive quantity, namely c(E) -1 at output gates U. Crosspoint pulse 10G is also produced by commands IC7, DCS0, SUO, and a particular branch condition during DV4.

The last action of subinstruction CCSO occurs at time pulse Til during which crosspoint pulse 11E is produced and converted into control pulses RU and WA. These control pulses cause the content of adder gates U to be copied into register A. Crosspoint pulse 11E is also produced from signals DASO, ADSO, ICII, and particular branch conditions of MP3 and DASI. Subinstruction CCSO is followed by subinstruction STDS.

Special attention is given to the divide instruction because the crosspoint circuit, which produces pulses DVXP1 through DVXP3 and PIFL, differs from the T01 through T12 crosspoint circuits (figure 4-134). The crosspoint and control pulses for subinstructions DV0, DV1, DV3, DV7, DV6, and DV4 are listed in tables 4-XIII through 4-XVII.

Table 4-XIII. Subinstruction DV0

	BRI	Involuntary		DV0		DIV	
Time	and BR2	XP CP		XP CP		XP CP	
1				1XP10	RA TMZ TSGN WB		
2	xx	$\triangle$				DVST	
2	0x			2XP5	RC TMZ WA		
3	2	DIVSTG (DVXP3)	RU WB				

 $\Lambda$ 

Crosspoint pulse 2B is inhibited by command DV0.

2

Crosspoint pulse DIVSTG is involuntary during the DV instruction. Crosspoint pulse DIVSTG also produces signal DVXP3 which is converted into control pulses RU and WB.

Table 4-XIV, Subinstruction DV1, Part 1

	BRI	Involu	ntary	ים	V1
Time	and BR2	XP	CP	XP	CP
4	XX			4K 4L	RL WB
4	X1			4D	TSGN
5	xx			B15X	WY
5	0X			5XP19	RB
5	1X			5R Z16	RC
6			į	6XP5	RU TOV WL
7				7A	RSC TSGN
				7F	RG WB
8	xx			8XP5	RA WY
8	X0	$\triangle$		8XP6	PONEX
9	0X			9 H	RB WA
9	1X			9K	RC WA Z15
10				10D	RU WB
11				11XP6	RL WYD
12				12A	RU WL

Crosspoint pulse 8XP10 is inhibited by command DV1.

Table 4-XV. Subinstructions DV3, DV7, and DV6, Part 1

							T		
	BRI	Involu	ntary	DV	376	Time	BR1 and	DVS	76
Time	and BR2	XP	CP	XP	CP		BR2	ХP	CP
5 5 5 6 7	xx 0x 1x	Δ		DVXP1  PIFL  DVXP3  DVXP1  PIFL  DVXP2	A2X L2GD RB WYD RG TSGU WL CLXC RB1F RU WB A2X L2GD RB WYD	8 8 9 10	0X 1X XX 0X 1X	DVXP3 DVXP1 PIFL DVXP2	CLXC RBIF RU WB A2X L2GD RB WYD  RG TSGU WL CLXC RBIF RU WB

A Crosspoint pulse 8XP10 is inhibited by command DV1376.

Table 4-XVI. Subinstructions DV1, DV3, DV7, and DV6, Part 2

Time	BRI	Involuntary		DV1376		D	IV
	BRZ	XР	CP	XP	CP	XP	СР
2 2 2 3	0X 1X	DIVSTG (DVXP3)	RU	DVXP1 PIFL DVXP2	A2X L2GD RB WYD RG WL TSGU CLXC RB1 F	DVST	

A Crosspoint pulse 8XP10 is inhibited by command DV1376.

Crosspoint pulse DIVSTG produces signal DVXP3 which is converted into control pulses RU and WB.

Table 4-XVII. Subinstruction DV4

	BRI	Involu	ntary	DI	74
Time	and BR2	XP	CP	XP	CP
4				DVXP1	A2X L2GD RB WYD
5	xx			5XP28	RG TSGU WB WA
5	0X				CLXC
5	1X				RB1 F
6				6X P7	RZ TOV
7	X1			7XP7	RC WA
7	1X			7XP7	RC WA
8		8XP10	WS	RSTSTG 8XP4	TSGN RZ ST2
9				9L	RU WB WL
10	0X			10E 10G	WL RC

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The crosspoint and control pulses for subinstruction DV0 and part 1 of subinstruction DV1 (tables 4-XIII and 4-XIV) are produced in the conventional manner by the T01 through T12 crosspoint circuits. The crosspoint pulses listed in tables 4-XV and 4-XVI and some of those listed in table 4-XVIII are produced by the divide crosspoint circuit. This circuit is controlled by instruction commands DV376; subinstruction command DV34: signals DIVSTG and T12USE; and all time pulses except T03. Instruction command DV3176 is used to produce crosspoint pulse DVXP1 at time pulse T01. Crosspoint pulse DVXP1 is also produced at time pulse T04, T07, and T10 by Instruction command DV376 and at time pulses T04 by subinstruction command DV376 converted into control pulses A2X, L2GD, RB, and WYD, by the control pulse gates. Control pulses CLXC and RB1F are discussed in detail in the branch control circuit description.

Signal DVXP1 is also applied to the set side of the PIFL flip-flop. Signals DVXP1 and PIFL occur simultaneously since the reset side of the PIFL flip-flop is pulsed at time pulses T02, T05, T08, and T11.

Crosspoint pulse DVXP2 is produced at time pulse T02 by instruction command DV1376 and at time pulses T05, T08, and T11 by instruction command DV376. This signal is converted into control pulses RC, TSCU, and WL.

Control pulse DIYSTG occurs at time pulse T03 of the divide subinstructions and produces crosspoint pulse DYXP3. Signal DYXP3 is also produced at time pulses T06, T09, and T12 When signals DV376 and T12USE are present. Signal T12USE is a flip-flop signal produced by the stage counter and decoder circuit. Crosspoint pulse DYXP3 is converted into control pulses RU and WB.

The multiply instruction also requires special consideration because the multiply crosspoint circuit fiffers from the conventional T01 through T12 crosspoint circuits. The multiply crosspoint circuit produces signals ZIP, ZAP, MPXP1, MPXP2, MPXP3, MCR0, and ZIPCI, as shown in figure 4-134 and listed in tables 4-XVII through 4-XXI. Crosspoint pulse ZIP is converted into control pulses APX and L2GD and is produced at time pulses T01, T03, T05, T07, T09, and T11 of subinstruction MP1. It is also produced by crosspoint pulse 2XP7 which occurs at time pulse T02 during subinstruction MP3.

Table 4-XVIII. Subinstruction MP0

	BRI	Involu	ntary	M	P0	IC	14
Time	and BR2	XP	CP	XP	CP	XP	CP
2		2B	RSC WG				
3				3C 3F	TSGN RA WB		
4	0X			4B	RB WL		
4	1X			4C	RC WL		
7				TSGN2		7 <b>F</b>	RG WB
8		8XP10	WS	8X P3	RZ		
9	0X			9D	RB WY		
9	1X			9E	RC WY		
9	01			9F	CI		
9	10			9 <b>F</b>	CI		1
10		$\triangle$		MP0T10	ST1 TSGN	100	RU WB
11	xx			10A	RL	11C	WA
11	1X			11A	R1C RB1		

Control pulse NEACON is produced in the adder at time period T10 and inhibits end around carry.

Table 4-XIX. Subinstruction MP1

	BR1	lnvolu	ntary	MP	1
Time	and BR2	XP	CP	ХP	СР
1			2	ZIP	A2X L2GD
2		Δ		ZAP	G2LS RU WALS
3				ZIP	A2X L2GD
4				ZAP	G2 LS RU W ALS
5				ZIP	A2X L2GD
6				ZAP	G2LS RU WALS
7				ZIP	A2X L2GD
8			).	ZAP	G2LS RU WALS
9				ZIP	A2X L2GD
10				ZAP	G2LS RU WALS
				10XP15	ST1 ST2
11				ZIP	A2X L2GD

↑ Crosspoint pulses 2B and 8XP10 are inhibited by command MP1.

See table 4-XXI for additional crosspoint pulses produced by ZIP.

Table 4-XX. Subinstruction MP3

	BRI	Involu	ntary	MI	23
Time	and BR2	XP	CP	ХP	CP
1				ZAP	G2LS RU WALS
2		A	<u> 2</u>	ZIP	A2X L2GD
3				ZAP	G2LS RU WALS
4				4E	RSC WG
5				5P	RZ WY12 CI
6		<u> </u>		TL15 6D	RU WZ
7	1X			7XP19	A2X RB WY
8	1	8XP10	ws	RAD	WB
9				9G	RA
10				10A	RL
11	1X			11E	RU WA

Crosspoint pulse 2B is inhibited by command MP3.

See table 4-XXI for additional crosspoint pulses produced by ZIP.

Control pulse NEACOF is produced in the adder at time period T06 and permits end around carry.

Table 4-XXI. Crosspoint Pulse ZIP

c(L)	ZIP	
15, 2, 1	XP	CP
000	MPXP1	WY
001	MPXP1 MPXP3	WY RB
010	MPXP2 MPXP3	WYD RB
011	MPXP1 ZIPCI	WY RC CI
100	MCR0 MPXP1 MPXP3	WY RB
101	MPXP2 MPXP3	WYD RB
110	MPXP1 ZIPCI	WY RC CI
111	MCR0 MPXP1 MCR0	WY

Crosspoint pulses MPXP1 through MPXP3, MCRO, and ZIPCI are dependent on the star of bits 15, 2, and 1 of register L and are produced in conjunction with crosspoint pulse ZIP. Table 4-XXI lists the crosspoint and control pulses produced by signal ZIP for all possible states of these bits. Crosspoint pulse MPXP1 is produced and converted into control pulse WP for all states except 010 and 101. During states 010 and 101, crosspoint pulse MPXP2 is produced instead of MPXP1 and converted into control pulse WYD. Control pulse RB is produced from crosspoint pulse MPXP3 during states 001, 010, 100, and 101 whereas control pulses RC and CI are produced from ZIPCI during states 011 and 110. In addition, crosspoint pulse MCRO is produced during states 011, 110, and 111 and used directly as a control pulse.

Crosspointpulse ZAP is produced and converted into control pulses G2LS, RU, and XL at time pulses T02, T04, T06, T08, and T10 of subinstruction MP1. It is also produced at time pulses T01 and T03, during subinstruction MP3.

During the multiply instruction, the adder is switched to perform arithmetic in the two's complement system. Switching is accomplished by signal NEACON which occurs at time pulse T10 of subinstruction MPO. Signal NEACON sets a flip-flop (part of the adder) which inhibits end around carry until it is resetby signal NEACOF at time pulse T06 of subinstruction MP3.

Tables 4-XXII through 4-LXXIV list the crosspoint and control pulses produced for the remaining subjustructions.

4-5, 4.11 Control Pulse Gates. The control pulse gates (figure 4-135) convert crosspoint pulses into control pulses. For example, control pulse NISQ is produced by crosspoint pulse 2XP37, or 8XP15. A single crosspoint pulse may produce several control pulses. For example, crosspoint pulse 2XP5 produces control pulses RC, TMZ, and WA. Two control pulses, CLXC and RBIF, produced from control pulses TSGU, signal PHS4, and a branch signal, occur during the divide instruction. Only one is produced at a time. Control pulse CLXC is produced when the branch flip-flops are in the OX state and control pulse RBIF is produced during the IX state. Control pulse TSGU is produced by crosspoint pulse 5XP28 or DVXP2. Table 4-LXXV lists all of the control pulses produced by the control pulse gates and other circuits.

Table 4-XXII. Subinstruction STD2

	BR1	Involuntary		ST	STD2		3
Time	and BR2	XP	CP	XР	CP	XР	CP
1				1C	RZ	1A	WY12 CI
2		2B	RSC WG			2C	NISQ
6						6D	RU WZ
8		8XP10	ws			RAD	WB

Table 4-XXIII. Subinstruction TC0

Time BR1 and BR2		Involuntary		TC0		IC3	
	XP	CP	XР	CP	XP	CP	
1				10	RB	1A	WY12 CI
2		2B	RSC WG			2C	NISQ
3				3XP6	RZ WQ		
6						6D	RU WZ
8	'	8XP10	ws			RAD	WB

Table 4-XXIV. Subinstruction TCF0

				- Descripti	action 1		
	BR1 and	Involuntary		тс	TCF0		C3
BR2		XP	CP	XP	CP	XP	CP
1				1D	RB	1A	WY12 CI
2	j	2B	RSC WG			2C	NISQ
6						6D	RU WZ
8		8XPI0	ws			RAD	WB

Table 4-XXV. Subinstruction TCSAJ3

Time	BR1 and BR2	Involu	ntary	TCSAJ3		
Time		XP	CP	XР	CP	
2		2B	RSC WG			
8		8XP10	ws	8E	WZ ST2	

Table 4-XXVI. Subinstruction GOJ1

Time	BR1 and	Involu	ntary	GOJ1		
Time	BR2	XP	CP	XР	CP	
2		2B	RSC WG			
8		8XP10	ws	8D RSTRT	WB	

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Table 4-XXVII. Subinstruction DAS0

	BRI	lnvolu	ntary	DA	S0	10	210
Time	and BR2	XP	CP	XP	CP	XР	CP
1				RL10BB	ws	1A 1B	CI WY12 MONEX
2		2B	RSC WG				
3				3F	RA WB		
4				4H	RL WA		
5				5XP12	RU WL		
6				6B	A2X RG WY		
7				7B 7G	RB WA		
8		$\triangle$		8D 8XP12	WB RL		
9				9XP5	RU TOV WG WSC		
10	xx			10C	RA WY	10XP1	ST1
10	01			10XP8	PONEX		
10	10			10XP7	MONEX		
11				11E	RU WA		

A Crosspoint pulse 8XP10 is inhibited by command signal DAS0.

Table 4-XXVIII. Subinstruction DAS1

				T Tuestion DA	
Time	BR1 and	1nvolu	ntary	DA	S1
Time	BR2	XP	CP	XP	CP
1 2		2B	RSC WG	RL10BB	ws
5				5K 5L	RG A2X WY
6				6XP8	RU TOV WG WSC
7	xx			7G	WA
7	01			7XP10	RB1
7	10			7XP11	R1C
8		8XP10	ws	8XP4	RZ ST2
9				9M	RC TMZ
10	X0			10E	WL
11	01			11E	RU WA

Table 4-XXIX. Subinstruction LXCH0

Audio 1 Sustingui della prictio										
	BRI	Involu	ntary	IC8		IC9				
Time	Time and BR2	XР	CP	XР	CP	XР	CP			
1						RL10BB	WS			
2		2B	RSC WG							
3				3G	RL WB					
5				5XP13	RG WL					
7						7J	RB WG WSC			
8		SXP10	ws			8XP4	RZ ST2			

Table 4-XXX, Subinstruction INCR0

BR1		Involuntary		INCR0		PRINC	
Time	BR2	XP	CP	XP	CP	ХÞ	CP
2		2B	RSC WG			RL10BB	WS
5						5G	RG TMZ TPZG TSGN
6				6XP10	PONEX	5L	WY
7						7H WOVR	RU WG WSC
8		8XP10	ws			8XP4	RZ ST2

Table 4-XXXI. Subinstruction ADS0

	BRI	Involuntary		AI	080	DA	S1
Time	and BR2	XР	CP	XP	CP	XР	CP
1						RL10BB	ws
2		2B	RSC WG				
5						5 <b>K</b>	RG A2X
						5L	WY
6						6XP8	RU TOV WG WSC
7	xx					7 <b>G</b>	WA
7	01					7XP10	RB1
7	10					7XP11	R1C
8		8XP10	ws			8X P4	RZ ST2
9						9M	RC TMZ
11	xx			11E	RU WA		
11	01					11 E	RU WA

Table 4-XXXII. Subinstructions CA0 and DCA1

Table 1-MAMI. Submistractions CAV and BCAT											
Time ar	BRI	Involuntary		10	IC6		C13				
	and BR2	XP	СР	XP	CP	ХP	CP				
2		2B	RSC WG								
7						7 F	RG WB				
8		8XP10	ws	8XP4	RZ ST2						
9						9 B	RB WG				
10				10XP9 10F	RB WA						

Table 4-XXXIII. Subinstructions CS0 and DCS1

Time	BR1 and	Involuntary		10	27	IC13	
Time	BRZ	XP	CP	XP .	CP	XP	CP
2		2 B	RSC WG				
7						7 F	RG WB
8		8XP10	ws	8XP4	RZ ST2		
9						9B	RB WG
10				10G 10F	RC WA		

Table 4-XXXIV. Subinstruction NDX0

			111010		- Duoxiiovi	dotton 1.2			
	BR1	Involu	ntary	NDX0		IC1		IC13	
Time	and BR2	XP	CP	XР	CP	XР	CP	XP	CP
2		2B	RSC WG						
5 7				TRSM				7F	RG WB
8		8XP10	ws			8XP3	RZ	9B	RB WG
10						10XP1	ST1		

Table 4-XXXV. Subinstruction RSM3

	BR1	Involu	ntary	RSM3		
Time	and BR2	XP	CP	XP	CP	
1				R15		
2		2B	RSC WG	2C	NISQ	
5				5XP4	RG WZ	
6				6A	RB WG	
8		8XP10	ws	RAD	WB	

Table 4-XXXVI. Subinstruction NDX1

	BRI	Involu	ntary	I	72
Time	and BR2	XP CP		XР	CP
1				1A	WY12 CI
				1C	RZ
2		2B	RSC WG	2C	NISQ
3				3XP5	RB WZ
4				4F 4L	RA WB
5				5 H 5 S	RZ WA
6				6D	RU WZ
7			į	7C	A2X RG WY
8		8XP10	ws	8C	RU
9				9 H	RB WA
10				10D	RU WB

Table 4-XXXVII. Subinstruction XCH0

Time	BR1 and	Involu	ntary	IC	C5	IC	9
Time	BR2	XP	CP	XP	CP	XP	CP
1						RL10BB	ws
2		2 B	RSC WG				
3				3F	RA WB		
5				5Q 5S	RG WA		
7						7J	RB WG WSC
8		8XP10	ws			8XP4	RZ ST2

Table 4-XXXVIII, Subinstruction DXCH0

	BRI	Involu	ntary	DXC	:H0	IC	8	IC	10
Time	and BR2	XP	CP	XP	CP	XP	CP	XP	CP
1 2 3		2B	RSC WG	RL10BB	ws	3G 5XP13	RL WB RG WL	1A 1B	WY12 CI MONEX
7				73	RB WG WSC		WL		
8		8XP10	ws	8C 8D	RU WB			10XP1	STI

Table 4-XXXIX. Subinstruction DXCH1

	BRI	Involu	ntory	IC	15	IC	a
Time	and						
	BRZ	XP	CP	XP	CP	XP	CP
1						RL10BB	ws
2		2B	RSC WG				
3				3F	RA WB		
5				5Q 5S	RG WA		
7						73	RB WG WSC
8		8XP10	ws			8XP4	RZ ST2

Table 4-XL. Subinstruction TS0

Time	BR1 and	Involu	ntary	Т	'S0	IC	9
Time	BR2	XP	CP	XP	CP	XP	CP
1						RL10BB	WS
2		2B	RSC WG				
3				3XP2 3F	TOV RA WB		
4	XX			4XP5	RZ WY12		
4	01			4A	CI L16		
4	10			4A	CI L16		
5	01			5E 5S	RB1 WA		
5	10			5 F 5S	R1C WA		
6				6D	RU WZ		
7						7J	RB WG WSC
8		8XP10	WS			8XP4	RZ ST2

Table 4-XLI. Subinstruction AD0

Time	BR1 and	Involu	ntary	AD0		IC	11	IC	13
Time	BRZ	XP	CP	XP	CP	XP	CP	XP	СР
2		2B	RSC WG						
7								7F	RG WB
8		8XP10	WS			8XP4	RZ ST2		
9								9B	RB WG
10				10XP9	RB	10XP10	A2X WY		
11						11E	RU WA		

Table 4-XLII. Subinstruction MASK0

	BRI	Involu	ntary	MAS	K0	IC1	.4
Time	and BR2	XP	CP	XP	CP	XР	CP
2		2B	RSC WG				
3				3F	RA WB		
4				4J	RC WA		
7						7 F	RG WB
8		8XP10	ws	8XP4	RZ ST2		
9				9J	RA RC WY		
10						10D	RU WB
11				11B	RC	11C	WA

Table 4-XLIII. Subinstruction BZF0

	BR1	Involu	ntary	IC	15	IC	16	IC	17
Time	and BR2	XР	CP	XР	CP	XР	CP	XP	CP
2		2B	RSC WG						
3				3E	RA TMZ TSGN WG				
4				4G	TPZG				
5	Х1					5 N	RB WY12 CI		
6	X1					6D	RU WZ		
8	xx	8XP10	WS					1	
8	X1					RAD 8XP15	WB NISQ		
8	X0	2						8XP4	RZ ST2

A Branch condition X1 produces command IC16.

2 Branch condition X0 produces command IC17.

Table 4-XLIV. Subinstruction MSU0

	BRI	Involu	ntary	MS	710	IC	12
Time	and BR2	XP	СР	XP	CP	XP	CP
1 2 5		2B	RSC WG			RL10BB	WS RG WB
6 7 8 9		8XP10	ws	6C 7XP9 7G 8XP4	A2X CI RC WY RUS TSGN WA RZ ST2	9B	RB WG
10	1X			10C 10XP7 11XP2 11C	RA WY MONEX RUS WA		

Table 4-XLV. Subinstruction QXCH0

					raceton &	150110	
Time	BRI	Involu	ntary	QX	CH0	IC9	
17/ille	BRZ	ХP	CP	XP CP		XP CI	
1						RL10BB	WS
2		2B	RSC WG				
3				RQ	WB		
5				5XP15	RG WQ		
7						7J	RB WG WSC
8		8XP10	ws			8XP4	RZ ST2

Table 4-XLVI. Subinstruction AUGO

Time	BR1 and	Involu	intary	A	UG0	PR	INC
	BR2	XP	CF	XP	CP	XP	CP
1 2 5 6 6 7	0X 1X	2B	RSC WG	6XP10 6E	PONEX MONEX	RL10BB 5G 5L 7H WOVR 8XP4	RG TMZ TPZG TSGN WY RU WG WSC RZ ST2

Table 4-XLVII. Subinstruction DIM0

m'	BRI	Involu	ntary	DI	м0	PRI	NC
Time	and BR2	XP	CP	XP	CP	ХÞ	CP
1						RL10BB	WS
2		2B	RSC WG				
5						5G	RG TMZ
						5L	TPZG TSGN WY
6	00			6E	MONEX		
6	10			6XP10	PONEX		
7						7H WOVR	RU WG WSC
8		8XP10	ws			8XP4	RZ ST2

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	13	CP				RG WB		RB	\$
	IC13	XP				7 E		9.8	,
	0	CP	CI WY12	MONEX					STI
04	IC10	XP	1A	113					10XP1
ction DC	4	CP	RB		·	•	RU		WL
Table 4-XLVIII. Subinstruction DCA0	IC4	ΧЪ	110				90		10E
-XLVIII.	Α0	СР							RB
Table 4	DCA0	ХЪ							10XP9
	ıtary	CP			RSC		WS		
	Involuntary	ΧÞ			2B		8XP10		
	BRI	and BR2		-					
		Time			63	t-	œ	6	10

Table 4-XLIX. Subinstruction DCS0

	IC13	CP				RG		RB	
	or	XP				7 F		9.8	
	IC10	CP	CI	MONEX					STI
SO	or	dХ	1A	113					10XP1
Table 4-XLIX. Subinstruction DCS0	IC4	CP	RB				RU		WL
Subinstr	и	dХ	110				8C		10E
4-XLIX.	DCS0	CP							RC
Table	DC	XP							10G
	ntary	CP			RSC WG		WS		
	Involuntary	XP			2B		8XP10		
	BRI	BR2							
	Limb C	amr			01	-	80	6	10

Table 4-L. Subinstruction SU0

m	BRI	Involu	ntary	st	JO	IC	11	I	C13
Time	and BR2	XP	CP	XP	CP	ХP	CP	ХP	СР
2		2B	RSC WG						
7								7 F	RG WB
8		8XP10	ws			8XP4	RZ ST2		
9								9B	RB WG
10				10G	RC	10XP10	A2X WY		
11						11E	RU WA		

Table 4-LI, Subinstruction NDXX0

Time	BRI	lnvolu	ntary	IC	1	IC	:13
Time	and BR2	XP	CP	XP	CP	XP	CP
2		2B	RSC WG				
7						7F	RG WB
8		8XP10	ws	8XP3	RZ		1
9						9B	RB WG
10				10XP1	STI		

Table 4-LII. Subinstruction NDXX1

		1 1101		ubinstruc	TON MDZEZ	**	
Time	BR1 and	Involu	ntary	ND	CX1	IC	C2
Time	BR2	XP	CP	XP	CP	XP	CP
1						1A 1C	WY12 CI RZ
2		<b>2</b> B	RSC WG			2C	NISQ
3						3XP5	RB WZ
4			l			4F 4L	RA WB
5						5H 5S	RZ WA
6						6D	RU WZ
7						7C	RG WY
8		8XP10	WS	•		8C	RU
9						9H	RB WA
10				EXT		10D	RU WB

Table 4-LIII. Subinstruction BZMF0

Time	BR1 and	Involu	ntary	IC	15	IC	16	IC	217
Time	BR2	XР	CP	XP	СР	XP	CP	XP	СР
2		2B	RSC WG						
3				3E	RA TMZ TSGN WG				
4		_	1	4G	TPZG				
5	<b>X</b> 1	1				5N	RB WY12 CI		
5	1X					5N	RB WY12 CI		
6	Х1					6D	RU WZ		
6	1X					6D	RU WZ		
8	X1					RAD 8XP15	WB NISQ		
8	1X	_				RAD 8XP15	WB NISQ		
8	00	2						8XP4	RZ ST2
8	ХХ	8XP10	WS						

A Branch condition XI or 1X produces command IC16.

2 Branch condition 00 produces command IC17.

Table 4-LIV. Subinstruction READO

	BRI	Involu	ntary	RE	AD0	INO	UT
Time	and BR2	XP	CP	XP	CP	XP	CP
1					RL10BB	WS	
2		$\triangle$			2XP3	RA WB	
3					3D	WY	
4					4XP11 4L	RCH WB	
5				5A 5S	RB WA	2	
6						6XP2	RA WB
8		8XP10	ws			8XP4	RZ ST2

A Crosspoint pulse 2B is inhibited by command INOUT.

2 Crosspoint pulse 5XP11 is inhibited by command READO.

Table 4-LV. Subinstruction WRITE0

Time	BR1 and	Involu	ntary	WRI	LE0	INOUT	
Time	BRZ	XP	CP	XP	CP	XP	CP
1						RL10BB	ws
2		$\triangle$		2A	WG	2XP3	RA WB
3						3D	WY
4						4XP11 4L	RCH WB
5				5B	RA WCH	2	
6						6X P2	RA WB
8		8XP10	ws			8XP4	RZ ST2

A Crosspoint pulse 2B is inhibited by command INOUT-

2 Crosspoint pulse 5XP11 is inhibited by command WRITEO.

Table 4-LVI. Subinstruction RANDO

Time	BR1 and	Involu	ntary	RAI	ND0	INO	UT
Time	BR2	XP	CP	XР	CP	XP	CP
1						RL10BB	WS
2		Δ				2XP3	RA WB
3				3B	RC	3D	WY
4						4XP11 4L	RCH WB
5				5R	RC	5XP11	RU WA
6						6XP2	/ RA WB
7				7XP7	RC WA		
8		8XP10	ws			8XP4	RZ ST2

1 Crosspoint pulss 2B is inhibited by command INOUT.

Table 4-LVII. Subinstruction WANDO

T1	BR1 and	Involu	ntary	WAI	ND0	INOI	JT
Time	BR2	XP	CP	XP	CP	XP	CP
1	-					RL10BB	ws
2		$\triangle$				2XP3	RA WB
3				3B	RC	3D	WY
4						4XP11 4L	RCH WB
5				5R	RC	5XP11	RU WA
6						6XP2	RA WB
7				7XP7	RC WA		
				7XP14	WCH	l i	
8		8XP10	ws			8XP4	RZ ST2

A Crosspoint pulse 2B is inhibited by command INOUT.

Table 4-LVIII. Subinstruction ROR0

	BRI	Involu	Involuntary		ROR0		UT
Time	and BR2	XP	CP	XP	CP	XР	CP
1						RL10BB	WS
2		$\triangle$				2XP3	RA WB
3				3A	RB	3D	WY
4						4XP11 4L	RCH WB
5				5XP19	RB	5XP11	RU WA
6						6XP2	RA WB
8		8XP10	WS			8XP4	RZ ST2

1 Crosspoint pulse 2B is inhibited by command INOUT.

Table 4-LIX. Subinstruction WOR0

	BRI	Involu	ntary	wo	R0	INOU	Т
Time	and BR2	XP	XP CP XP CP		XP	CP	
1						RL10BB	WS
2		$\triangle$				2XP3	RA WB
3				3A	RB	3D	WY
4						4XP11	RCH WB
5				5C 5XP19	WCH RB	5XP11	RU WA
6						6XP2	RA WB
8		8XP10	ws			8XP4	RZ ST2

Table 4-LX. Subinstruction RXOR0

	BR1	Involu	ntary	RXC	ono	INOT	JT	IC	14
Time	and BR2	XP	CP	XP	CP	XP	CP	XP	СР
1 2		<u>^</u> î				RL10BB 2XP3	WS RA WB		
3				3XP7	RC RCH	3D	WY		
4						4XP11 4L	RCH WB		
5				5D	RA RC WO	2			
7				- 1				7F	RG WB
8		8XP10	ws			8XP4	RZ ST2		
9				9A	RC WG				
10				1				10D	RU WB
11				11D	RC RG			11C	WA

1 Crosspoint pulse 2B is inhibited by command INOUT.

Crosspoint pulses 5XP11 and 6XP2 are inhibited by command RXOR0.

Table 4-LXI. Subinstruction RUPTO

Time	BR1 and	Involu	ntary	RUI	PT0
Time	BR2	XP	CP	XP	CP
1				R15	WS
2		2B	RSC WG		
9		$\triangle$		9XP1	RZ WG
10				10XP1	ST1

Crosspoint pulse 8XP10 is inhibited by command RUPT0.

Table 4-LXII. Subinstruction RUPT1

	BR1 and	1nvolu	ntary	RUPTI			
Time	BRZ	XP	CP	XP	CP		
1				R15 RB2	WS		
2		2B	RSC WG				
3	ļ			RRPA	WZ		
8		8XP10	ws	8XP4	RZ ST2		
9				9B KRPT	RB WG		

Table 4-LXIII. Subjection PINC

mı	BRI	Involut	ntary	PII	1C	PA	RTC	INK	L
Time	and BR2	XP	CP	XP	CP	ХP	СР	XP	CP
1								RSCT	WS
2		2B	RSC WG						
5			WG			5G	RG		
							TMZ TPZG		
							TSGN		
						5 L	WY		
6	i			6XP10	PONEX				
7				7H	RU			WOVR	WG WSC
8		8XP10	ws					8B	RB

Table 4-LXIV. Subinstruction MINC

Time	BRI	Involu	ntary	MI	NC	PA	RTC	INK	L
Tine	BR2	XP	CP	XP	CP	XP	CP	XP	CP
1								RSCT	ws
2		2В	RSC WG						
5						5G	RG TMZ		
						0.7	TPZG TSGN		
				0.5		6 L	WY		
6				6E	MONEX				
7	ļ			7H	RU			WOVR	WG WSC
8	ļ.,	8XP10	ws					8B	RB

Table 4-LXV. Subinstruction PCDII

			Table	4-LXV.	Subinstru	ction PCI	70		
	BRI	Involur	itary	PCI	υu	PAF	RTC	INKL	
Time	and BRZ	XP	CP	XP	CP	XP	CP	XP	CP
1								RSCT	WS
2		2B	RSC WG						
5						5G	RG TMZ TPZG		
						5L	TSGN WY		
ß				6XP12	CI				
7				7XP15	RUS			WOVR	WG WSC
8		8XP10	ws					8B	RB

Table 4-LXVI, Subinstruction MCDU

	BR1	Involu		MC	DII	PAI		INKI	
Time	and BR2	XP	CP	XP	CP	XP	CP	XP	CP
1 2 5		2B	RSC WG			5G 5L	RG TMZ TPZG TSGN WY	RSCT	WS
6				6E 6XP12 7XP15	MONEX CI RUS			wovr	WG
8		8XP10	ws					8B	WSC RB

Table 4-LXVII. Subinstruction DINC

	BRI	T		T	Subinstri				
Time	and	Invoi	ntary	D.	INC	PA	RTC	IN	KL
	BRZ	XP	CP	XP	CP	XP	CP	XP	CP
1								RSCT	ws
2		2B	RSC WG						
5						5G	RG TMZ		
							TPZG		
			_			5 <b>L</b>	WY		
6	00		$\triangle$	POUT 6E	MONEX				
6	10			MOUT	MONEX				
				6XP10	PONEX				ĺ
6	X1			ZOUT					
7				7 H	RU			WOVR	WG WSC
8		8XP10	WS					8B	RB

 $\Lambda$ 

Crosspoint pulses POUT, MOUT, and ZOUT are three (3) microseconds long, starting at time period T06 and ending with time period T08.

Table 4-LXVIII, Subinstruction SHINC

	Table 4-LAVIII. Subinstruction Shine												
	BRI	Involu	ntary	SHI	FT	INK	L						
Time	BR2	XP	CP	XP	CP	XP	CP						
1						RSCT	WS						
2		2B	RSC WG										
5				5XP9	RG TSGN WYD								
7						wovr	WG WSC						
8		8XP10	WS			8B	RB						

Table 4-LXIX. Subinstruction SHANC

	BRI	Involu	ntary	SHA	NC	SHI	SHIFT INKL		L
Time	and BR2	XP	CP	XP	CP	XP	CP	XP	CP
1								RSCT	WS
2		2B	RSC WG						
5			wG	5M	CI	5XP9	RG TSGN WYD		
7								WOVR	WG WSC
8		8XP10	ws					8B	RB

Table 4-LXX. Subinstruction INOTRD

	Table + LEGIT business were a											
Time	BR1 and BR2	Involuntary		CHINC		INKL						
		XP	СР	XР	CP	XP	CP					
1				1E	ws	Λ						
2		2B	RSC WG									
5				5XP21	RCH							
8		8XP10	ws			8B	RB					

Crosspoint pulses RSCT and WOVR are inhibited by command MON+CH.

Table 4-LXXI, Subinstruction INOTLD

	Table 1 India banks account in a second												
Time	BRI and BR2	Involuntary		INOTLD		CHINC		INKL					
		XP	CP	XР	CP	XP	CP	XP	CP				
1						1E	ws	$\triangle$					
2		2B	RSC WG										
5						5XP21	RCH						
7				7XP14	WCH								
8		8XP10	ws					8B	RB				

A Crosspoint pulses RSCT and WOVR are inhibited by command MON+CH.

Table 4-LXXII. Subinstructions FETCH0 and STOREO

Time	BR1 and BR2	Involu	ntary	FETCH0		MON		INKL	
		XP	CP	XP	CP	XP	CP	XP	CP
2		2B	RSC WG	R6 2XP8	WS ST1 WY			Λ	
8		8XP10	ws			4 M	WSC	2	

Crosspoint pulses RSCT and WOVR are inhibited by command MON+CH.

2 Crosspoint pulse 8B is inhibited by command MON.

Table 4-LXXIII. Subinstruction FETCH1

Time	BR1 and	Involu	Involuntary		MON		STFET1		CL CL
	BR2	XP	CP	XP	CP	XP	CP	XP	CP
2		2B	RSC WG	À				2	
7 8 10		8XP10	WS			7E U2BBK RBBK	RG	8B	RB

A Crosspoint pulse 4M is inhibited by command FETCH1.

A Crosspoint pulses RSCT and WOVR are inhibited by command MON+CH.

. Crosspoint pulse U2BBK may be inhibited by signal MONWBK from the peripheral equipment.

tion STORE1	В	CP				RB		
	INKT	ΧP				8B		
	STORE1	CP					WG	
	STC	ΧP					90	
	STFETI	CP			RG	⊘		
Subinstruc	ST	ξX			7E	UZBBK		RBBK
Table 4-LXXIV. Subinstruction STORE1	MON	CP		WSC				
	MC	XP		4M				
	ntary	CP	RSC			WS		
	Involuntary	XP	2B			8XP10		
	BRI							
Į	Į.		2	4	7	∞	6	10

Crosspoint pulses RSCT and WOVR are inhibited by command MON+CH. €

Crosspoint pulse U2BBK may be inhibited by signal MONWBK from the peripheral equipment.

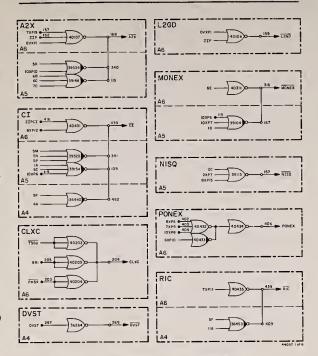


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 1 of 6)

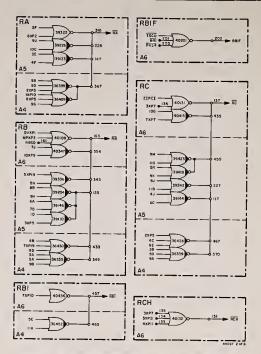


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 2 of 6)

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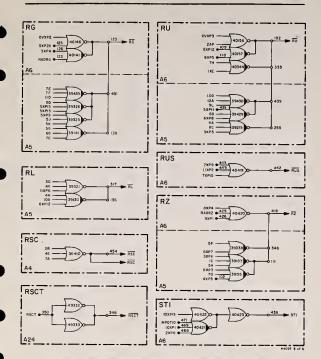


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 3 of 6)

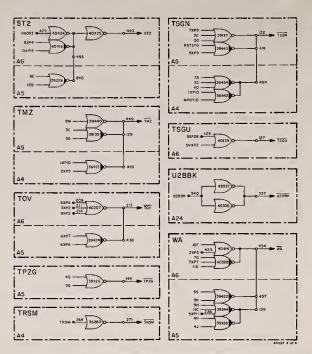


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 4 of 6)

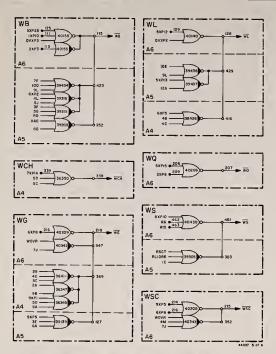


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 5 of 6)

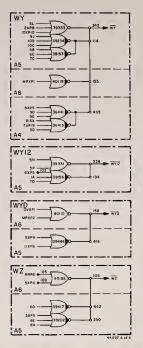


Figure 4-135. Control Pulse Gates, Logic Diagram (Sheet 6 of 6)

Table 4-LXXV. Control Pulse Origin

	Table 4-IMAV.				
Circuit	Control Pulses	Circuit	Control Pulses		
T01 crosspoint	R15 RB2 RL10BB	Control pulse gates (cont)	NISQ PONEX RIC		
T03 crosspoint	RRPA RQ		RA RB RB1		
T04 crosspoint	L16 (4A)		RB1F RC		
T05 crosspoint	B15X Z16		RCH RG RL RSC		
T06 crosspoint	T L15		RSCT		
T07 crosspoint	TSGN2 PTWOX WOVR		RU RUS RZ ST1		
T08 crosspoint	RAD RSTRT RSTSTG Z15 (9K)		ST2 TMZ TOV TPZG TRSM		
T09 crosspoint	KRPT		TSGN TSGU		
T10 crosspoint	EXT RBBK		U2BBK WA WB		
Divide crosspoint	PIFL		WCH WG WL		
Multiply crosspoint	MCR0 ZIP ZAP		WQ WS WSC		
Control pulse gates	A2X C1 CLXC DVST		WY WY12 WYD WZ		
	L2GD MONEX	L service	G2LS WALS		

(Sheet 1 of 2)

Table 4-LXXV. Control Pulse Origin

Circuit	Control Pulses	Circuit	Control Pulses
Channel 14	POUT MOUT ZOUT	Register EB	REB WEB
Adder	NEACOF NEACON	Register FB	RFB WFB WBBK
Register SQ control	WSQ	Stage Counter	DIVSTG (STAGE)

## (Sheet 2 of 2)

4-5, 4, 12 <u>Branch Control</u>. The branch control (figure 4-136) consists of the branch flip-flops, branch decoder, and special instruction flip-flop. The branch flip-flops and decoder control up to four different sets of control pulses at a given time during various subinstructions. The special instruction flip-flop controls two sets of control pulses at a given time depending on whether or not the next instruction to be executed is special instruction RELINT, INHINT, or EXTEND.

The branch 1 flip-flop is used to test the sign bit and the negative overflow bits of any word placed onto the write lines. It also tests bit 15 of register L and bit 16 of the adder. These tests are performed by control pulses TSGN, TOV, TL15, and TSGU, respectively. The test control pulses are similar to write control pulses in that they are used to clear the flip-flop register before or during the write process. As a result, the output of the branch flip-flops cannot be used until the final state is established. Normally all control pulses produced from a branch condition occur one or more time periods after the test control pulses. For example, test control pulse TOV of subinstruction TSO will establish a new state for the branch flip-flops at time pulse TOS. The control pulses resulting from the state of the branch flip-flops are produced at time pulses T04 and TOS.

A special case exists for the divide instruction. Control pulse TSGU does not set or reset the branch 1 flip-flop in the normal maner. Bit position 16 of the adder is used as a primary level device with the branch 1 flip-flop being the secondary level device. Control pulse TSGU transfers bit 16 of the adder to the branch 1 flip-flop. If bit 16 is a logic ONE (signals SUMA16 and SUMB16 are present) and the branch 1 flip-flop is aiready set, no change of state occurs. Signal TSGU is gated by signal PHS3. Therefore, the final state of the branch flip-flop is established 1/4-microsecond before



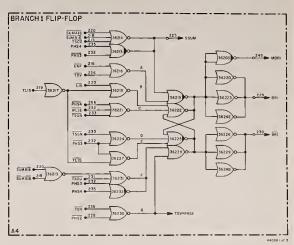
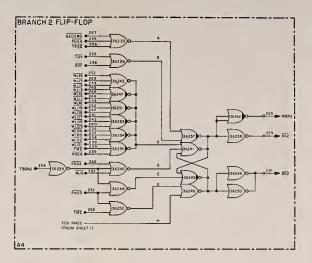
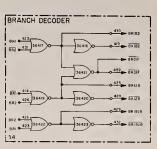


Figure 4-136. Branch Control, Logic Diagram (Sheet 1 of 3)







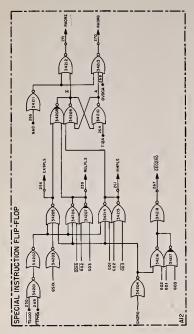


BRANCH DECODER							
SIGNAL	EQUATION						
98182	BAI BRZ						
BROLF	881 982 + 881 6A2						
BR178	991 BR2						
953188	9R1 9R2						

Figure 4-136. Branch Control, Logic Diagram (Sheet 2 of 3)



44098A 3143



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	SPECIAL INSTRUCTION FLIP-FLOP			312 COLA	15 (5)		TISK		
I	TION	×o	ZRO CSIX	TZPHS4 TSUDO GNZRO GGJ G02 G01A	TIPHSA TSUDO CNZRO CQU CTZ COT	M	EXTPLS + RELPLS + INHPLS + A TIZA		
ı	STRUC	EQUATION	TYPHS4 TSUDG GWZRO GSIX	TSUES ON	TSUDO CH	CNZHO COS COS COS	+ 8518138		
	AL IN		TYPHS4	TZPHS4	TIPHSA	GNZRO	EXTPLS	A RAD	A RAD
	SPECI	SIGNAL	EXTPLS	RELPLS	SHPLS	GEQ 280		RADRZ	RADRG

Figure 4-136. Branch Control, Logic Diagram (Sheet 3 of 3)

control pulse TSGU ends. During this 1/4-microsecond interval, TSGU is gated by signal PHS4 and, in conjunction with the output of the branch 1 flip-flop, produces control pulse CLXC or RBIF. These control pulses are generated by the control pulse gates shown in figure 4-135.

Negative overflow exists when bits 16 and 15 of a word are logic ONE and ZERO, respectively. Negative overflow means that a large negative quantity has been produced in some manner and cannot be processed by the computer because of its limited word length. This condition is monitored during certain operations to prevent faulty computations. When negative overflow exists, a new branch state is established, and a set of control pulses designed to adjust computer operations are produced. The test is accomplished by control pulse TOV. This control pulse is gated by signal PHS2 to first clear the branch 1 and 2 flip-flops. At the same time control pulse TOV tests signal UNF. If signal UNF is present, the branch 1 flip-flop is set. Since the PHS2 signal occurs during the second 1/4-microsecond interval of a time period, the branch 1 flip-flop does not set until the third 1/4-microsecond period.

Control pulse TL15 tests bit 15 of register L. Control pulse TL15 is first gated by signal PHS3 to reset the branch 1 flip-flop and then by signal PHS4 to set the flip-flop if signal L15 is present.

Control pulse TSGN tests write line WL16 for sign. Control pulse TSGN is first gated by signal PHS3 to reset the branch I flip-flop and then by signal PHS4 to set the flip-flop if signal WL16 is present. Signal WL16 is present when the content placed onto the write lines is negative.

Signal BR1 is produced when the branch 1 flip-flop is set. Signal MBR1 is applied to an indicator on the peripheral equipment together with the output of the branch 2 flip-flop. In this manual the content of the two branch flip-flops are referred to as c(BR1, BR2) whereas the indicators on the peripheral equipment display c(BR2, BR1).

The branch 2flip-flop is used to test plus zero, positive overflow, and minus zero. It is also used to test the sign of one quantity while the branch 1 flip-flop tests the sign of another quantity. It is necessary to determine the sign of two quantities being multiplied together in order to establish the correct sign of the product. The branch 2 flip-flop is always cleared before a net input occurs. Control pulse TPZG tests for plus zero in register G. Control pulse TPZG is first gated by signal PHS3 to clear the branch 2 flip-flop and then by signal PHS4 to set the flip-flop if signal GEQZRO is present.

Positive overflow exists when bits 16 and 15 of a word are 0 and 1, respectively. Positive overflow means that computer word length has been exceeded by a large positive quantity. Signal OVF is present when this condition exists. Control pulse TOV, which also tests negative overflow, is gated by signal PHS2 to clear both branch flipflops. After the flip-flops are cleared, the branch 2 flip-flop will be set if signal TOV is present.



